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DEVELOPMENT OF TECHNIQUES FOR SHORT-RANGE
PRECIPITATION FORECASTS

Robert K. Crane

Environmental Research & Technology, Inc.
696 Virginia Road
Concord, Massachusetts 01742

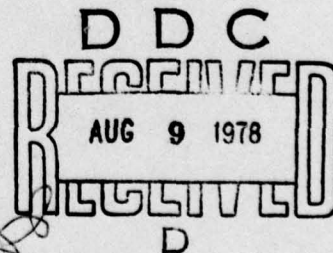
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TABLE OF CONTENTS

	Page
ABSTRACT	1
1. INTRODUCTION	5
1.1 Program Objectives	5
1.2 Summary of Results	5
1.3 Software Development	8
1.4 Organization of the Report	9
2. IMPROVEMENTS TO THE CELL DETECTION PROGRAM	10
2.1 Cell Detection Logic Changes	10
2.2 Refinements in Velocity Data Processing	11
2.3 Doppler Spread Processing	13
3. VOLUME CELL DETECTION AND TRACKING	14
3.1 Definition of a Volume Cell	14
3.2 Detection and Tracking Algorithms	16
3.3 Volume Cell Attributes	17
3.4 Software for Volume Cell Detection and Tracking	19
4. CELL FORECASTING	21
4.1 Extrapolation Along Cell Tracks	21
4.2 New Cell Development	22
5. ANALYSIS OF SELECTED DATA SETS	30
5.1 Use of the Computer Programs	30
5.2 Volume Cell Observations	33
6. RECOMMENDATIONS	42
6.1 Parameter Optimization	42
6.2 Real Time Processing	42
6.3 Spatial Analysis of Cell Development	43
6.4 Morphological and Climatological Analysis	43
REFERENCES	44
ACKNOWLEDGEMENTS	45
APPENDIX A: CELL DETECTION AND TRACKING PROGRAM INSTRUCTIONS FOR OPERATION	A-1

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TABLE OF CONTENTS (cont)

	Page
APPENDIX B: PLOTTING PROGRAM 'EXPAND' (VERSION 1.0)	B-1
APPENDIX C: TRACKING PROGRAM (ASOCCL)	C-1
APPENDIX D: COMPUTER PROGRAM LISTINGS AND SAMPLE OUTPUT	D-1

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1. INTRODUCTION

1.1 Program Objectives

The ultimate goal of the work reported herein is the development of a real-time method for the short-range (0-20 minute) forecast of storm development and motion. The initial step in this program was the development of objective techniques for the efficient representation of information obtained from a single Doppler weather radar (Crane, 1977). The radar data are processed to obtain fixed and peak referenced reflectivity contours and peak referenced tangential shear contours. The essential information contained in the contour data are represented by a set of attributes. In this report, we consider the second step in the program, the assembly of data obtained from a set of radar scans into a set of attributes that characterize the three-dimensional structure of the small precipitation cells and surrounding echo regions, their motion, and their development in time. Initial consideration is given to the problem of forecasting precipitation cell development and motion.

1.2 Summary of Results

The work performed under this contract was concentrated in three major areas: (a) improvement to the cell detection program developed under the previous contract (Crane, 1977), (b) development of the volume cell detection and tracking program, and (c) preparatory data analysis to support the development of cell forecast algorithms.

The cell detection program was extensively revised to reduce the amount of core storage required for some of the integer arrays used in peak referenced contour analysis; to process reflectivity, tangential shear, and Doppler spread data simultaneously; to include spread information in the reflectivity and tangential shear peak attributes; to use the relatively spiky nature of ground clutter as an aid in rejecting ground clutter; to resolve automatically Doppler velocity ambiguities using radial velocity data from resolution elements adjacent in range and in azimuth; and to vary the quantization steps used in the peak referenced contouring operation. In the process of revising the program additional refinements were made in the cell detection logic to correct several

defects detected using actual radar data and to improve the technique used to store temporarily the peak referenced contour data to increase the speed of the processing algorithm and reduce overall core storage. At present, the entire program required for the simultaneous processing of reflectivity, tangential shear, and Doppler spread data fits into the core storage available on the CDC 6600; a result not anticipated at the start of the program.

The program is currently relatively slow in operation due to (1) the extensive number of input and output tape or disk operations used to read the input radar data, store data for plotting, store data for subsequent volume cell detection and tracking and to store data for B scan printouts and (2) the large number of bit manipulation operations required to pack and unpack data for storage. A considerable time savings can still be accomplished by reducing the amount of output data and by rewriting the program in assembler language to reduce the time spent in subroutine calls for bit manipulation and indirect storage addressing.

A volume cell detection and tracking algorithm was developed to combine the data from successive radar scans. The fixed and peak referenced contouring operations are performed independently for each azimuth scan of the radar. The reflectivity cells (peak referenced) are associated from one elevation angle to the next to form a volume cell and from one volume cell to the next to form a track. The reflectivity cells are used to identify the basic organization of the radar data. Fixed contours that enclose associated reflectivity cells are used to determine the 3-dimensional echo envelope for the reflectivity cell (or cells). Tangential shear and Doppler spread cells are likewise associated from scan-to-scan; associated with reflectivity cells (if possible); and identified with fixed contour envelopes. The lowest threshold fixed contour that encloses each of the reflectivity, shear, or spread cells is used to tag that cell to aid in the association processing.

A new set of attributes are developed for each volume cell. A list of these attributes are given in Table I for fixed contours and for reflectivity, shear, and spread cells. The attributes to be calculated for each volume cell are readily modified. The basic volume cell detection and tracking algorithm is used to perform the scan-to-scan association.

TABLE I

VOLUME CELL ATTRIBUTES

<u>Fixed Contours</u>	<u>Reflectivity Peaks</u>	<u>Tangential Shear Peaks</u>	<u>Doppler Spread Peaks</u>
Surface Area	Reflectivity at Peak	Shear at Peak	Spread at Peak
Echo Top	Height of Peak	Height of Peak	Height of Peak
Enclosed Volume	Height of Top	Height of Top	Height of Top
Centroid Location*	Height of Base	Height of Base	Height of Base
Total Surface Precipitation	Centroid Location*	Centroid Location*	Centroid Location*
Average Surface Rain Rate	Area at Peak	Area at Peak	Area at Peak
Average Reflectivity	Volume	Volume	Volume
Maximum Enclosed Peak Values	Area at Surface	Area at Surface	Area at Surface
Profile of Areas vs Centroid	Reflectivity at Surface	Shear at Surface	Spread at Surface
Heights	Average Tangential Shear	Average Velocity Spread	Associated Reflectivity Peaks
Profile of Average Reflectivity vs Centroid Heights	Average Radial Shear	Associated Reflectivity Peaks	Associated Shear Peaks
Number of Enclosed Peaks (by type)	Average Vertical Shear	Associated Spread Peaks	
Nearest Neighbor Distances for Enclosed Cells	Average Velocity Spread		
	Associated Shear Peaks		
	Associated Spread Peaks		

*Centroid Locations are Defined on the Surface Using Data from the Lowest Possible Elevation Angle

When data from two scans are associated, they can be used readily to calculate any desired attribute. The lists given in Table I are preliminary in nature covering the parameters we currently expect to be most important in subsequent analyses. Experience with the use of these programs for a larger data set will be required before a final set of attributes can be specified.

Experience with a larger data set is required as a prerequisite to the development of cell forecast algorithms. Crane (1976) processed reflectivity data from a number of radar scans obtained at Wallops Island during the summer of 1973 by the Johns Hopkins Applied Physics Laboratory (APL) in the process of initially establishing the utility of the peak referenced contouring technique. These data were used by Crane (1976) to investigate cell lifetime and possible cell tracking/extrapolation techniques. In this study, we used the same data set to determine the relative spacings between cells. The object of the spacing study was to determine if preferred spacings are evident in nature. If so, the preferred structure can be used to forecast the most probable location for new cell development. The ability to forecast locations for new cell development would add significantly to the 0-20 minute forecast because the median cell lifetime is less than 20 minutes and forecasting by extrapolation along a cell track is not adequate. An examination of the Wallops Island data revealed that the nearest neighbor distances between cells were between 7 and 9 km and that these distance values did not depend on the type of rain observed. This suggests that new cell site forecasts are feasible.

1.3 Software Development

The goal of this contract with the Air Force Geophysics Laboratory (AFGL) is to provide efficient computer software to obtain parameters to represent the essential information obtained in a sequence of scans of a single Doppler weather radar. The radar used to provide the data is the C-band Doppler radar operated by the Weather Radar Branch of AFGL at Sudbury, Massachusetts. The computer programs were prepared for the CDC-6600 at AFGL.

There are now three separate programs in the sequence of programs to be used for weather radar data processing. The first is the cell

detection program which was developed under the previous contract (Crane, 1977) and extensively modified during the course of this contract. The second is a plotting program used to display contours and cell centroids. This program was developed under the previous contract and modified under this contract to display separately the locations of the centroids of the fixed echo regions and the centroids for each of the peak detected cells - reflectivity, tangential shear, and Doppler spread cells. The third program detects and tracks volume cells. It was developed under this contract. This program uses data generated by the cell detection program to develop three-dimensional cells and to describe their location, height and intensity. The volume cell attributes are listed in Table 1.

The ultimate goal of this work will be the development of real-time radar processing techniques to be used on a dedicated computer system that is an integral part of the radar system. The programs generated to date on the current contract are exploratory in nature. They were designed to fit within the core storage limitations of the CDC-6600 computer but still have a high degree of flexibility in modifying storage array sizes and in providing auxilliary output for testing the program. The program design had real-time processing in mind and, in the end, should be reasonably efficient when tailored to an on-site computer system. Listing and operating instructions for the programs developed on this contract are included in the appendices.

1.4 Organization of the Report

A summary of the modifications to the cell detection program and plotting program is given in Section 2. A description of the volume cell detection program is given in Section 3. Initial consideration of the cell forecasting problem is given in Section 4. Sample outputs are provided in Section 5. Section 6 summarizes progress to date and provides recommendations.

2. IMPROVEMENTS TO THE CELL DETECTION PROGRAM

2.1 Cell Detection Logic Changes

The cell detection program was modified to include the detection of Doppler spread peaks and to pack integer addresses used in the peak detection routine six to a CDC word. The latter change was required to make room for the additional data used in Doppler spread processing. In the process of revising the address storage procedure, a number of minor logic errors were detected. These errors were associated with the operation of the radial-to-radial association of contours at different threshold levels (see Section 5.2 of Crane, 1977). The errors have been corrected and, in the process, changes were also made to streamline the storage of the temporary contour data.

At present, the temporary attribute storage array (TATR in subroutine PEAKD, see Appendix D) is used to identify active cells at each possible threshold level (relative to the peak level for the cell) and to store pointers to previously associated active cells as well as provide partial attribute summations for the active cells. The TATR array is doubly subscripted maintaining temporary storage for the number identification of the peak for the active cells. For each active cell the stored data includes the current estimate of the peak value; a set of partially summed attribute values for each of the nested contours for each possible threshold level below the peak, area, average value, centroid location plus, for reflectivity cells, Doppler spread, radial shear, tangential shear, and radial velocity; the azimuth count for the last azimuth on which the attributes for each contour were updated; and a pointer to the enclosing fixed contour. This last item is included for later use in the volume cell detection program. If a cell is not active at a particular threshold level but was previously active on the current radial, the area attribute contains a pointer to the cell, now active at that level. After processing the data for a radial the cell-to-cell pointers are zeroed. If a cell becomes inactive, all pointers to that cell are also zeroed before processing data for the next radial.

The program as it now stands is configured to allow rapid changes in the dimensions of all the storage arrays. This convenience costs in

producing relatively longer processing times than for a program with fixed storage allocations. A final program modification should be made when the exploratory runs of the computer program are finished to fix the array sizes and optimize the program for rapid operation.

2.2 Refinements in Velocity Data Processing

The program was modified to provide automatic resolution of Doppler velocity ambiguities. The first detected velocity data for each scan is assumed to be in the velocity interval spanning zero velocity. Successive observations at different but adjacent range or azimuth locations are assumed to differ from the first observation by less than the velocity ambiguity. If the difference is larger, it is adjusted so that it is smaller by adding or subtracting a value equal to the velocity ambiguity ($\lambda/2 \cdot \text{PRF}$ where λ is the wavelength and PRF is the pulse repetition frequency). The data for each radial are then reexamined to ensure that each velocity observation differs from the average of the velocity values for the two surrounding range intervals by less than the velocity ambiguity and adjusted again if required.

The above processing is used for contiguous range and azimuth elements. If large spacings exist between regions of radar data above the processing threshold, the first data point in one region is compared with the average velocity for the previous region. The data therefore are objectively adjusted to remove ambiguities. Provision is provided to reject data from this analysis if the Doppler spread is not within pre-set bounds but this option has not been exercised.

The processed data appear to be reasonably smoothly varying as indicated in Figure 1. The tangential shear data obtained by numerically differentiating the radial velocity data are however, more variable as illustrated in the figure. The apparent noise evident in the tangential shear field led to the inclusion of Doppler spread data in the analysis process. The program was also modified to introduce a new constant to specify the quantization interval for peak detection contouring. By setting this constant, additional control is exercised over the peak detection process. Referring to Figure 1, no peaks would be detected if the quantization step is 1 m/s but a number of peaks are detected for a 0.1 m/s quantization step (see Section 5).

NA RANGE (3/2 M. INCREMENTS)

0 1 2 3 4 5 6 7 8 9 0 1 2 3 4 5 6 7 8 9 0 1 2 3 4 5 6 7 8 9

REFLECTIVITY 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31 32 33 34 35 36 37 38 39 40 41 42 43 44 45 46 47 48 49 50 51 52 53 54 55 56 57 58 59 60 61 62 63 64 65 66 67 68 69 70 71 72 73 74 75 76 77 78 79 80 81 82 83 84 85 86 87 88 89 90 91 92 93 94 95 96 97 98 99 100

RADIAL VELOCITY 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31 32 33 34 35 36 37 38 39 40 41 42 43 44 45 46 47 48 49 50 51 52 53 54 55 56 57 58 59 60 61 62 63 64 65 66 67 68 69 70 71 72 73 74 75 76 77 78 79 80 81 82 83 84 85 86 87 88 89 90 91 92 93 94 95 96 97 98 99 100

VELOCITY SPREAD 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31 32 33 34 35 36 37 38 39 40 41 42 43 44 45 46 47 48 49 50 51 52 53 54 55 56 57 58 59 60 61 62 63 64 65 66 67 68 69 70 71 72 73 74 75 76 77 78 79 80 81 82 83 84 85 86 87 88 89 90 91 92 93 94 95 96 97 98 99 100

TANGENTIAL SHEAR 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31 32 33 34 35 36 37 38 39 40 41 42 43 44 45 46 47 48 49 50 51 52 53 54 55 56 57 58 59 60 61 62 63 64 65 66 67 68 69 70 71 72 73 74 75 76 77 78 79 80 81 82 83 84 85 86 87 88 89 90 91 92 93 94 95 96 97 98 99 100

Figure 1 Sample Data Set Including Two Fixed Contour Echo Areas and Three Reflectivity Peaks

2.3 Doppler Spread Processing

Velocity variance data may now be routinely processed using the computer program. Facilities to analyze this data field were added because of the apparently high noise levels in the tangential shear data and the expectation that at high signal-to-noise ratios, the spread data may be more reliable. As discussed before (Crane, 1977), the spread data are assumed to contain the same information as the tangential shear data due to the dominant effect of velocity fluctuations on the scale of the antenna beamwidth at the observation range. Both data fields are now processed to allow an intercomparison between the information available from each field and to investigate their relative sensitivity to noise.

The velocity variance output from the pulse pair processor is known to be adversely affected by low signal-to-noise ratios. A noise level dependent threshold parameter is provided for thresholding the velocity variance data but has not been exercised as yet. To reduce the sensitivity of the variance data due to noise, the square root of the variance is used for analysis of the Doppler spread. A sample of this data is depicted in Figure 1. It is noted that the velocity data, radial velocity, Doppler spread, and tangential shear, are processed only when the reflectivity values are above the lowest (processing) threshold level which, for this figure, is 20 dBZ. High Doppler spreads are evident in two regions of the figure, (1) at low reflectivity values and (2) at high reflectivity values. The high spreads at low values are presumably caused by signal-to-noise problems and should be suppressed using the signal-to-noise threshold level. The high values corresponding to the higher reflectivity values are presumably real, although the correlation with the tangential shear values is not good for the data in this figure. A larger data sample must be analyzed to optimize the processing of tangential shear and/or Doppler spread data.

Modifications for Doppler spread processing were made in several areas of the program. The largest change included the addition of temporary attribute storage arrays for the detection of Doppler spread peaks. In addition, the reflectivity peak and tangential shear peak detection algorithms were changed to increase the number of attributes so the average Doppler spread within a detected cell could be determined. This attribute is now listed with the others as described in Section 5.

3. VOLUME CELL DETECTION AND TRACKING

3.1 Definition of a Volume Cell

The cell detection program provides, as one of its outputs, a list of attributes for fixed contours, reflectivity peaks, tangential shear peaks, and Doppler spread peaks. At a minimum, each attribute list defines the average value, area, and centroid location of each cell for each azimuth scan of an elevation scan sequence. The expected scan sequence for the radar includes azimuth scans (or azimuth sectors in a raster scan) at successively higher elevation angles until a complete volume scan is completed. The data for each elevation or tilt of the scan sequence must be combined with the data from other tilts to provide a three-dimensional picture of each cell or echo volume.

The process of combining data from scan to scan in a volume scan sequence is illustrated schematically in Figure 2. This figure represents a height section through three cells. The contours represent quantized data (e.g. reflectivity data in 1 dB steps) that have been processed on each azimuth scan to produce a set of reflectivity peak cells. The minimum attribute set is identified by the length of the heavy bar (detected length or in three-dimensions, the cell area) and its location (centroid) on each tilt. The data obtained for the lowest tilt is assumed to extend to the surface. The height of the centroid is determined from the range to the centroid and the elevation angle for the scan.

The three-dimensional cell or volume cell is defined by the volume enclosed within the peak detected cells that are associated from scan-to-scan. A criterion similar to the one used to define a peak referenced cell is used to define the volume cell. From the sequence of attributes for cells detected scan-to-scan, cells 1, 2 and 3 on this figure, a peak value and its height may be selected. The top and base of the volume cell are defined by the height at which the reported average value drops the required number of quantization units below the peak value. This height is determined by extrapolation if detected cells are obtained for each tilt or is taken as halfway between the height of a value above the required threshold and the expected height of the intersection of the cell with the next tilt plane if no associated cell was detected on the next scan. The locations of the peaks, tops, and bases are depicted on the

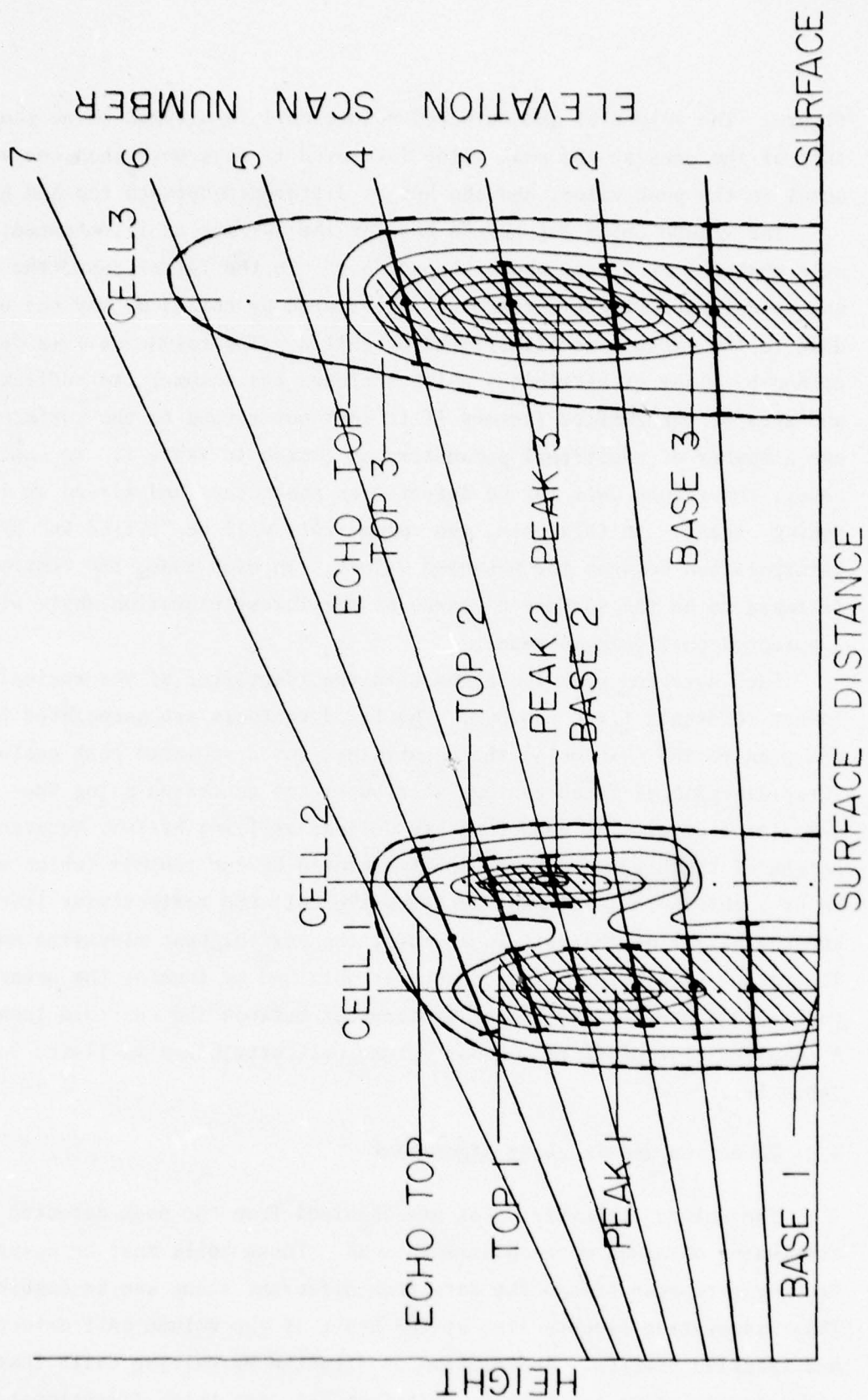


Figure 2 Illustration of Scan-to-Scan Data Association in a Volume Scan Sequence

figure. The volume of the detected volume cell is assumed to be the product of the area at the peak value (averaged if have more than one value equal to the peak value) and the height difference between top and base.

The volume cells may have a base at the surface as illustrated by cell number 1 or a base above the surface. In the latter case, the cell may be detected at the surface as illustrated by cell 3 or may not extend down to the surface as illustrated by cell 2. The volume cell is described by a set of attributes which includes its volume, its reflectivity and area at the surface (zeroes if it does not extend to the surface) and a number of additional parameters as listed in Table I. In some cases, the volume cell may be detected on some scans and missed on intervening scans. In this case, the volume cell will be "filled in" by interpolation between the measured values. In each case, the centroid is taken to be the surface distance at the lowest elevation angle with a detected cell (single scan).

Each detected peak is tagged with the identifier of the enclosing lowest threshold fixed contour. The fixed contours are associated from one scan to the next using the identifiers for associated peak cells. Three-dimensional fixed contour attributes are generated using the associated data. The echo tops are defined as lying halfway between the height of the highest detected peak enclosed by the contour (which may be at a threshold level many dB below the cell top reflectivity level) and the height of the cell location at the next highest elevation angle. The volume within the fixed contour is obtained by summing the areas on each scan and using the height differences between the centroid locations. A complete list of fixed contour volume cell attributes is listed in Table I.

3.2 Detection and Tracking Algorithms

The volume cell attributes are obtained from the peak detected cell attributes obtained on each azimuth scan. These cells must be associated from scan-to-scan before the data from different scans can be combined. This association process lies at the heart of the volume cell detection and tracking process. Association is affected by pairing cells that are sufficiently close together to come from the same three-dimensional structure. The location of the contours surrounding each peak is not available

for use by the association algorithm. Association is accomplished by first selecting cells from each scan whose centroid locations, when projected on the surface, are separated by less than the square root of the combined areas, plus the distance the cell might move during the interval between scans, plus a fixed distance to account for the statistical centroid location uncertainty introduced by the expected variability of the radar data. Comparison is always made between the cell location for a particular scan and the detected volume cell location from the lowest elevation scan on which it was observed.

In most cases, only pairs of cells will be evident from the association algorithm listed above. Occasionally, in a cluster of cells, more than one cell may meet the association criterion. In this case, the cells will be associated by picking those cells which are closest after a uniform offset is made between cell locations to provide the largest number of associations. This is illustrated in Figure 3. In this figure, the cell to be tested, cell A, is closest to the previously detected volume cell number 2, but after translation of the surface locations relative to each other by the amount shown by the straight line on the figure, all three cells (lettered) may be associated with the detected cells (numbered) with smaller physical separations. This procedure for conflict resolution (correlation) will be used only when the resultant translation is physically realizable (i.e. corresponds to a possible cell tilt or translation velocity).

The scan-to-scan cell association logic is also used for volume-to-volume scan sequence association for cell tracking. For the tracking problem, the translation analysis for conflict resolution becomes more important and guidance in selecting the appropriate translations is taken either from a prescribed wind vector (700 mb wind for instance) or from the results from the previous scan. The conflict resolution or correlation algorithm is performed separately for large echo regions in that the translation values are allowed to vary from one echo region to the next.

3.3 Volume Cell Attributes

The volume cell attributes were partially defined in Section 3.1 and are listed in Table 1. A different set of attributes is generated for

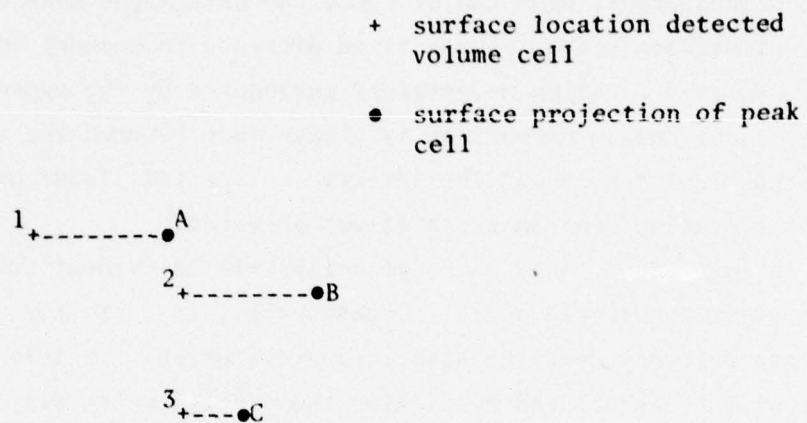


Figure 3 Illustration of Scan-to-Scan Association
for Volume Cell Detection and Tracking

each volume cell type. Fixed contour attributes include measurements of the total precipitation produced within the echo region, average rain rates on the surface, profiles of area and of average reflectivity for the data contained within the fixed contour envelope, and summaries of the numbers and locations of peak referenced cells detected within the echo envelope. The peak referenced volume cell attributes include the size, intensity, and location parameters listed above plus information on associated volume cells of different types. The reflectivity peak attributes also include average spread and shear values for data obtained within the cell (between base and top). The vertical shear values are calculated using the variation of the average radial velocity with height.

Each detected volume cell is characterized by its attributes. Each volume cell track by the time variation of its attributes. In addition, tracks may be characterized by a lifetime and average velocity. Observations obtained to date indicate that the individual peak referenced reflectivity cells neither merge nor split but only develop and translate. Observations of a much larger data set are needed to verify this model for small cell behavior. The larger fixed contour regions may merge or split depending upon its stage of development. By tracking the enclosed cells and maintaining the cell to fixed contour identification relationship, the merger, growth, division and decay of the larger echo regions may be automatically taken into account. The morphology of the echo development process may be important to the understanding of precipitation dynamics, however, suitable attributes to characterize the relevant processes have yet to be defined. Again, experience with a significantly larger data set is required before further progress can be made.

3.4 Software for Volume Cell Detection and Tracking

A computer program (TRACK) was generated under this contract to associate cells from scan-to-scan, resolve conflicts between multiple associations and generate the volume cell attributes listed in Table I. The listing is provided in Appendix D and operating instructions are given in Appendix C. The program processes data which have been generated by the cell detection program (EXTRAD) and then recorded on disk or tape; the algorithms described in Sections 3.1 to 3.3 are used. The current output is a list of attributes for each detected volume cell (or

track). These outputs are again stored on disk or tape and listed on printout for subsequent analysis. Programs have not been generated as yet to summarize the track histories, do climatological analysis, or provide samples for case study analysis.

4. CELL FORECASTING

4.1 Extrapolation Along Cell Tracks

Short range, 0-20 minute, forecasts are of importance for severe weather warning and weather hazard avoidance. The objective of a forecast on this time (and by implication comparatively small distance) scale is the occurrence of a severe event at a point or over a small area such as an airport or the approach path to the airport. Events such as high winds produced by downbursts or by gust fronts, or regions of intense hail fall are of most interest. Larger time and area forecasts may be made of the probable occurrence of a severe weather event but the problem considered here is the remote detection, tracking, and prediction of the development and decay of a severe weather event. The first parts of the problem, the detection and tracking of small scale features in the radar data, were considered in previous sections. The association of these features with severe weather events is a second problem that is not being considered under this contract. The third part, the forecast of cell development and motion are given initial consideration in this section.

The short range forecast problem considered here is different from most meteorological forecast problems in that the occurrence of at least one cell is assumed. The problems are where will it move, how will it develop in time, where will new ones develop, and will it produce a severe weather event. The measure of success of the forecast procedure must depend upon the particular problem addressed. The success of a cell position forecast should be measured by the distance between its actual position and forecast position at forecast time. The success of the cell development forecast should be measured by the difference between the actual intensity (reflectivity, say) and forecast intensity at forecast time. Classical evaluation procedures that test the occurrence or non-occurrence of the event at a number of geographical locations are not recommended in that the reason for failure of the forecast may not be readily apparent.

Crane (1976) used data obtained by APL at Wallops Island to perform some initial tests of cell tracking/track position forecast algorithms. He assumed that a single cell motion vector would adequately describe the

propagation of a field of cells and tested that assumption by measuring the along track and cross track position errors as a function of forecast time (0-20 minutes). His results showed that the forecast error (position) was the order of the cell diameter (median value) at the half life (median lifetime) of the cell. He also found that the half life was of the order of 10 to 15 minutes and the median cell diameter was of the order of 3 km. This result was, however, based on a limited amount of data.

Crane found that the operation of the track extrapolation forecast procedure could be improved by using different motion vectors for different regions of the display area (see Figure 4 for an example showing the different directions possible for cell tracks observed during the same time interval). This idea is incorporated in the volume cell detection and tracking program. The major problem of using extrapolation along a track for forecasting is the relatively short lifetime of most cells. The largest and most intense cells persisted for a relatively long time, 40 to 50 minutes. Except for these cells, the cell could disappear by forecast time and a significant number of new cells could appear. Forecasts based upon cell time histories could be used to estimate cell lifetime but the forecast of new cell site development is a major problem for any radar data based short range forecast procedure.

4.2 New Cell Site Development

The requirement for a procedure to forecast the most probable sites for new cell development and the observation of a seemingly persistent organization or structure for the location of active cells lead to an investigation of the most probable distance or spacing between the cells. The Wallops Island data previously processed by Crane (1976) were used for this analysis. The data consisted of computer prepared maps of detected cell locations for each of the azimuth scans processed from the 1973 summer data set provided by APL. Nearest neighbor distances were obtained from the data to investigate the existence of persistent dominant scales for cell organization. The smallest, second and third shortest distances between each cell and its neighbors were determined and tabulated for each cell for each available volume scan. It is noted that with the processing technique used, the distance between two closely spaced cells is counted twice, each cell being the nearest neighbor of the other. Nearest

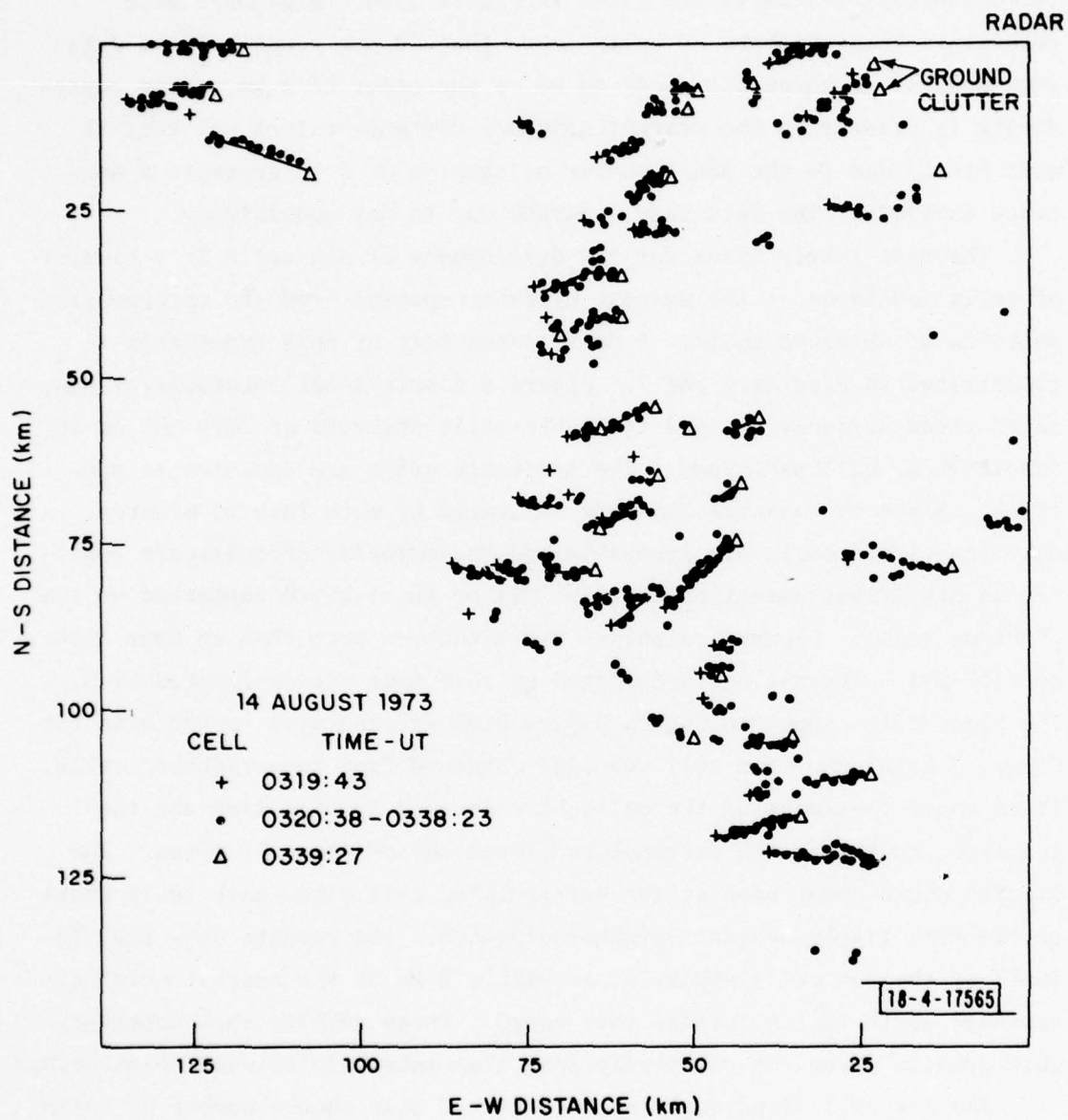


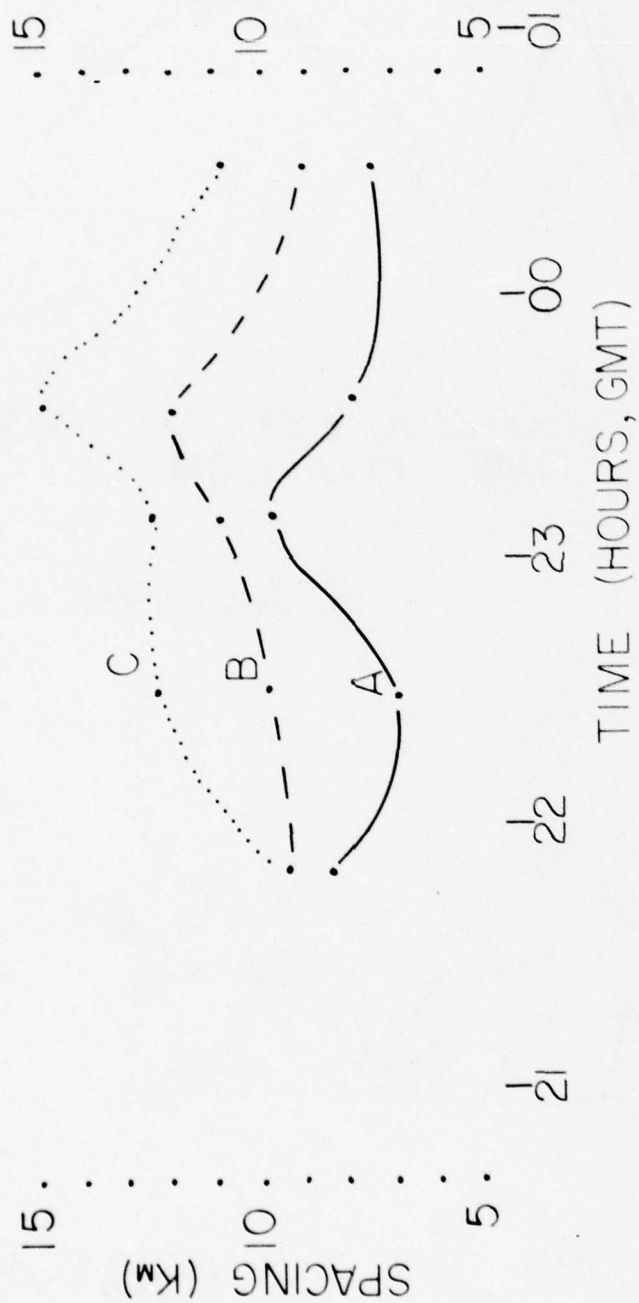
Figure 4 Cell Tracks for a 20-minute Interval Observed by the Wallops Island SPANDAR Radar (from Crane, 1976)

neighbor distributions were generated for each scan. The mode for each distribution was used to estimate the most probable cell spacing for that scan. Time histories of the modal values for the smallest, second and third shortest distances are given in Figure 5 for three days with relatively large numbers of cells (more than 20 per scan). These data show nearest neighbor distances to be on the order of 8 km. Some periodicity is evident in the nearest neighbor distance values but this is most likely due to the small number of samples used to generate a distance estimate. The data show a marked day to day consistency.

The most likely sites for the development of new cells in a cluster of cells should be at the nearest neighbor spacing from the extrapolated position of observed cells. A preliminary test of this hypothesis is illustrated in Figures 6 and 7. Figure 6 displays the locations of new, short-lived or decaying, and trackable cells observed at 2229 GMT on 18 June 1973 at Wallops Island. The trackable cells are depicted at mid-track. Since the observations are separated by more than 20 minutes, only long-lived cells are trackable and the majority of cells are depicted as new (first detection at 2229 GMT) or short-lived (detected on the previous scan). Figure 7 displays the situation more than an hour later, at 2337 GMT. The new cells depicted at this time are designated by N. The older cells shown on Figure 6 have been extrapolated to the time for Figure 7 using the mean cell velocity obtained from the trackable cells. It is noted that most of the cells have decayed by this time and the locations represent the extrapolated locations of the cell sites. The circles drawn about each of the extrapolated cell sites have radii equal to the most likely nearest neighbor distance. The results show that 23 (66%) of the new cells appear at or within 2 km of the nearest neighbor distance while 12 lie outside this range. These results show considerable promise given the relatively long time intervals between observations.

The new cell sites depicted on Figure 7 also show a number of cells approximately spaced from each other by the nearest neighbor distance but not connected to an older cell site. A forecast based upon a more complex pattern using the nearest neighbor distances in a more regular extended structure may be capable of predicting the locations of a larger number of cells. The structure may also reduce the size of the region

A - NEAREST NEIGHBOR
 B - SECOND NEAREST
 C - THIRD NEAREST



18-19 JUNE 1973

Figure 5 Nearest Neighbor Distances

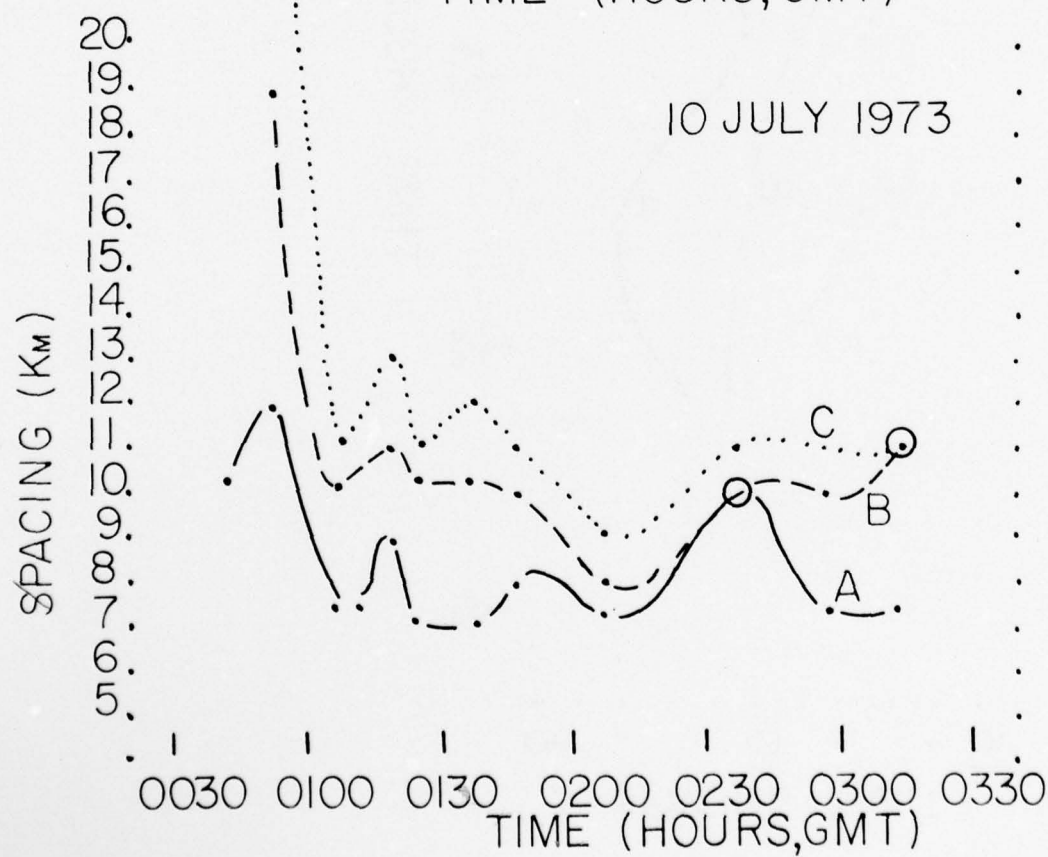
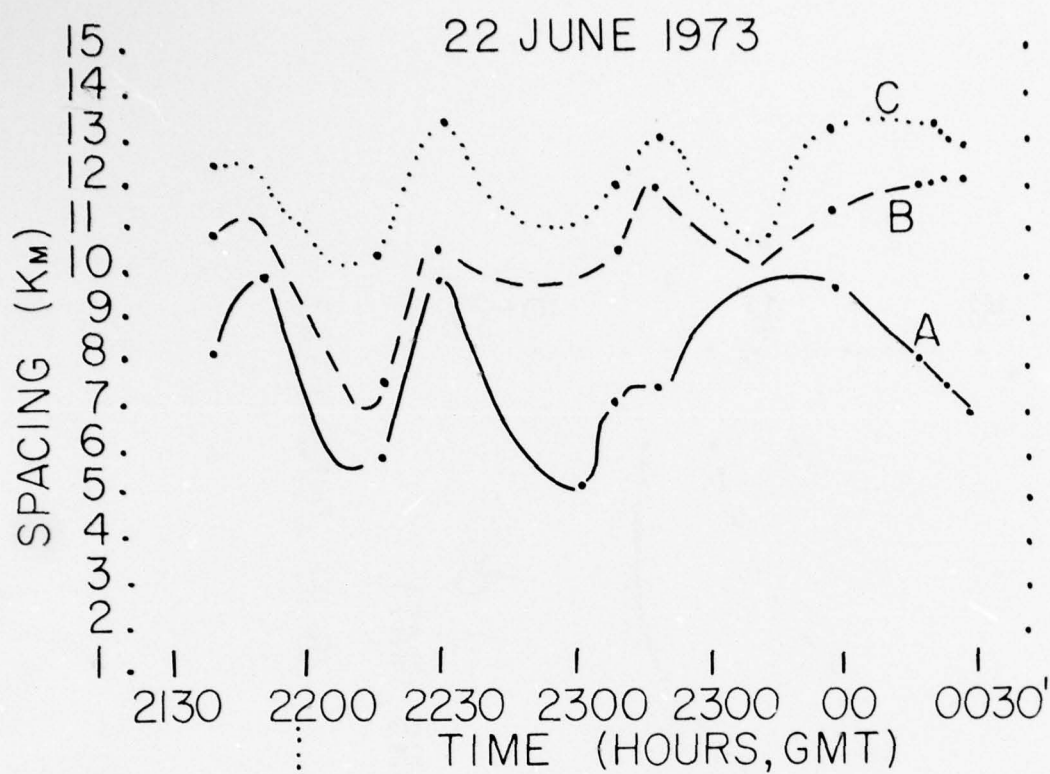


Figure 5 (cont) Nearest Neighbor Distances

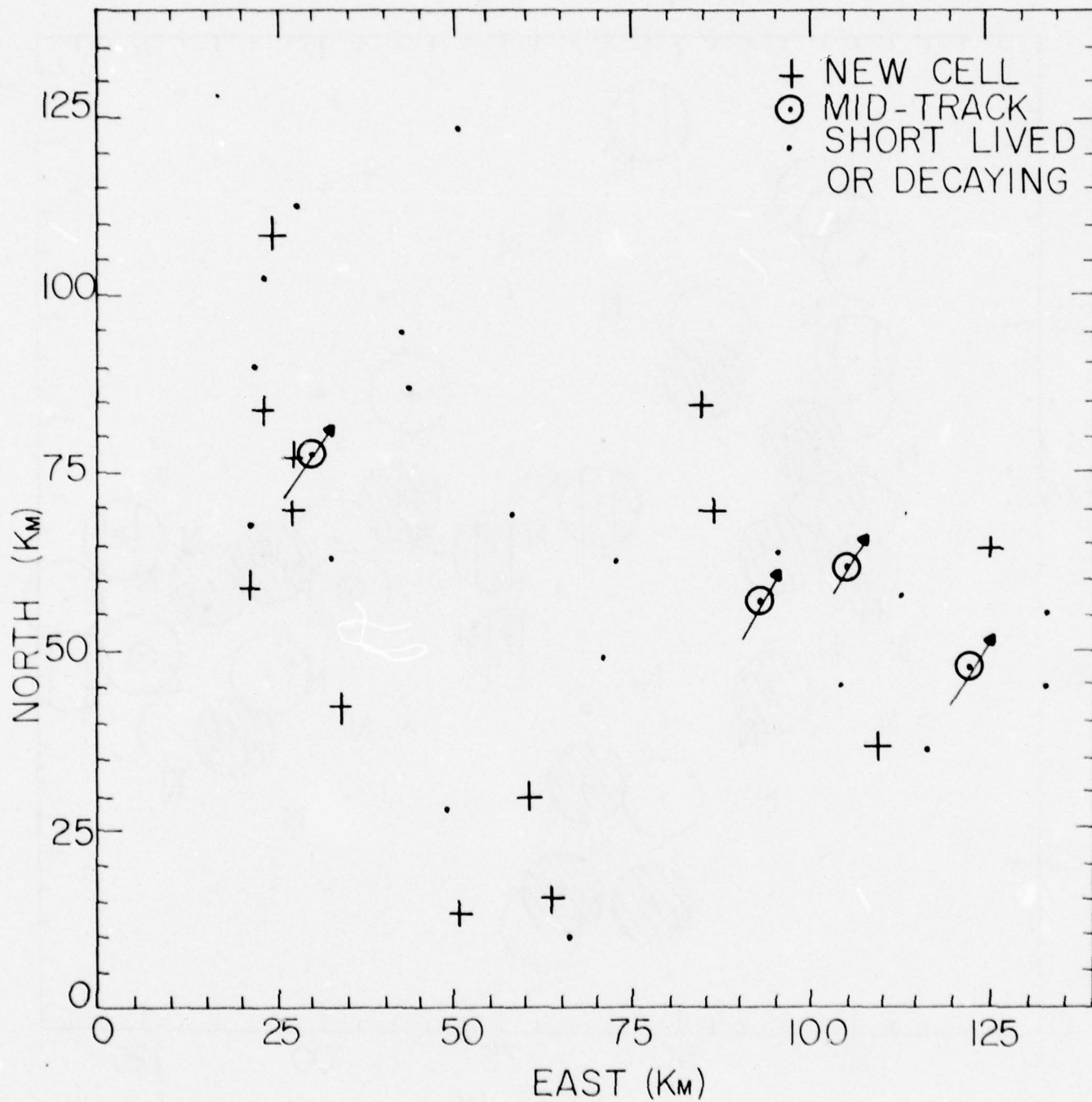


Figure 6 Cell Locations at 2229 GMT, 18 June 1973 at Wallops Island

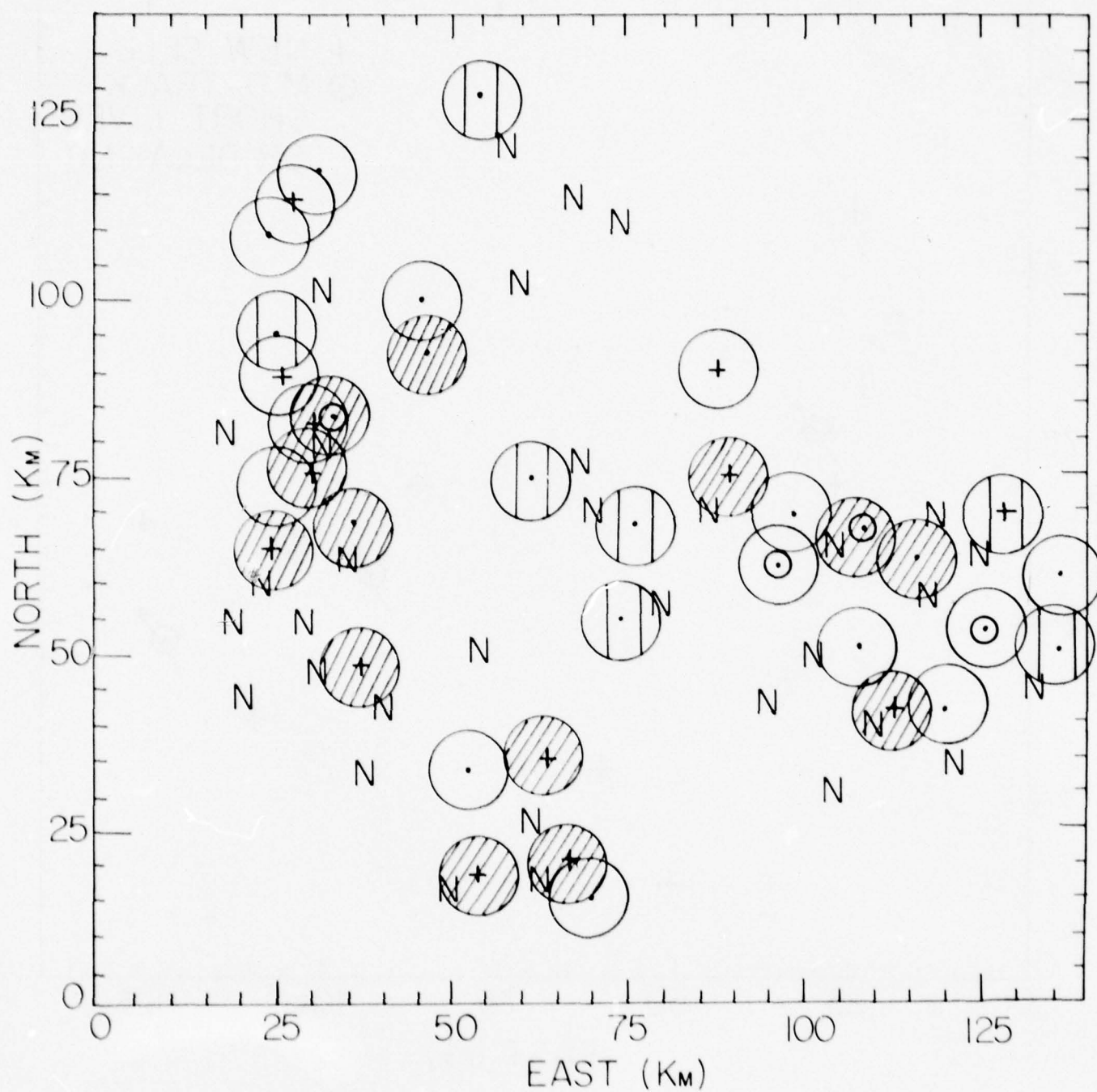


Figure 7 Cell Locations at 2337 GMT, 18 June 1973 at Wallops Island

forecast for probable new cell development by specifying a segment or segments of the nearest neighbor arc. A considerably larger sample of data with smaller time steps between observations is required before a procedure for new cell site forecasting can be developed and tested. The preliminary results presented here are encouraging and indicate that a new cell site forecasting procedure can be developed.

5. ANALYSIS OF SELECTED DATA SETS

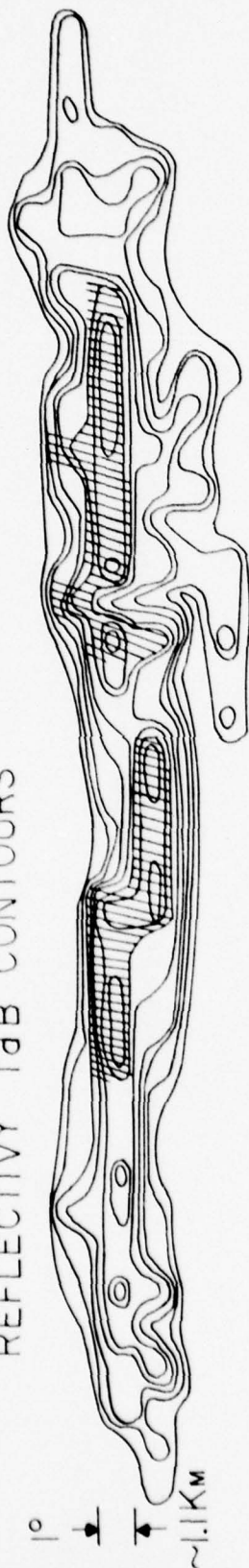
5.1 Use of the Computer Programs

The computer programs described above were developed as a prototype for a real-time processing system to be employed in reducing the number of data bits required to describe a set of radar observations. The objective of the program was to replace the large volumes of data obtained by a radar system to a set of fixed contour and peak referenced cell attributes capable of representing the same essential information. A prototype program is now available with optional choices for many of the processing parameters and for representing the cell and contour attributes. The major thrust of this contract has been program development and initial testing of critical hypotheses such as the possibility of forecasting the locations of new cell sites. A considerable amount of work still remains using the programs to optimize the processing parameters.

An example of the input radar data for a pair of fixed contours is given in Figure 1. The raw data are the three input parameters, reflectivity, radial velocity, and Doppler (or velocity) spread. An internally generated data field, tangential shear, is also depicted. Contoured data for the three fields used in further processing for one of the echo regions are depicted in Figure 8. In this figure, the quantization steps for each data field are 1 dB, 0.5 m/s, and 0.1 m/s/km for the reflectivity, spread, and tangential shear fields respectively. The reflectivity data show relatively long, thin contours. The basic resolution element for processing, 1° by 0.3 km, is a square on this figure. For more efficient processing, the resolution elements should be adjusted so the contours to be detected are nearly circular. The radar data are read into the computer in 1° by 0.15 km resolution elements. In this example, the data along a radial should be averaged by at least a factor of 6 (3 times the factor used for this figure) to produce $1^\circ \times 0.9$ km resolution elements. This adjustment may be made automatically in the cell detection program. The spread and tangential shear data show large changes from one resolution element to the next although, with the quantization steps used, the data reveal the same tendency toward elongation as the reflectivity data.

Contours enclosing peak detected cells are indicated by the cross hatching on Figure 8 and on Figure 9. The contours are generated at

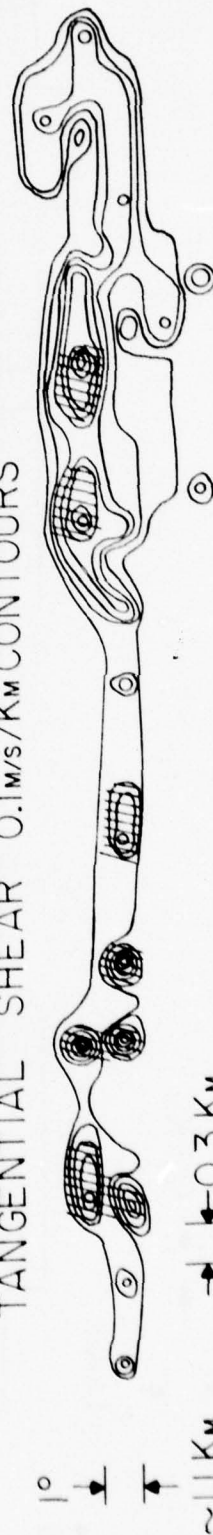
REFLECTIVITY 1dB CONTOURS



DOPPLER SPREAD 0.5 m/s CONTOURS



TANGENTIAL SHEAR 0.1 m/s/Km CONTOURS



three quantization units below the peak values. The outer contour for reflectivity on Figure 8 and the outer contour on Figure 9 correspond to the 20 dBZ threshold used for processing. Two reflectivity peaks were detected although a shoulder on the first peak (in range, the shoulder is at shorter ranges) would have been detected as an individual cell if two quantization steps were used to define the cell. The shoulder would also be included with the two detected cells in a single cell if the 1° by 0.9 km resolution area were used.

The tangential shear and Doppler spread peaks are shown superimposed on the reflectivity contours in Figure 9. The two tangential shear peaks occur for each reflectivity peak if the shoulder were included. These peaks together with the reflectivity data appear to be delineating the updraft, down draft structure of the cell. With a change to a 1° by 0.9 km resolution area, these sub-cell structures would be averaged to a consistent, one cell picture for this echo region. The Doppler spread data reveal two types of peaks, four of the seven detected peaks coincide with the tangential shear peaks outlining regions of high shear and high spread. These peaks are also intimately related to the reflectivity structure. Three other Doppler spread peaks also are evident at the very edges of the 20 dBZ contour. These peaks correspond to regions of relatively low reflectivity (23 dBZ and lower) and ostensibly represent regions where low signal-to-noise values give rise to deceptively high Doppler spreads.

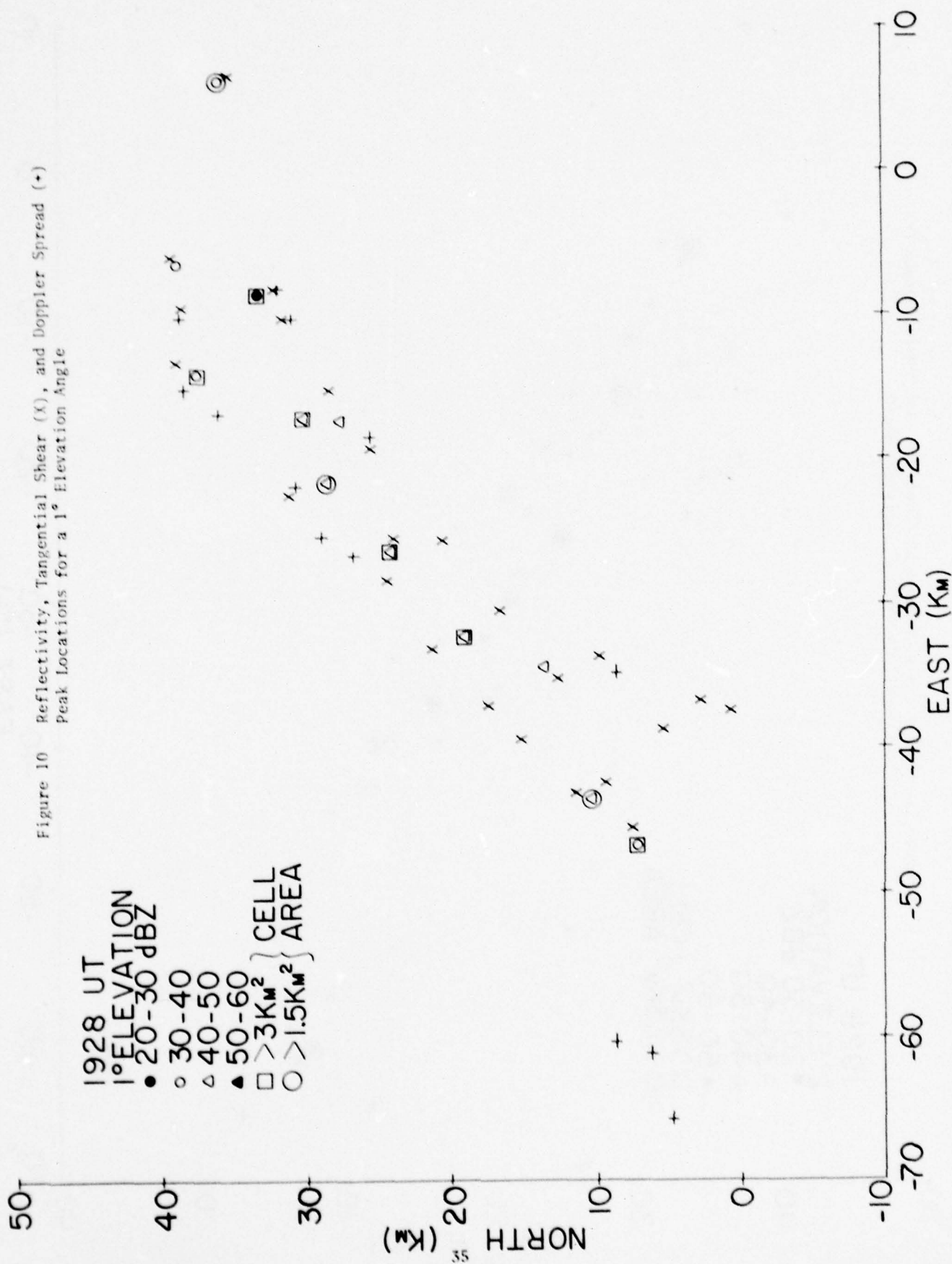
The number and shapes of the peak referenced cells will vary as the quantization step size, the number of quantization steps for peak detection, and the size of the resolution area are changed. More experience is required using these computer programs to select the optimum combination of these parameters for the detection of physically meaningful cells. As used in generating Figures 8 and 9, it appears that too much detail is present and some of the detected regions especially for spread and tangential shear data represent structure on too small a scale (for example, the individual updraft and downdraft regions within a cell).

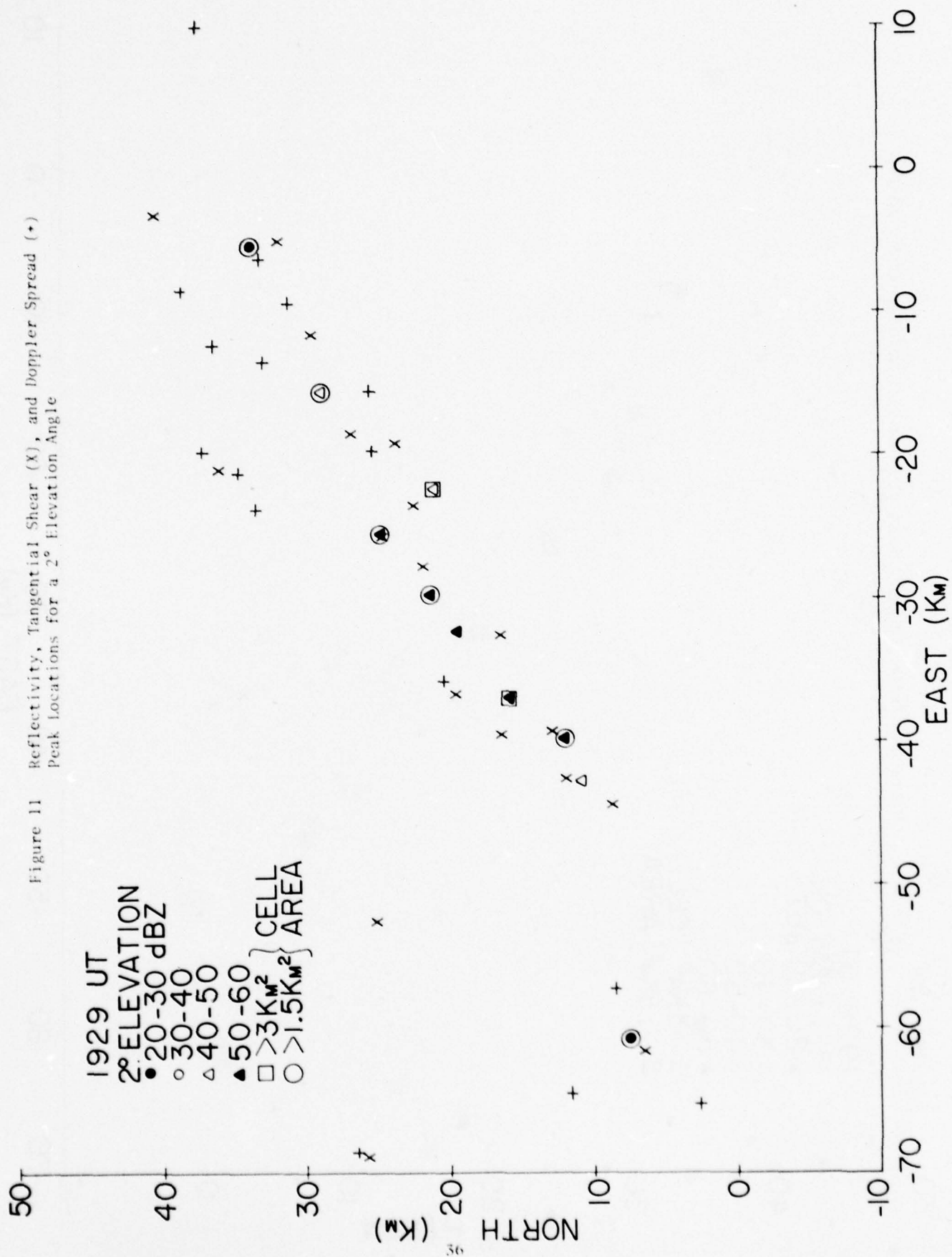
5.2 Volume Cell Observations

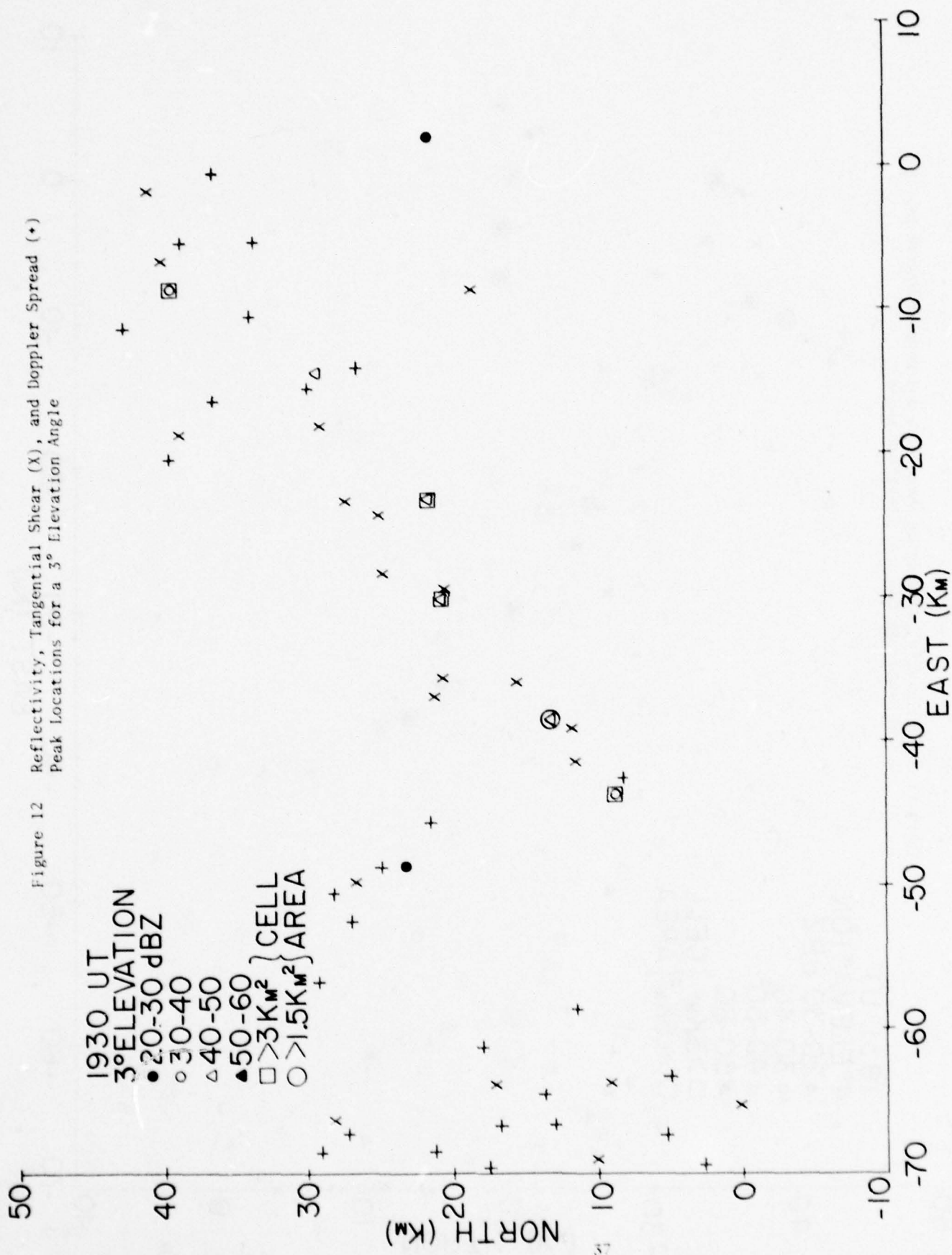
The volume cell detection program is used to combine the data from a number of individual azimuth scans. Data obtained from the Sudbury radar, subsequent to 1928 GMT on August 13, 1975 using 1° by 0.9 km

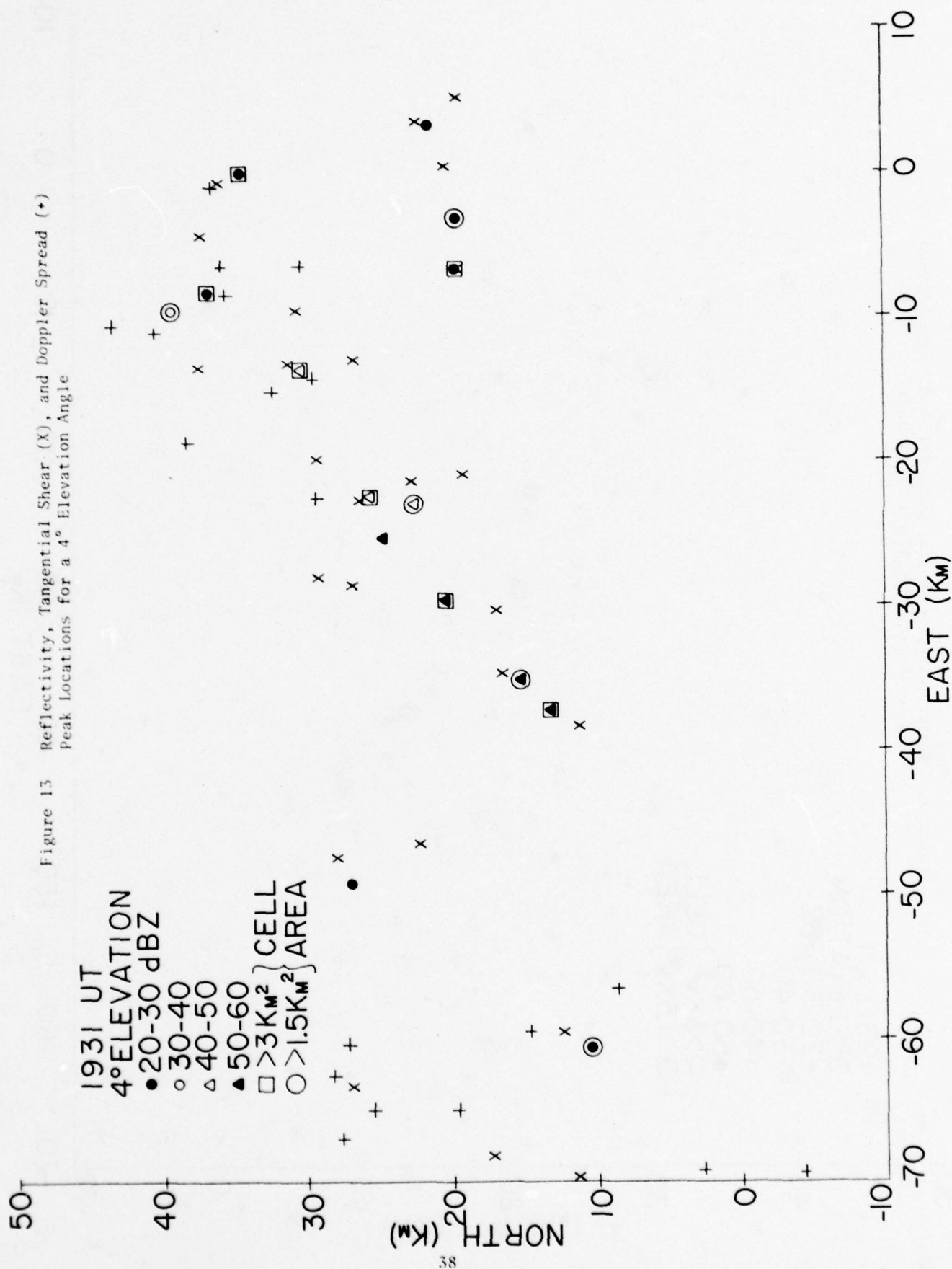
resolution areas are depicted in Figures 10-14. These data show the centroid location of each reflectivity peak referenced cell coded both by average reflectivity and by area. The locations of the tangential shear peaks are denoted by X and the locations of Doppler spread peaks are denoted by +.

The data from each of the scans were combined to form volume cells shown in Figure 15. In this figure, the solid lines connect the cell locations as detected on each scan using the algorithms described in Section 3 (Track Program). Cells within 50 km of the radar were detected at elevation angles up to 5° ; cells at further ranges were only detected at elevation angles below 4° (heights less than 5 km). A limited set of volume cell attributes for this data set is listed in Table 2.









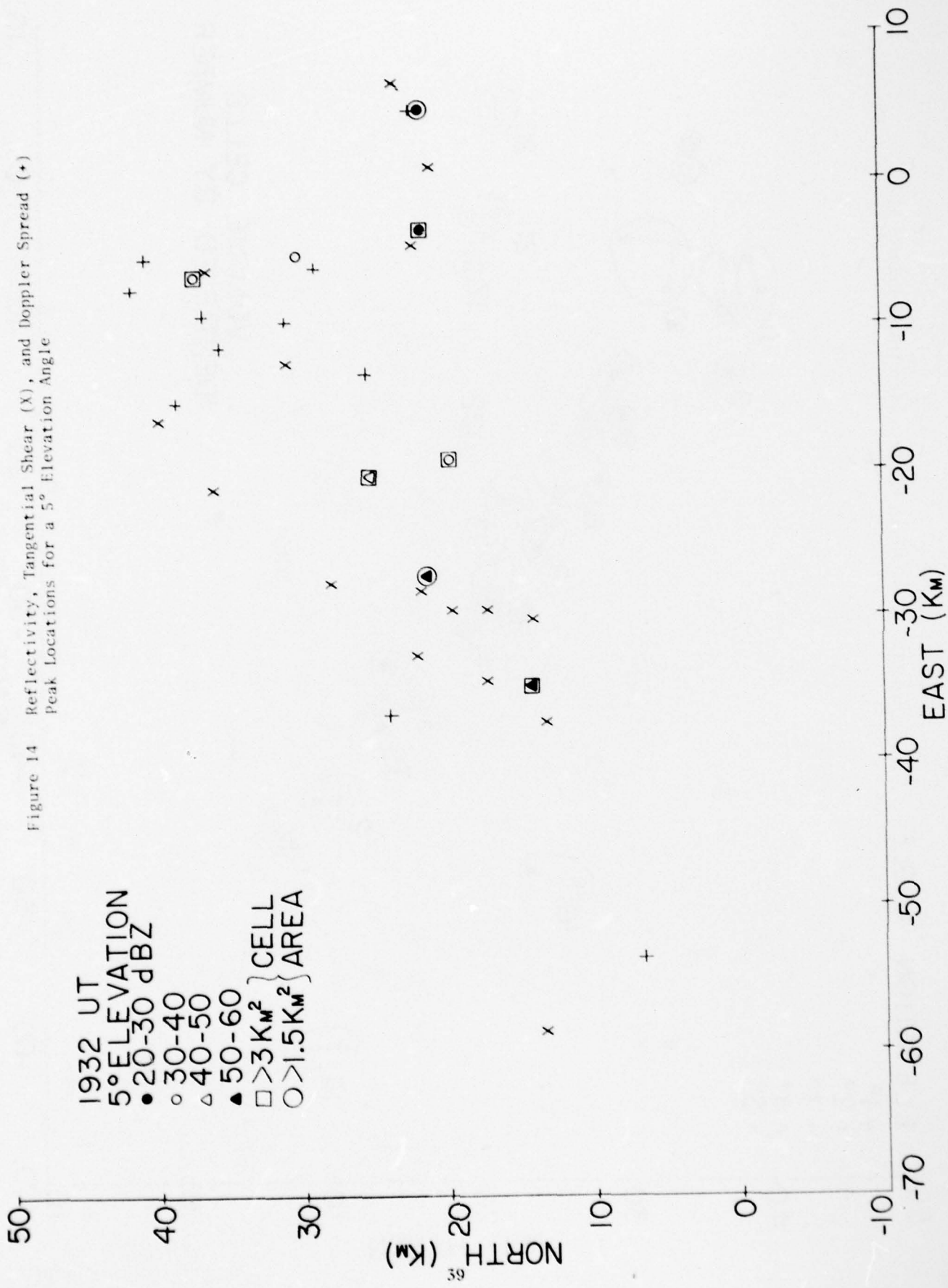


Figure 14 Reflectivity, Tangential Shear (X), and Doppler Spread (+)
Peak Locations for a 5° Elevation Angle

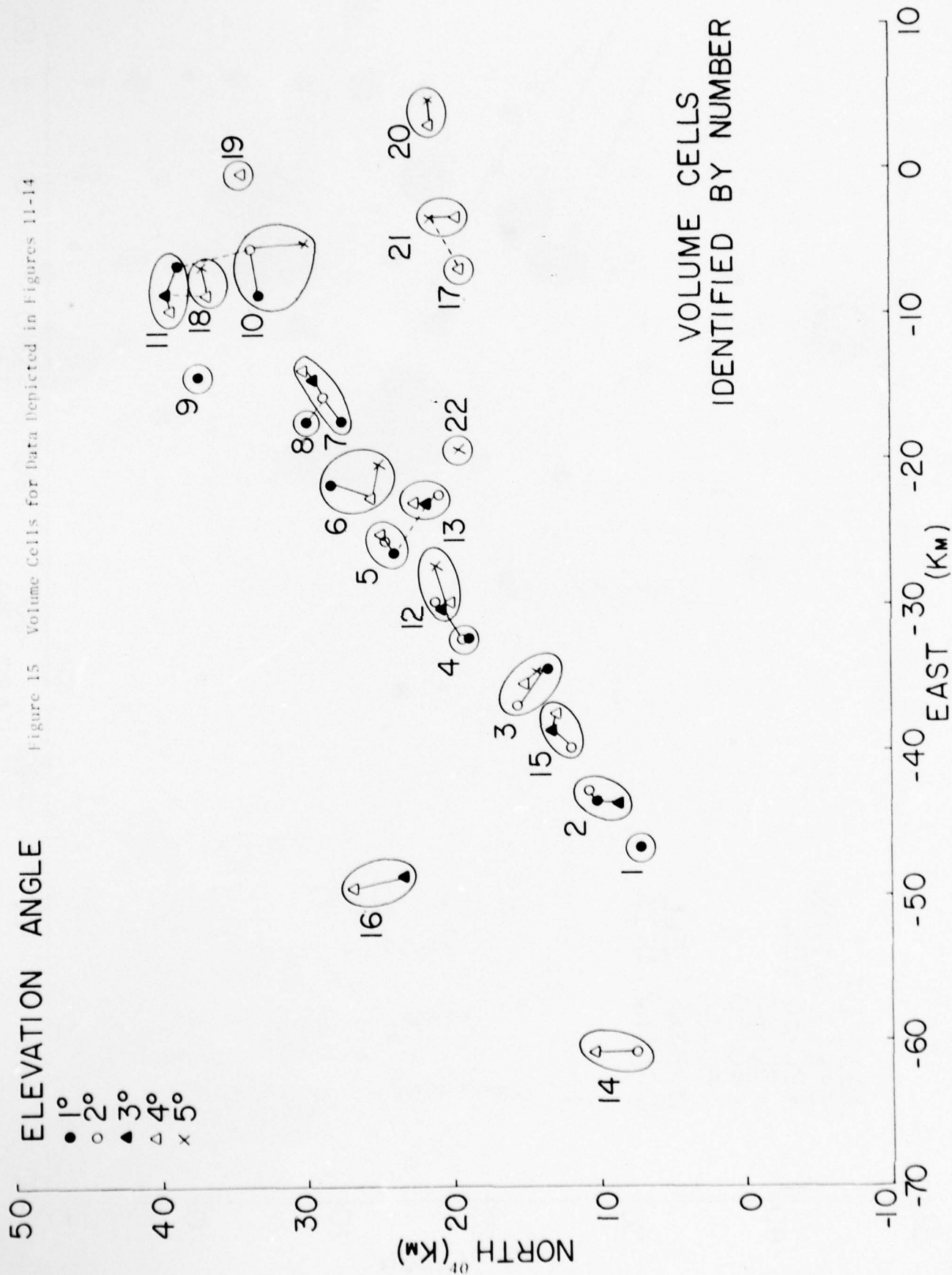


TABLE 2
VOLUME CELL ATTRIBUTES

ID*	X	Y	H _p	Z _p	H _b	H _T	ΔH	Δp	Volume
1	-46.8	7.3	0.9	39.9	0.9	0.9	0.5	4.0	2.0
2	-43.8	10.3	1.7	49.0	1.1	1.8	0.7	1.5	1.1
3	-34.4	13.7	3.4	54.9	2.9	-	-	3.5	-
4	-32.3	19.1	1.4	53.2	0.9	1.4	0.5	1.5	0.8
5	-26.4	24.1	2.5	52.9	1.0	2.4	1.4	5.4	7.6
6	-21.8	28.5	2.5	49.5	1.9	-	-	3.5	-
7	-17.4	27.8	2.4	47.8	0.7	2.4	1.7	3.2	5.4
8	-17.2	30.1	0.7	40.9	0.7	0.7	0.5	3.9	2.0
9	-14.2	37.5	0.8	33.0	0.8	0.8	0.5	4.4	2.2
10	- 8.9	33.1	2.7	30.7	1.8	-	-	1.4	-
11	- 6.8	38.8	2.2	31.9	0.8	2.9	2.1	2.0	4.2
12	-29.8	21.3	2.4	55.3	1.4	-	-	3.5	-
13	-22.4	21.1	2.3	44.6	1.1	2.3	1.2	1.4	1.7
14	-60.9	7.6	2.4	29.1	2.4	3.6	1.2	1.9	2.3
15	-39.9	12.0	2.2	53.6	1.7	2.8	1.1	1.2	1.4
16	-48.7	23.4	3.0	25.7	3.0	4.0	1.0	12.9	12.9
17	- 6.9	19.8	1.5	21.9	1.5	1.5	0.5	3.4	1.7
18	- 8.5	36.5	3.4	31.0	2.7	-	-	1.9	-
19	- 0.0	34.2	2.5	23.8	2.5	2.5	0.5	1.0	0.5
20	3.4	21.7	2.0	22.4	1.6	-	-	9.0	-
21	- 3.1	19.9	1.9	22.5	1.4	-	-	12.4	-
22	-19.3	-19.8	2.5	39.1	2.5	-	-	1.0	-

*See Figure 15

6. RECOMMENDATIONS

6.1 Parameter Optimization

A set of computer programs has been generated to provide an automatic means for the extraction of information from large volumes of radar data. The programs are written to be as general as possible to enable rapid changes in processing parameters. As indicated in Section 5, the optimum values for these parameters are not known and must be determined. It is expected that the parameters should change from one radar system to the next depending principally on the resolution volume and number of independent samples per resolution element. The first problem to be considered in the use of this set of programs is the optimization of parameters. This can only be done by processing a relatively large number of radar scans for different rain conditions.

Ideally, auxiliary data should be available to provide a standard of comparison for the output from the program. Many case studies such as the one reported in Section 5.1 should be performed to obtain the raw contour data to provide a comparison standard. For use in detecting severe weather events, auxiliary data on the severe events are also required.

6.2 Real Time Processing

The programs, although general in nature, were written with the ultimate goal of use in a real time processor. After the analysis for parameter optimization has been completed, specialization to a real time processor may be accomplished. Real-time processing requires the minimization of computer storage and operating time. Major steps can be made in this direction by increasing the resolution element area for processing (averaging over ~ 1 km in range as recommended in Section 5.1) and by reducing the number of peak detection operations. The latter can be accomplished by processing either tangential shear or Doppler spread data but not both as is currently done. Another time saving step is to reduce the volume of output by not preparing the fixed level contour plotting displays in the computer but doing the fixed contouring in the color display processor as is currently done for the output of digital integrators.

Preprocessing of the data for calibration, velocity ambiguity resolution, and conversion from variance to velocity spread will also save some time.

Current running time for reflectivity processing only but including fixed contour generation for display is 2 minutes per azimuth scan. By just doing the preprocessing, the running time could be reduced by more than a factor of two. The other reductions recommended above plus internal programming changes to reduce the use of indirect array addressing should result in a program that will do at least two data fields, reflectivity and tangential shear or Doppler spread, in real time (30 seconds per scan).

6.3 Spatial Analysis of Cell Development

The initial considerations of the forecast of new cell site locations indicates that improvements should be possible if attention is focused on the structure or organization of the cell location patterns. Processing to date has used the determination of nearest neighbor distances to obtain information about cell spacings. The nearest neighbor distances provide estimates of the locations of secondary maxima in the spatial correlation function for cell locations. Information on structure can better be obtained from more refined correlation function (or spatial power spectra) of cell location. These analyses should be conducted using a much larger data sample preferably for a number of different locations and storm types.

6.4 Morphological and Climatological Analysis

The programs described above are used to extract the significant information from a large volume of radar data. The result is still a formidable data set comprised of a number of lists of volume cell attributes for each scan, storm, and day. These data must in turn be reduced to a manageable set to describe the morphology of cell development. This analysis must be performed before any meaningful cell forecast procedures can be developed and tested. The analysis entails both the construction of new programs and the processing of large volumes of data.

REFERENCES

- Crane, R.K. (1976): "Radar Detection of Thunderstorm Hazards for Air Traffic Control Vol. I Storm Detection", Project Report ATC-67, Vol. I, MIT Lincoln Laboratory, Lexington, Massachusetts.
- Crane, R.K. (1977): "Parameterization of Weather Radar Data for Use in the Prediction of Storm Motion and Development", Final Report, Contract No. F19628-76-C-0264, Environmental Research & Technology, Inc.; AFGL-TR-77-0216, Air Force Geophysics Laboratory, Hanscom Air Force Base, Massachusetts.

ACKNOWLEDGEMENTS

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APPENDIX A

CELL DETECTION AND TRACKING PROGRAM INSTRUCTIONS FOR OPERATION

A.1 Description of Input and Output

Program input and output are depicted in Figure A1. The tape input format is given in Table A1. The control cards are discussed in section A2. The program produces (a) tapes of computed attributes for input to a second program for computing volume scans; (b) a plot tape is generated that can be stored for input to another program "EXPAND" which is a general purpose plotting package for plotting the fixed contours, centroids, cell identification and peak locations expanded over selected areas; (c) B-scan maps are also produced as an option; and (d) at the completion of a scan the program will print out fixed contour attributes, peak detected cell attributes and tangential shear maxima attributes. All of the attributes printed have identifiers which can be associated with the identifiers displayed on the expanded plots.

A.2 Control Card Format

Control card input to the program is NAMELIST input which allows certain parameters in the program to default or to be set to different values. The variable names, type (LOGICAL L, INTEGER I, and REAL R), dimension, default value and their meanings are listed in Table A2.

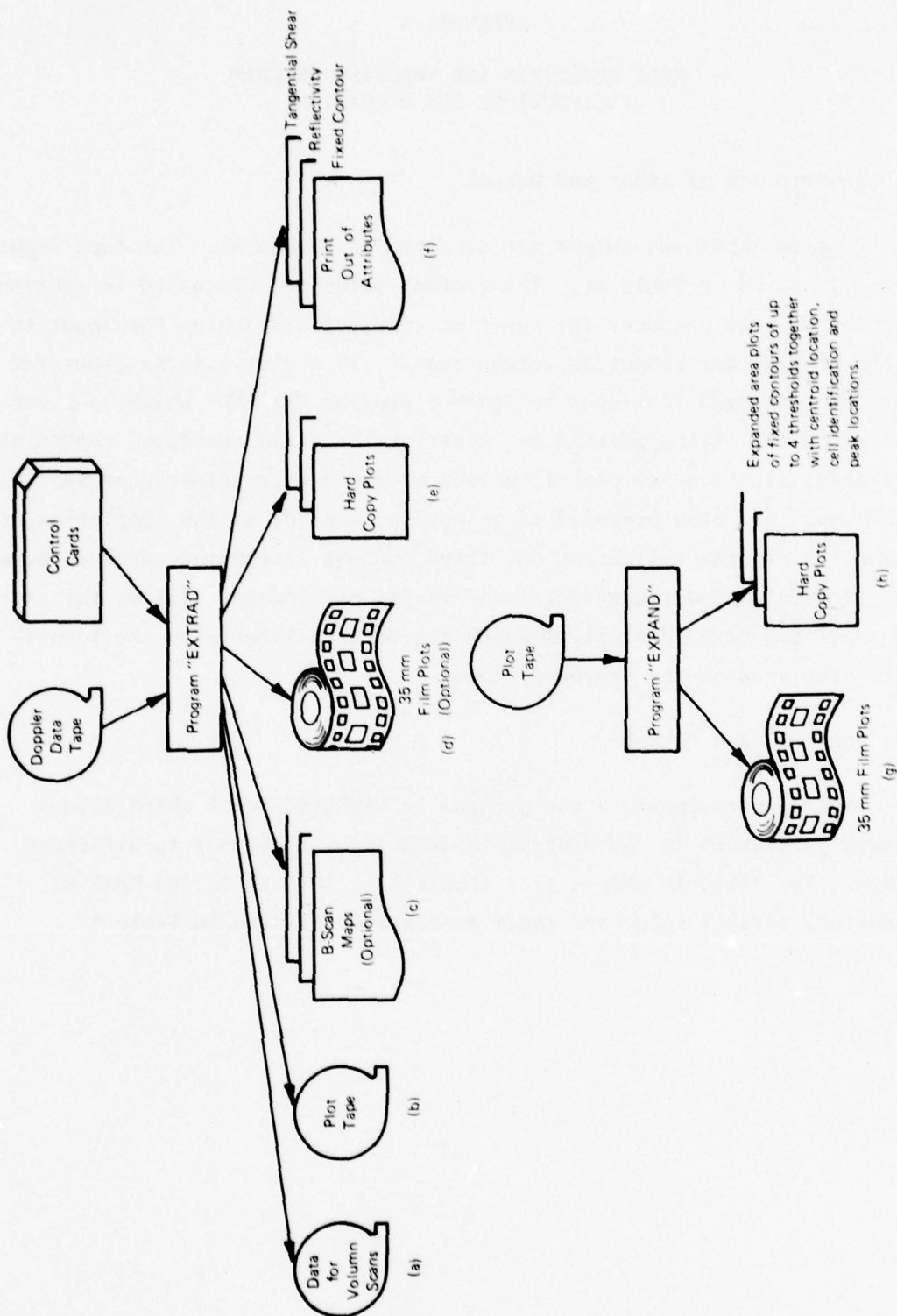


Figure A1 EXTRAD Products

Ancillary Data												12 Bit Word Position
Day	211	210	29	28	27	26	25	24	23	22	21	20
800	400	200	100	20	10	8	4	2	1	8	4	2
Hour				20	10	8	4	2	1			
Min			40	20	10	8	4	2	1			
Sec							40	20	10	8	4	2
Status			T ₁	T ₀	SF ₁	SF ₀	DD	1)NRC ₁	1)NRC ₀			1
A												
*PRF	PRF ₁₁	PRF ₁₀	PRF ₉	PRF ₈	PRF ₇	PRF ₆	PRF ₅	PRF ₄	PRF ₃	PRF ₂	PRF ₁	PRF ₀
Azimuth	AZ ₁₁	AZ ₁₀	AZ ₉	AZ ₈	AZ ₇	AZ ₆	AZ ₅	AZ ₄	AZ ₃	AZ ₂	AZ ₁	AZ ₀
Spare												
Spare												
Elevation	EL ₁₁	EL ₁₀	EL ₉	EL ₈	EL ₇	EL ₆	EL ₅	EL ₄	EL ₃	EL ₂	EL ₁	EL ₀
Spare												
Spare												
Mean	5)M ₁₁	5)M ₁₀	M ₉	M ₈	M ₇	M ₆	M ₅	M ₄	M ₃	M ₂	M ₁	M ₀
Variance	5)V ₈	V ₇	V ₆	V ₅	V ₄	V ₃	V ₂	V ₁	2)V ₀			
Power	6)P ₈	P ₇	P ₆	P ₅	P ₄	P ₃	P ₂	P ₁	2)P ₀			

Repeated 256 times**

1) Number Range Cells

256 0 0

512 0 1

768 1 0

1024 1 1

Subframe

SF₁ SF₀

ALT 0 0

ALL 1 1

0 0 1

1 0 0

1 1 1

Cell Width

0.5 μ s

1 μ s

2 μ s

Frequency of Dump Pulses DD

ALT 0

ALL 1

Least Significant Bit

Not Included in Parity

Sign

Parity

1 physical record = 158 sixty bit words

* If any group A bit = 1 and any group B bit = 1: PRF = 394

If A has 1 bit and B has 3 bits: PRF = 794

If A has 3 or more and B has 1 or less: PRF = 1613

If A has 3 or more and B has 3 or more: PRF = 3333

If A has 2 bits or B has 2 bits: PRF = Previous PRF

If all zero for A and B groups: use an input PRF

** First cell is the 21st twelve bit data word.

TABLE A1

TABLE A2

CARD FORMAT FOR PROGRAM EXTRAD

Reads in program parameters via NAMELIST format.

NAMELIST VARIABLES: (Level 780415)

<u>NAME</u>	<u>TYPE</u>	<u>DIMENSION</u>	<u>DEFAULT</u>	<u>MEANING</u>
PRINT1	L	1	FALSE	Unused.
PRINT2	L	1	FALSE	If .TRUE. print B-scan maps of mean and variance.
PRINT3	L	1	FALSE	If .TRUE. print B-scan maps of dBz.
PRINT4	L	1	FALSE	Unused.
ICODES	I	36	Blank thru Z then 1 thru 9.	Codes for representing dBz categories for B-scan map output.
A1	R	1	.13779	In the linear equation $y = mx + b$ for computing coded dBz for B-scans, A1 = M and B1 = b.
B1	R	1	1.5	
A2	\$	1	.017	Unused.
B2	R	1	18.6	Unused.
CONTRZ	L	1	TRUE	If FALSE, do not process peak cell attributes.
CONTRV	L	1	TRUE	If FALSE, do not process reflectivity, shear, & spread.
CONTRS	L	1	TRUE	If FALSE, do not process shear and spread.
NFILE	I	1	0	Number of files on tape to skip before processing.
NUMF	I	1	1	Number of files on tape to process.
AC	R	4	-107.7, +1.97, -0.94, +.0018	Calibration coefficients for computing DBM below a threshold XCUT. (see XCUT)

<u>NAME</u>	<u>TYPE</u>	<u>DIMENSION</u>	<u>DEFAULT</u>	<u>MEANING</u>
COPLLOT	L	1	FALSE	If TRUE, output a tape for plotting.
VOLTAP	L	1	TRUE	If FALSE, do not output an attribute tape.
CALM	R	1	.332	In the calibration equation for DBM $y = mx+b$, CALM = M & CALB = b.
CALB	R	1	-98.3	
XCUT	R	1	10.0	Threshold value that determines which equation to use for calibration. (linear or non-linear)
CK	R	1	10.0	In the equation for computing dBz, $K+P+20\text{ALOG}_{10}(S(I-.5))$ K = CK.
ZMAX	R	1	0.0	Not currently used.
VMAX	R	1	0.0	Not currently used.
NREC	I	1	1	Not currently used.
NUMR	I	1	999	Number of radials to be processed. Use default value when doing full scan.
IRUN	I	1	0	Run number chosen by user.
INC	I	1	0	Not currently used.
STARTR	R	1	0.0	Where along a radial in kilometers processing is to start.
STOPR	R	1	300.0	Where along a radial in kilometers processing is to stop.
INPRF	I	1	3333	Value of PRF (Pulse Repetition Frequency) to be used when PRF cannot be obtained from the data tape.
SCALE	R	1	1.0	Scale factor for drawing fixed contours.
AE	R	1	1.21	Constant for computing heights of cells.
AA	R	1	300	Constant for computing rain rate.
BB	R	1	1.5	Exponent for computing rain rate.

<u>NAME</u>	<u>TYPE</u>	<u>DIMENSION</u>	<u>DEFAULT</u>	<u>MEANING</u>
X1	R	1	0.0	Frame size coordinates for fixed contour plotting. Less than or equal to 8 inches.
X2	R	1	8.0	Same as above.
Y1	R	1	0.0	Same as above.
Y2	R	1	8.0	Same as above.
TV	I	1	35	Mean wind velocity in a fixed echo contour is not computed for dBz greater than this value.
TSV	R	1	10 ⁶	Not currently used.
LDV	I	1	3	Cell detection threshold for reflectance peaks.
LTV	I	1	3	Cell detection threshold for velocity peaks.
LSV	I	1	3	Cell detection threshold for shear peaks.
ICOMP	I	1	6	Data compression factor. (range integration)
VMIN	R	1	0.0	Unused.
SVMIN	R	1	0.0	Unused.
AREAMN	R	1	1.0	Any completed contour having an area less than AREAMN will be ignored but is plotted if a fixed contour.
WAVEL	R	1	0.0542	Radar wavelength in meters.
VQUANT	R	1	10.0	Tangential shear quantization step (m/s/km) ⁻¹ .
SQUANT	R	1	2.0	Doppler spread quantization step (m/s) ⁻¹ .
RQUANT	R	1	1.0	Reflectivity quantization steps (in dB ⁻¹).
DAZM	R	1	1.0	Beam width (degrees).

<u>NAME</u>	<u>TYPE</u>	<u>DIMENSION</u>	<u>DEFAULT</u>	<u>MEANING</u>
ESTART	R	1	(1.5°)	Elevation start angle (degrees).
DELT	R	1	(.5°)	Delta elevation angle (degrees) defining next scan.

APPENDIX B

PLOTTING PROGRAM 'EXPAND' (VERSION 1.0)

B.1 Description of Input and Output

Program EXPAND utilizes the plot tape generated by program 'EXTRAD' as input to generate not only full scan plots of fixed contours and their centroids but on option will expand and plot certain areas of interest. Also on option, it will plot out locations of centroids of fixed contours, peak detected cells, Doppler spread and tangential shear locals. These plotting options apply to full scan plots as well as expanded plots.

The plots are generated on the CALCOMP ink pen drum plotter. The X axis are labeled negative kilometers west of the radar and positive east. Y axis are labeled negative kilometers south of the radar and positive north. The date and elevation angle are also annotated.

B.2 Control Card Format

Control card input to the program is NAMELIST input which allows certain parameters to default or to be set to different values. The variable names, type, dimension, default and meaning are listed in Table B1.

It is suggested that program EXPAND generate full scan plots of fixed contours from the entire EXTRAD tape first before generating expanded areas of view. This allows one to examine exactly what each scan contains and where expansion would be of interest. One set of NAMELIST input cards are needed for each scan. If, for example, it is desired to go into the third scan on tape, three NAMELIST set ups must occur.

TABLE B1

CARD FORMAT FOR PROGRAM EXPAND
 READS IN PROGRAM PARAMETERS VIA NAMELIST INPUT

NAMELIST VARIABLES:

<u>NAME</u>	<u>TYPE</u>	<u>DIMENSION</u>	<u>DEFAULT</u>	<u>MEANING</u>
IPLT	L	4		
IPLT(1)	L		.FALSE.	If .TRUE. plot a dot to locate peak detected cells.
IPLT(2)	L		.FALSE.	If .TRUE. plot a C to locate fix contour centroids.
IPLT(3)	L		.FALSE.	If .TRUE. plot a + to locate Doppler spread.
IPLT(4)	L		.FALSE.	If .TRUE. plot an X to locate tangential shear.
Z1	L	1	.TRUE.	Plot fix contours for first level contour.
Z2	L	1	.TRUE.	Plot fix contours for second level contour.
Z3	L	1	.TRUE.	Always set to .FALSE.
Z4	L	1	.TRUE.	Always set to .FALSE.
LS	L	1	.FALSE.	When .TRUE. expanded area plots are requested. When .FALSE. draw full scan only.
XK1	R	1	-320.0	Western plot area limit (km).
XK2	R	1	320.0	Eastern plot area limit (km).
YK1	R	1	-320.0	Southern plot area limit (km).
YK2	R	1	320.0	Northern plot area limit (km).
LK	L	1	.FALSE.	If .TRUE. plot centroids of given areas.

*Note: Expanded plots will always square off any rectangular area request to the largest axis requested.

APPENDIX C

TRACKING PROGRAM (ASOCCL)

C.1 Description of Input and Output

The input tape is the tape produced by program "EXTRAD". This program takes the cell attributes and associate cells for tracking volume cells. The output listing includes the location of volume cells and the updated cell ID.

C.2 Control Card Format

Control card input to the program is NAMELIST input which allows certain parameters in the program to default or to be set to different values. The variable names, type (LOGICAL L, INTEGER I, and REAL R), dimensions, default values and their meanings are listed in Table C1.

TABLE C1

CARD FORMAT FOR PROGRAM ASOCCL

Reads in Program Parameters via NAMELIST Format

NAMELIST VARIABLES:

<u>NAME</u>	<u>TYPE</u>	<u>DIMENSION</u>	<u>DEFAULT</u>	<u>MEANING</u>
PR1	L	1	FALSE	When .TRUE. program prints out the input attributes data.
PR2	L	1	FALSE	When .TRUE. program prints out the initial volume cell attributes and the total number of cells.
PR3	L	1	FALSE	When .TRUE. program prints out the associated update cell attributes and the total number of associated cells.
PR4	L	1	FALSE	Currently unused.
IDEV1	I	1	1	Input tape or file.
IDEV2	I	1	1	Currently unused.
ISTOP	I	1	1	Stop program, when "0" continue processing.

APPENDIX D

COMPUTER PROGRAM LISTINGS
AND SAMPLE OUTPUT

D-3

6	DATA ZMAX/0.0/,VMAX/0.0/,AC/-107.76555,1.9767838,-.094297528,.0801	TEST	32
68	18226317,CALH/0.332/,CAL/3/-36.3/,XCUT/10.0/	EXTRAD	92
	DATA TITLE/PROGRAM,7H EXTRAD,1M ,1M ,1M /	EXTRAD	93
	DATA IRUN/0/,NPAGE/0/,LCODE/162/,VERS/2.0/,LEVEL/788501/	EXTRAD	94
	DATA IMPRF/794/	EL	5
	DATA CK/10.0/,INC/0/	EL	7
65	DATA SCALE/1.0/,LDW/3/,-10/3/,LSV/3/	EL	8
	DATA TERR/0/	TEST	33
	DATA WAVEL/8.0542/	EXTRAD	99
	DATA VQUANT/10.0/,SQUANT/6.8/,RQUANT/1.0/	TEST	34
70	DATA M10F/120/,IAT/5/,N2A/4/,IENAX/22/,NFC/2/	EL	9
	DATA KRX/30/,JRX/0/50/,JMAX/50/,IAX/2650/,IWK/30/,KR/22/,	TEST	36
	IMJMX/24/,NCL/123/	TEST	37
	DATA M10Z/280/,MOP/97/,N13/778/,MUMAX/29/	TEST1	5
	DATA MUMAX/23/,MUV/7/,NSHAX/17/,MUS/5/	TEST	38
75	DATA ESTRT/1.57/DELT/57	TEST	40
	-----	EL	10
	-----	EXTRAD	102
	-----	EXTRAD	103
	END		


```

      JK=TL(I)+IX-1
      C PRESET PAIR RATE - 1 DBZ STEPS
      C
      DBZARY(I)=XU.**((DBZ-FLOAT(JK)-XU)
      C BUILD LINEAR Z TABLE
      C
      ZARY(I)=IC.**((FLOAT(JK)*QUANT/10.)
      10 CONTINUE
      IF (.NOT. COMPTO) GO TO 21
      11 SCALE=8.0/(V2-V1)
      IF ((V2-X1).GT.(V2-V1)) SCALE=8.0/(X2-X1)
      XMIN=SCALE*X1
      YMAX=SCALE*Y2
      YMIN=SCALE*Y1
      YMAX=SCALE*Y2
      21 IF (.NOT. PRINT2) GO TO 51
      C PRINT ICODES VALUES.
      C
      CALL PAGE
      31 WRITE (6,31)
      FORMAT (1M0,8X,13MCODE FOR MEAN,7X,5HVALUE,5X,12MCODE FOR VAR,7X,5
      1HVALUE/4BX,7HEND PRN)
      DO 41 I=1,36
      XA=(FLOAT(I)-81)/41
      IF (XA-1.0.) XA=0.
      XB=(FLOAT(I)-82)/42
      41 WRITE (6,51) ICODES(I),X9,ICODES(I),XA
      51 FORMAT (15X,A1,9X,F9.3,11X,A1,9X,F9.3)
      61 CONTINUE
      IF (.NOT. PRINT3) GO TO 101
      CALL PAGE
      71 WRITE (6,71)
      FORMAT (1M0,8X,13MCODE FOR DBZ,7X,5HVALUE)
      DO 81 I=1,36
      XA=(FLOAT(I)-81)/41
      IF (XA-1.0.) XA=0.
      81 WRITE (6,91) ICODES(I),XA
      91 FORMAT (15X,A1,9X,F9.3)
      101 CONTINUE
      RETURN
      111 WRITE (6,121)
      121 FORMAT (30H END OF FILE IN NAMELIST INPUT)
      STOP
      END
  
```

D-7

D-9

53	CONTINUE	EXTRAD	327
55	CONTINUE	EXTRAD	328
175	IF(N .LT. 155) GO TO 61	EXTRAD	329
		EXTRAD	330
	CLEAN OFF EXTRA BITS.	EXTRAD	331
		EXTRAD	332
		EXTRAD	333
		EXTRAD	334
		EXTRAD	335
		EXTRAD	336
		EXTRAD	337
		EXTRAD	338
		EXTRAD	339
		EXTRAD	340
		EXTRAD	401
		EXTRAD	402
		EXTRAD	403
		EXTRAD	404
		EXTRAD	405
		EXTRAD	406
		EXTRAD	407
		EXTRAD	408
		EXTRAD	409
		EXTRAD	410
		EXTRAD	411
		EXTRAD	412
		EXTRAD	413
		EXTRAD	414
		EXTRAD	415
		TEST2	21
200	IF(TMS .GT. NSF .AND. NRG .GE. NST.DR. AZ .EQ. AZMUTHNAST) GOTO 21	EXTRAD	417
	IF(TMS .GT. NSF .AND. NRG .GE. NST.DR. AZ .EQ. AZMUTHNAST) GOTO 21	EXTRAD	418
	IF(TMS .GT. NSF .AND. NRG .GE. NST.DR. AZ .EQ. AZMUTHNAST) GOTO 21	EXTRAD	419
	IF(TMS .GT. NSF .AND. NRG .GE. NST.DR. AZ .EQ. AZMUTHNAST) GOTO 21	EXTRAD	420
	IF(TMS .GT. NSF .AND. NRG .GE. NST.DR. AZ .EQ. AZMUTHNAST) GOTO 21	EXTRAD	421
	IF(TMS .GT. NSF .AND. NRG .GE. NST.DR. AZ .EQ. AZMUTHNAST) GOTO 21	EXTRAD	422
	IF(TMS .GT. NSF .AND. NRG .GE. NST.DR. AZ .EQ. AZMUTHNAST) GOTO 21	EXTRAD	423
	IF(TMS .GT. NSF .AND. NRG .GE. NST.DR. AZ .EQ. AZMUTHNAST) GOTO 21	EXTRAD	424
	IF(TMS .GT. NSF .AND. NRG .GE. NST.DR. AZ .EQ. AZMUTHNAST) GOTO 21	EXTRAD	425
	IF(TMS .GT. NSF .AND. NRG .GE. NST.DR. AZ .EQ. AZMUTHNAST) GOTO 21	EXTRAD	426
	IF(TMS .GT. NSF .AND. NRG .GE. NST.DR. AZ .EQ. AZMUTHNAST) GOTO 21	EXTRAD	427
	IF(TMS .GT. NSF .AND. NRG .GE. NST.DR. AZ .EQ. AZMUTHNAST) GOTO 21	EXTRAD	428
	IF(TMS .GT. NSF .AND. NRG .GE. NST.DR. AZ .EQ. AZMUTHNAST) GOTO 21	EXTRAD	429
	IF(TMS .GT. NSF .AND. NRG .GE. NST.DR. AZ .EQ. AZMUTHNAST) GOTO 21	EXTRAD	430
	IF(TMS .GT. NSF .AND. NRG .GE. NST.DR. AZ .EQ. AZMUTHNAST) GOTO 21	EXTRAD	431
	IF(TMS .GT. NSF .AND. NRG .GE. NST.DR. AZ .EQ. AZMUTHNAST) GOTO 21	EXTRAD	432
	IF(TMS .GT. NSF .AND. NRG .GE. NST.DR. AZ .EQ. AZMUTHNAST) GOTO 21	EXTRAD	433
	IF(TMS .GT. NSF .AND. NRG .GE. NST.DR. AZ .EQ. AZMUTHNAST) GOTO 21	EXTRAD	434
	IF(TMS .GT. NSF .AND. NRG .GE. NST.DR. AZ .EQ. AZMUTHNAST) GOTO 21	EXTRAD	435
	IF(TMS .GT. NSF .AND. NRG .GE. NST.DR. AZ .EQ. AZMUTHNAST) GOTO 21	EXTRAD	436
	IF(TMS .GT. NSF .AND. NRG .GE. NST.DR. AZ .EQ. AZMUTHNAST) GOTO 21	EXTRAD	437
	IF(TMS .GT. NSF .AND. NRG .GE. NST.DR. AZ .EQ. AZMUTHNAST) GOTO 21	EXTRAD	438
	IF(TMS .GT. NSF .AND. NRG .GE. NST.DR. AZ .EQ. AZMUTHNAST) GOTO 21	EXTRAD	439
	IF(TMS .GT. NSF .AND. NRG .GE. NST.DR. AZ .EQ. AZMUTHNAST) GOTO 21	EXTRAD	440
	IF(TMS .GT. NSF .AND. NRG .GE. NST.DR. AZ .EQ. AZMUTHNAST) GOTO 21	EXTRAD	441
	IF(TMS .GT. NSF .AND. NRG .GE. NST.DR. AZ .EQ. AZMUTHNAST) GOTO 21	EXTRAD	442
	IF(TMS .GT. NSF .AND. NRG .GE. NST.DR. AZ .EQ. AZMUTHNAST) GOTO 21	EXTRAD	443

```

C      FINISHED SCAN
230      122 ISCANF=+1
          GO TO 131
          TEST2 27
          EXTRAD 466
111      IEOP=1
          EXTRAD 467
121      ISCANF=-1
          EXTRAD 468
131      IF INA.LE.10)GO TO 132
          TEST1 18
          ISCANF=ISCANF
          TEST1 19
          ISCANF=0
          TEST1 20
          ELFV=ELEV+ELEVAT
          TEST2 26
          DELTAZ=ABS((AZMUTH(MINA)-AZMUTH(MNA-1)))**PPD
          TEST1 22
          CALL COMPTZ
          TEST1 23
          CALL CONTOP
          TEST1 24
          ISCANF=ISCANF
          TEST1 25
          ELFVAT=ELEV/MNA
          TEST1 25
          CALL CONTRZ
          TEST 77
          EXTRAD 455
132      REMIND 4
          EXTRAD 456
240      IF (COPLOT) WRITE(21)DAY,IM,MM,IEOD
          TEST2 29
          IF (IEOP.EQ.1) GO TO 181
          EXTRAD 457
          IF (MNA.GE.NUMR) RETURN
          EXTRAD 458
          GO TO 5
          EXTRAD 459
          WRITE (6,191)
          EXTRAD 460
          IF ILEFFILEV1
          EXTRAD 461
          IF (IFILE .LT. NUMR*NFIL) GO TO 2
          EXTRAD 462
          191  FORMAT (19H EOF REED ON UNIT 1)
          EXTRAD 463
          211  FORMAT (21H PAPITY ERR ON UNIT 1)
          EXTRAD 464
          221  RETURN
          EXTRAD 465
          END
          EXTRAD 466

```


D-12

115	C	COMPUTE V		EXTRAD	567
	C			EXTRAD	568
		IF (XABST(MVP(1,J)) -LT. VEL(MIN) M(JP)=8		EXTRAD	569
		IF (IABST(MVP(2,J)) -LT. VARMIN) M(JP)=0		EXTRAD	570
		IF (V(JP) -EQ. VEL(1)) GO TO 37		EXTRAD	571
120		M(4,1)=IF (INCOMFLOAT(MVP(1,J)))		EXTRAD	572
		IF (V(L -EQ. -999) VEL=V		EXTRAD	573
		IF (V(L -VL -GT. V(M) V(JP)=V(JP)-V(M)		EXTRAD	574
		IF (V(L-V(JP) -GT. V(M) V(JP)=V(JP)+V(M)		EXTRAD	575
		IF (V(L(JP) -EQ. -999 -OR. M(A -EQ. 1) GO TO 37		EXTRAD	576
125		IF (V(JP) -V(JP) -GT. V(M) V(JP)=V(JP)-V(M)		EXTRAD	577
		IF (V(L(JP) -V(JP) -GT. V(M) V(JP)=V(JP)+V(M)		EXTRAD	578
		V(M)=V(M) + V(JP)		EXTRAD	579
		V(S)=V(S)+1		EXTRAD	580
		GO TO 35		EXTRAD	581
130	37	IF (IUS -LE. 10) GO TO 33		EXTRAD	582
		V(M)=V(M)+V(S)		EXTRAD	583
		IF (I(A -EQ. 0) V(S) =V(M)		EXTRAD	584
		I(A =1		EXTRAD	585
	33	V(M) =0		EXTRAD	586
135		V(L)=V(JP)		EXTRAD	587
	35	IF (V(JP) -EQ. -999) GO TO 41		EXTRAD	588
		IF (MVP(2,J) -LT. 0 -OR. MVP(2,J) -GT. 5) GO TO 411		TEST1	40
		V(JP)=V(JP)+V(MVP(2,J)+1)		TEST1	41
140	411	IF (V(L(JP) -EQ. -999 -OR. M(A -EQ. 1) GO TO 41		TEST	95
		IF (V(L(JP) -EQ. -999 -OR. M(A -EQ. 1) GO TO 41		EXTRAD	592
		IF (V(L(JP) -EQ. -999 -OR. M(A -EQ. 1) GO TO 41		TEST1	42
	41	CONTINUE		EXTRAD	594
		DO 45 JP=3,N		EXTRAD	595
145		IF (V(JP) -EQ. -999 -OR. V(JP) -EQ. -999 -OR. V(JP)+1 -EQ. -999)		EXTRAD	596
	1	GO TO 45		EXTRAD	597
		V(M)=V(JP)+V(JP)-1/2		EXTRAD	598
		IF (V(JP) -I(MEAN -GT. V(M) V(JP)=V(JP)-V(M)		EXTRAD	599
		IF (V(MEAN-V(JP) -GT. V(M) V(JP)=V(JP)+V(M)		EXTRAD	600
150	45	CONTINUE		EXTRAD	601
		DO 51 J=1,NOL		EXTRAD	602
	51	V(JP)=V(J)		EXTRAD	603
		IF (IFLAG -EQ. 0 -OR. V(M) -GT. 70) RETURN		TEST1	43
		WRITE(6,308) M, N, (M(J), V(J), V(S(J), V(L(J), J=M, N)		EXTRAD	605
155	300	FORMAT 1X, 214, / (1X, 2015/)		EXTRAD	606
		RETURN		EXTRAD	607
		END		EXTRAD	608

D-15


```

C
IFLAG=0
IF (IFLAG.EQ.1) PRINT 7, (I(IX), IX=1, 173)
RANG=SCON/ICOMP*(RN(NRC+1)-.5)/4.
SCON=SCON/PIRE
RANG=RANG*CELTW(INTP+1)/1000.
FORMAT(11,2015)
IF (.NOT.PRINT3) GO TO 1
IF (IN.EQ.1) CALL PRANG
CALL PRN2(1)
1 CONTINUE
IF (IN4.EQ.1) WRITE(2) RN(NRC+1), CELTW(INTP+1), ELEVAT
KZND=KZMUTH(N8)
IF (IN4.EQ.1) GO TO 11
TEMP=KZMUTH(N4-1)
TEMP=TEMP*RPD
GO TO 61
C
C
C INITIALIZE.
11 TEMP=0.0
SL=SIN(ELEVAT*RPD)/1000.
CECOS(ELEVAT*RPD)**27A=76.731E8
MCEL=1
NMC=1
NMC=1
DO 312 J=1, MID
DO 313 K=1, NUP
313 OPTJ,K=0.0
DO 314 K=1, NUV
314 UV(J,K)=0.0
DO 315 K=1, NUS
315 USTJ,K=0.0
312 CONTINUE
DO 31 KEL,MIDF
OSI(K)=0.0
31 CONTINUE
DO 311 J=1, MCL
VSI(J)=VS(J)
311 SWITCH=VSI(J)
DO 32 J=1, NME
DO 32 L=1, NZH
DO 32 K=1, NZP
32 ZH(K,L,J)=0.0
DO 41 K=1, MIDF
DO 41 J=1, IAT
DO 41 L=1, MFC
41 ATR(J,K,L)=0.0
DO 51 K=1, MFC
DO 51 L=1, IENAY
CTR(L,K)=0.0
DO 51 J=1, NPA
51 ICL(J,L,K)=0
DO 52 J=1, MFC
52 VBNY(J)=0

```


400	IF (IATK(J,NUMPI).EQ.RKNIDU) IATP(J,NUMPI)=RKNIDY	TEST	162
	413 CONTINUE	EXTRAD	957
	IF (IATC(J).EQ.0) GO TO 416	EXTRAD	960
	IF (IATK(J,NUMPI).EQ.RKNIDU) IATP(J,NUMPI)=RKNIDY	TEST1	962
	414 CONTINUE	EXTRAD	962
405	IF (IATC(J).EQ.0) GO TO 4131	TEST1	76
	IF (IATP(J,NUMPI).EQ.RKNIDU) IATP(J,NUMPI)=RKNIDY	TEST1	77
	4131 CONTINUE	TEST1	78
410	DO 4161 J=1,NIC	TEST1	79
	IF (J.GT.NCCL.AND.J.LE.NCCL) GO TO 4211	TEST1	80
	IF (IUP(J,NUMPI).EQ.0) GO TO 415	TEST	166
	IF (IUP(J,NUMPI).EQ.RKNIDU) J(PJ,NUMPI)=RKNIDY	TEST	167
	415 CONTINUE	EXTRAD	966
	IF (IUP(J,NUMPI).EQ.0) GO TO 416	TEST	168
415	IF (IUP(J,NUMPI).EQ.RKNIDU) J(PJ,NUMPI)=RKNIDY	TEST	169
	416 CONTINUE	EXTRAD	970
415	IF (IUST(J,NUMPI).EQ.0) GO TO 4181	TEST	170
	IF (IUST(J,NUMPI).EQ.RKNIDU) J(SIJ,NUMPI)=RKNIDY	TEST	171
	4181 CONTINUE	EXTRAD	972
420	4211 IF (INFC.EQ.1) GO TO 421	TEST1	81
	DO 4201 LK=2,NFC	TEST1	82
	MIOPK=K001(K)	TEST2	63
	MIOPK=MAX(MIOPK,NIOPK)	TEST2	64
	DO 4201 JK=1,NIOFK	TEST2	65
	IF (IUSDT(JK,LK).EQ.0) GO TO 4201	TEST1	84
425	IF (IABS(IATP(J,K,LK)).EQ.RKNIDU) IATP(J,K,LK)=SIGN(RKNIDY,IATP(J,K,LK))	TEST2	66
	X IATP(J,K,LK)	TEST2	67
	4201 CONTINUE	TEST1	86
	421 CONTINUE	EXTRAD	971
430	DS111(D)=DS111(D)+DS1(KID)	EXTRAD	972
	DS1(KID)=0	EX1	42
	GO TO 381	EXTRAD	973
	3811 RKNIDU=ABS(CTR(REVENT,K1))	TEST2	68
	MIOPK=K001(K)	TEST2	69
435	DO 3812 JK=1,NIOFK	TEST2	70
	IF (IABS(IATP(J,K,K1)).EQ.RKNIDU) GO TO 3813	TEST2	71
	3812 CONTINUE	TEST2	72
	GO TO 381	TEST2	73
	3813 KID=JK	TEST2	74
	GO TO 3814	TEST2	75
440	441 IF (REVENT.GT.IEVT) GO TO 451	TEST1	87
	IF (IIG(I1,REVENT+1,K1).GT.I3(I2,IEVENT,K1)) GO TO 451	TEST1	88
	C	EXTRAD	976
	C	EXTRAD	977
	C	EXTRAD	978
445	IF (I.MOT.COPLCT) GO TO 6001	TEST	172
	X=FCURT(IIG(I2,REVENT,K1))-I.0	EXTRAD	979
	R=SCONC*X	TEST	173
	X=SCALE*(R+SINA*4.-0)	EXTRAD	981
	Y=SCALE*(R+COISA*4.-0)	EXTRAD	982
450	WRITE(21X,Y,TPU)	EXTRAD	984
	X=FLOAT(IIG(I1,REVENT+1,K1))-1.0	EXTRAD	985
	R=SCONC*X	TEST1	89
	X=SCALE*(R+SINA*4.-0)	EXTRAD	987
	Y=SCALE*(R+COISA*4.-0)	EXTRAD	988
455	WRITE(21X,Y,IPD)	EXTRAD	990
	6001 REVENT=REVENT+1	TEST	175

515	C	STRAIGHT LINE IN IC.		EXTRAD 1059
521	C	IF IC(1,KEVENT,K).EQ.0) 50 TO 562	EXTRAD 1060	
		DO 5522 I10=1,N10F	EXTRAD 1061	
		IF I10SL0T(I10,K).NE.016J TO 5522	TEST 1065	
		I00=I10	EXTRAD 1064	
520		IC(INPA,KEVENT,K)=I10	TEST 1066	
		IF (K.NE.1) GO TO 5521	TEST 1067	
		I0SL0T(I10,K)=KN10	EXTRAD 1065	
		KN10=K10+1	EXTRAD 1067	
5521		IF I=IC(13,KEVENT,K)	TEST 1088	
525		I101=I(CNPA,IE,1,1)	TEST1 104	
		I0SL0T(I10,K)=I0SL0T(I101,1)	TEST 190	
		GO TO 5523	TEST1 105	
5522		CONTINUE	EXTRAD 1072	
C** NOTE			EXTRAD 1073	
530	C**	WHEN ALL I0'S ARE USED,	EXTRAD 1076	
		IC(I010F,K) WILL 30K0=N ALL OTHER CELLS	TEST 191	
		IC(INPA,KEVENT,K)=I10F	TEST1 106	
		IF (K.NE.1) GO TO 5524	TEST2 77	
		KN10=KN10+1	TEST2 78	
535		I0SL0T(I10,K)=KN10	TEST2 79	
5524		I10F=I10F	TEST2 80	
		I00=I10	TEST2 81	
		IERR=4	EXTRAD 1077	
5523		K00(K)=MAX0(K00(K),I00)	TEST2 82	
540		I10=I00	TEST2 83	
524		IF (1-NOT,C0PLOT,0-N4,E0,1) 50 TO 527	TEST2 84	
		Z=FL0R(I010F,KEVENT,K)/I10	TEST 193	
		Z=SC0NC*Y	TEST 194	
545		X=SCALE*(R*SIN(A+4,0)	EXTRAD 1084	
		Y=SCALE*(R*C0S(A+4,0)	EXTRAD 1065	
		WRITE(21,X,Y,I10	EXTRAD 1087	
		X=FL0A(I10(2,KEVENT,K))-1.0	EXTRAD 1088	
		Z=SC0NC*Y	TEST 195	
550		X=SCALE*(R*SIN(A+4,0)	EXTRAD 1090	
		Y=SCALE*(R*C0S(A+4,0)	EXTRAD 1091	
		WRITE(21,X,Y,I10	EXTRAD 1093	
527		IF (I=SCANF.NE.0) 50 TO 531	TEST2 85	
		ATRI(1,I00,K)=DELTAZ*CI(1,KEVENT,K)*ATRI(1,I00,K)	TEST2 86	
		ATRI(2,I00,K)=DELTAZ*CI(2,KEVENT,K)*ATRI(2,I00,K)	TEST2 87	
555		ATRI(3,I00,K)=SIN(A*DELTAZ*CI(3,KEVENT,K)*ATRI(3,I00,K)	TEST2 88	
		ATRI(4,I00,K)=C0S(A*DELTAZ*CI(3,KEVENT,K)*ATRI(4,I00,K)	TEST2 89	
531		IE=I10(13,KEVENT,K)	EXTRAD 1102	
		I101=I(CNPA,IE,1,1)	EXTRAD 1103	
		ATRI(1,I00,K)=I0SL0T(I101,1)	EXTRAD 1104	
560		IF (IN4.EQ.1) ATRI(1,I00,K)=ABS(ATTRI(1,I00,K))	EXTRAD 1105	
		IF (IC(1,KEVENT,K).LT.1M4,0,X,IC(2,KEVENT,K).GE.1M4) ATRI(1,I00,K)=--	TEST2 90	
		1ABS(ATTRI(1,I00,K))	EXTRAD 1107	
		IF (K.NE.1) GO TO 561	EXTRAD 1108	
		DO 551 I=1,NZ	EXTRAD 1109	
		IF (I2(I2,I14,KEVENT),LE.0,1) 50 TO 551	EXTRAD 1110	
565		IF (VI(13,I14,KEVENT).EQ.0,1) 50 TO 561	EXTRAD 1111	
		ZH(1,I14,NNE)=VI(1,I14,KEVENT)	EXTRAD 1112	
		ZH(2,I14,NNE)=VI(2,I14,KEVENT)	EXTRAD 1113	
		ZH(3,I14,NNE)=SIN(A*VI(1,I14,KEVENT)	EXTRAD 1114	
570		ZH(4,I14,NNE)=C0S(A*VI(1,I14,KEVENT)	EXTRAD 1115	

[illegible]


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180 LOCATION,IX,CHAREA,5X,8HVELOCITY,2X,6HRAIDIAL,5X,18HANGENTIAL, TEST1 147
22X,6HRAIDIAL,4X,5HFIXED,7,6X,12HREFLECTIVITY,3X,6HAREA,3X,6HAEAST, TEST1 148
32X,5HNOPT,2X,5HFRANGE,2X,12HRESOLUTION,2X,5HSPREAD,5X,5HSHRINK,5X, TEST1 149
45HSHRINK,7X,6HVELOCITY,2X,7HCONTOUR,7,2X,2HID,5X,5HIDB21,5X, TEST1 150
57HIDB21,2X,5HSHRINK,2X,5HSHRINK,2X,5HSHRINK,2X,5HSHRINK,2X,5HSHRINK,2X, TEST1 151
65X,6H(M/S/KM),2X,6H(M/S/KM),4X,5H(M/S),5X,9HREFERENCE) TEST1 152
705 IF(.NOT.VOLTACTION) GO TO 6021
715 IF(.NOT.VOLTACTION) GO TO 6021
725 IF(.NOT.VOLTACTION) GO TO 6021
735 IF(.NOT.VOLTACTION) GO TO 6021
745 IF(.NOT.VOLTACTION) GO TO 6021
755 IF(.NOT.VOLTACTION) GO TO 6021
765 IF(.NOT.VOLTACTION) GO TO 6021
775 IF(.NOT.VOLTACTION) GO TO 6021
785 IF(.NOT.VOLTACTION) GO TO 6021
795 IF(.NOT.VOLTACTION) GO TO 6021
805 IF(.NOT.VOLTACTION) GO TO 6021
815 IF(.NOT.VOLTACTION) GO TO 6021
825 IF(.NOT.VOLTACTION) GO TO 6021
835 IF(.NOT.VOLTACTION) GO TO 6021
845 IF(.NOT.VOLTACTION) GO TO 6021
855 IF(.NOT.VOLTACTION) GO TO 6021
865 IF(.NOT.VOLTACTION) GO TO 6021
875 IF(.NOT.VOLTACTION) GO TO 6021
885 IF(.NOT.VOLTACTION) GO TO 6021
895 IF(.NOT.VOLTACTION) GO TO 6021
905 IF(.NOT.VOLTACTION) GO TO 6021
915 IF(.NOT.VOLTACTION) GO TO 6021
925 IF(.NOT.VOLTACTION) GO TO 6021
935 IF(.NOT.VOLTACTION) GO TO 6021
945 IF(.NOT.VOLTACTION) GO TO 6021
955 IF(.NOT.VOLTACTION) GO TO 6021
965 IF(.NOT.VOLTACTION) GO TO 6021
975 IF(.NOT.VOLTACTION) GO TO 6021
985 IF(.NOT.VOLTACTION) GO TO 6021
995 IF(.NOT.VOLTACTION) GO TO 6021

```



```

915      USIN,3)=USIN,3)/USIN,2)/I. DE03
      USIN,2)=USIN,2)/USIN,1)/SQUANT
      USIN,1)=USIN,1)/DELZ/I. DE06
      PBAR=SQRT(USIN,3)*USIN,3)+USIN,4)*USIN,4))
      PCELS=USIN,1)/PBAR*DE02
      IUS=USIN,5)
      WRITE(721) N,USIN,2),JSIN,1),USIN,3),USIN,4),PBAR,PCELS,IUS
920      721 FORMAT (I4,F7.1,5X,F6.1,2A,F6.1,5X,F7.1,2X,F7.1,5X,I4)
      IF (XLTAP) WRITE(3)USIN,2),USIN,1),USIN,3),JSIN,4),IUS
      IF (.NOT. COPILOT) GO TO 944
      XREG=USIN,3)/PANG*4.0
      YREG=USIN,4)/PANG*4.0
      IPU=ISSPEN
      WRITE(2) XREG, YREG, IPU
925      944 CONTINUE
      1413 WRITE(6,950)KNID,NMR,NM,NMS
930      950 FORMAT(10I5,10F5.2)
      ISCANF=0
      IF (PRINT2) CALL PRN2(2)
      RETURN
      END

```


D-32


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102=1*(LNB-I)*LM
IF (INA.NE.-1.OR.ISCANF.NE.0) GO TO 2109
C
C      ZERO ARRAYS
C
NMX=1
DO 2108 I=1,NICP
  IACT(I)=0
DO 2105 J=1,NUMAX
  TATRI(J)=0.
2108 TATRI(J)=0.
C
2109 NGM=0
DO 21 I=1,IEMAX
  IPTC(I)=0
DO 21 K=1,KMAX
  ICTK(I)=0
  IPCNT(K,I)=0
DO 22 J=1,IMAX
  IPC1(J)=0
  IPC2(J)=0
  IPC3(J)=0
22 IPC3(J)=0
C
C      OUTER C EVENT -DOOP
C
1844 JEM=IBVNT(1)
IF (IEM.LC.0) GO TO 952
IF (IEM.GT.KR) IEM=KR
DO 951 I=1,IEM
  IIO1=IC(INPA,IE,1)
  IF (IIO1.NE.0) GO TO 9510
  WRITE(6,9511) IIO1
9511 FORMATTED, IIO1=*,1107
GO TO 951
9510 CONTINUE
IF (INA.EQ.1.AND.ISCANF.EQ.1) GO TO 940
IPL=0
IF (IE.GT.1) IPL=IDC(IE-1)
IPL=IDC(IET)
IF (IPL.EQ.0) IPL=EQ,IP) GO TO 951
IF (IPL.LC.0) IPL=1
IF (IPL.GT.JMAX) IPL=JMAX
JE1=0
JE2=0
C
C      FIND 8 EVENTS ASSOCIATED WITH C EVENTS.
C      JEM IS NO. OF EVENTS IN PREVIOUS RADIAL.
C
105 IF (JEM.EQ.0) GO TO 41
IF (JEM.GT.KR) JEM=KR
DO 31 JE=1,JEM
  IF (IIB(2,JE,1).LT.IC(1,IE,1)) GO TO 31
  IF (IIB(1,JE,1).GT.IC(2,IE,1)) GO TO 41
  JE2=JE
  IF (JE1.EQ.0) JE1=JE
31 CONTINUE
C
C      FIND THRESHOLDS FOR IE EVENT
C
1492

```


SUBROUTINE	PEAK	74/74	OPT=2	FTN 4.64428	05/04/78	21.36.09	PAGE 4
131	CONTINUE					EXTRAD 1534	
	GO TO 161					EXTRAD 1535	
175	C	END RANGE FOR SEGMENT				EXTRAD 1536	
						EXTRAD 1537	
						EXTRAD 1538	
141	DO 151 KL=K,IPT					EXTRAD 1539	
	IF (JF2.EQ.0) GO TO 161					EXTRAD 1540	
180	IPE=IPCNT(KL,IE)					EXTRAD 1541	
	IPE=I-1					EXTRAD 1542	
	CALL IPKIPIC2,INEG,IPE,KL,IE,IJKR					EXTRAD 1543	
	CONTINUE					EXTRAD 1544	
151	CONTINUE					EXTRAD 1545	
161	CONTINUE					EXTRAD 1546	
185	C					EXTRAD 1547	
	ASSOCIATE CELLS LOOP ON THRESHOLD HIGHEST TO LOWEST					EXTRAD 1548	
						EXTRAD 1549	
940	DO 941 LC=L,IPT					EXTRAD 1550	
	KC=IPT-LC+1					EXTRAD 1551	
190	IF (KC.LE.0) GO TO 961					EXTRAD 1552	
	NPCE=IPCNT(KC,IE)					EXTRAD 1553	
	IF (NPCE.LE.0) GO TO 961					EXTRAD 1554	
	LOOP ON SEGMENTS					EXTRAD 1555	
195	DO 951 IPE=I,NPC					EXTRAD 1556	
	INB=IUPK(IPC1,IPE,KC,IE,I,JR)+1					EX1 83	
	INB=INB-1					TEST1 206	
	END=IUPK(IPC2,IPE,KC,IE,I,JR)					EX1 84	
	K=KC+1					EXTRAD 1557	
	NPKE=0					EXTRAD 1558	
200	TATM=0					EXTRAD 1559	
	IF (K.GT.IPT) GO TO 193					EXTRAD 1560	
	IPE=IPCNT(K,IE)					EXTRAD 1561	
	IF (IPE.LE.0) GO TO 193					EXTRAD 1562	
205	192. DO 191 L=1,LPE					EXTRAD 1563	
	IF (IUPK(IPC1,L,K,IE,I,JR).LT.INB) GO TO 191					TEST1 207	
	NPCE=IUPK(IPC3,L,K,IE,I,JR)					TEST1 208	
	IF (NPCE.EQ.0) GO TO 191					EXTRAD 1568	
	TATM=MAX1(TATM,TATR(NPCE,1))					EXTRAD 1569	
210	IF (TATM.EQ.TATR(NPCE,1)) NPKE=NPCE					TEST 327	
						TEST 328	
						EXTRAD 1572	
	NPCE IS FOR NEXT HIGHER ENCLOSED THRESHOLD ON C RADIAL					EXTRAD 1573	
215	231. IF (ABS(ITATR(NPCE,1))>.GT.(ITC(K,IE)+LOB)) GO TO 932					EXTRAD 1574	
	CONTINUE					TEST 329	
	GO TO 193					EXTRAD 1576	
932	NPKE=NPCE					EXTRAD 1577	
	GO TO 193					EXTRAD 1578	
1911	NPKE=-(NIDP+1)					EXTRAD 1579	
						EX1 85	
220	C	ASSOCIATE CELLS ON B RADIAL, TOP DOWN				EXTRAD 1581	
						EXTRAD 1582	
						EXTRAD 1583	
						EXTRAD 1584	
225	IF (JF2.EQ.0) GO TO 361					EXTRAD 1586	
	GO 261 JE=JE1,JE2					EXTRAD 1587	
	IF (I6(2,JE,1).LT.INB) GO TO 261					EXTRAD 1594	
						EXTRAD 1595	
						TEST1 209	


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230      C      IF(I1B(I,JE,I),GT,IHQ) GO TO 361
      C      JE EVENT ON B RADIAL IS ASSOCIATED
      C      271  IP3=IP1B(JE)
      C      IF(IPB.LE.0)GO TO 261
      C      DO 291 LB=1,IP3
      C      KB=IPB-LB+1
      C      KP=IPBNT(KB,JE)
      C      IF(IP1.LE.0)GO TO 231
      C      DO 281 JPE=1,MP1
      C      IF(IUP(IIP2,JEL,K3,JE,I2,J3),LT,IHBM) GO TO 281
      C      IF(IUP(IIP2,JPE,K3,JE,I2,J3),GT,IHQ) GO TO 231
      C      LPCEL=IUP(IIP3,JPE,K3,JE,I2,J3)
      C      IF(LPCEL.EQ.0)GO TO 281
      C      IF(IICAC,IE) .LE. I3(KB,JE)) GO TO 282
      C      282  IATM=AMAX1(IATM,IATRLP,LPCEL,I1JGO TO 281
      C      IF(IATF.NE.IATF,LPCEL,I1JGO TO 281
      C      MPK=LPCEL
      C      KB=KB
      C      JBM=JE
      C      281  CONTINUE
      C      291  CONTINUE
      C      261  CONTINUE
      C      IF(MPK.NE.0)GO TO 3661
      C      DO 194 I=IHB,IHQ
      C      IF(IHB(I).EQ.-999)GO TO 194
      C      IF(IHB(I).GT.IICAC,IE)I1JGO TO 934
      C      194  CONTINUE
      C      GO TO 361
      C      2661  IF(ABS(IATF(MPK,I1),GT,I2(K2,IE)+LOB)MPK=-MPK
      C      GO TO 361
      C      934  MPK=-I1JOP+1)
      C      C      HAVE B COMPARE WITHIN RANGE
      C      C      361  CONTINUE
      C      IF(MPK.EQ.0.AND.NPK.EQ.0)GO TO 631
      C      C      MPK=0.AND.NPK=J - NO COMPARE
      C      C      MPK=0.AND.NPK.NE.0 - NO B COMPARE
      C      C      NPK=0.AND.NPK.NE.0 - B COMPARE
      C      C      HIGHEST THIS RADIAL
      C      C      IF(MPK.EQ.0.AND.NPK.LT.0)GO TO 931
      C      IF(MPK.NE.0)GO TO 921
      C      C      NO PRIOR RADIAL. FOR COMPARISON, INCREMENT NPKEL
      C      C      361  NPKEL=MPK
      C      IF(MA.EQ. 1 .AND. ISCANF .EQ. 1) GO TO 392
      C      IF(I1J2.I1JGO TO 351
      C      DO 352 I=IHB,IHQ
      C      IF(I1J(I).EQ.-999)GO TO 352
      C      IF(I1J(I).GT. I2(K2,IE))GO TO 931
      C      352  CONTINUE

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353 INDX=IATR(NPCEL,I)-TC(K2,IEI)-1 TEST 334
391 IF (INDX-GE.LDB-OR.INDX-LE.0) GO TO 366 EXTRAD 1653
392 IN=I+INDX*LM TEST 335
INX=ID+INDX*LM EXTRAD 1657
290 IF (IATR(NPCEL,IN)-NE.U+JX-NR-EU-IGU TJ 3921 TEST 336
IF (IATR(NPCEL,IN-LM4).LE.0) GO TO 931 TEST 337
NPCEL=IATR(NPCEL,IN-LM4) TEST 338
NPCEL=IATR(NPCEL,IN-LM4) TEST 339
IF (NPG-EG.NPCEL)IGU TO 931 TEST 340
295 GO TO 359 EXTRAD 1662
3921 CALL IPKTPCS,NPCEL,PE,K,IE,IK,JKT TEST 341
2SP=IDU TEST 214
DO 411 I=1ST,ISP TEST 215
R=SQRT(FLOAT(I)-.5) TEST 342
RU=R*ABS(FLOAT(U(I))) TEST 343
IATR(NPCEL,IN+I)=IATR(NPCEL,IN+I)+DAZ*R TEST 344
IATR(NPCEL,IN+2)=IATR(NPCEL,IN+2)+DAZ*RJ TEST 345
IATR(NPCEL,IN+3)=IATR(NPCEL,IN+3)+DAZ*SZ*R*ZJ TEST 346
IATR(NPCEL,IN+4)=IATR(NPCEL,IN+4)+DAZ*CAZ*R*ZJ TEST 347
IF (IIV-EG.IGU TO 411 TEST 348
IF (SV(I).NE.-999) EX2 154
IATR(NPCEL,IN+5)=IATR(NPCEL,IN+5)+DAZ*R*SV(I) TEST 349
IF (IIV-GE.2)IGU TO 401 TEST 350
IF (IIV-EG.-999)IGU TO 401 TEST 351
IATR(NPCEL,IN+8)=IATR(NPCEL,IN+8)+DAZ*R*V(I) EXTRAD 1672
IF (IIV-EG.-999)IGU TO 401 TEST 216
IF (IIV-EG.-999)IGU TO 401 EXTRAD 1674
IATR(NPCEL,IN+7)=IATR(NPCEL,IN+7)+DAZ*R*IV(I)-V(I-1) TEST 352
401 IF (IIV-EG.-999) GO TJ 411 EXTRAD 1676
IATR(NPCEL,IN+6)=IATR(NPCEL,IN+6)+R*VS(I)+DAZ TEST 353
411 CONTINUE TEST 1678
419 IF (NPG-EG.I)IATR(NPCEL,IN)=SIGN(FLOAT(IN),IATR(NPCEL,INX)) TEST 354
IF (NPG-EG.I)IATR(NPCEL,IN)=SIGN(IATR(NPCEL,INX),-I.0) TEST 355
IF (IIV-LE.IMN-OR.ISP-GE.IMX) IATR(NPCEL,LOX)=-999. TEST 154
IF (IIV-LE.IMN-OR.ISP-GE.IMX) IATR(NPCEL,LOX)=-999. TEST 155
GO TO 365 EXTRAD 1682
3652 NPCEL=MPK EXTRAD 1683
IF (NPCEL-GE.NIUP-OR.NPCEL-LE.0) GO TO 931 EX1 94
365 INDX=IATR(NPCEL,I)-TC(K2,IEI)-1 TEST 357
C COMBINE LPCEL WITH NPCEL AT THIS LEVEL EXTRAD 1686
C COMBINE BY SETTING AREA AS POINTER AND IOX TO NA = 0 EXTRAD 1687
C EXTRAD 1689
DO 365 L=1,LPCE EXTRAD 1690
IF (IUPKTPCEL,K,IE,IK,JKT,IN) GO TO 365 TEST 217
IF (IUPKTPCEL,K,IE,IK,JKT,IN) GO TO 931 TEST 218
LPCEL=IUPKTPCEL,K,IE,IK,JKT EXTRAD 1695
IF (LPCEL-EG.0)IGU TO 365 TEST 1696
IF (IATR(LPCEL,IN)-EG.0)IGU TO 365 TEST 358
IF (NPCEL-EG.LPCEL)IGU TO 365 EXTRAD 1698
335 INDX=IATR(LPCEL,I)-TC(K2,IEI)-1 TEST 359
IF (INDX-GE.LDB)GO TO 365 EXTRAD 1700
IF (INDX-LE.0)INDX=0 EXTRAD 1701
IND=ID+INDX*LM EXTRAD 1702
IF (IATR(LPCEL,IND)-EG.0)IGU TO 365 TEST 360
IND=INDX*LM EXTRAD 1704
IPG=0 EXTRAD 1705

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DO 3663 J=IND,LOB
IN=(J-1)*LM+1
IF (IATR(LPCEL,IN*LM).EQ.NA)PG=IPG+1
DO 3663 I=1,LM
3663 IATR(LPCEL,IN*LM)=I
IF (IPG.EQ.0.OR.IE.LE.1)GO TO 3664
IE=IE-I
DO 3665 I=1,IET
IPTE=IPCTII
IF (IPTI.LE.0)GO TO 3665
DO 3666 KTEI,IPTI
NPCT=IPCTI(KT,I)
IF (NPCT.LE.0)GO TO 3666
DO 3667 LP=1,NPCT
3667 IATR(LPCEL,IN*LM)=NPCT
INOT=IATR(NPCEL,I)-I
IF (INDX.LT.LOB)GO TO 3668
3669 CALL IPK(IPC3,IZERO,LP,KT,I,IR,JR)
GO TO 3667
3668 IF (INDX.GE.LOB)GO TO 3669
CALL IPK(IPC3,NPCEL,LP,KT,I,IR,JR)
3667 CONTINUE
3666 CONTINUE
3665 CONTINUE
IPG=0
3664 IF (INDX.GE.LOB)GO TO 365
IATR(LPCEL)=NPCEL
IATR(LPCEL,2*INDX*LM)=NPCEL
IF (INDX.NE.0)GO TO 365
IATR(LPCEL)=NIOP-1
IATR(LPCEL,2I)=0.
365 CONTINUE
GO TO 931
C
C COMBINE NPCEL AND LPCEL, PEAK VALUES EQUAL
C
C
C COMBINE WITH 8 RADIAL CELLS
C
421 IF (NPK.LE.0)GO TO 422
IF (NPK.LT.0)GO TO 3662
NGH=0
LPCEL=NPK
IF (IATR(LPCEL,IDX).EQ.NA.AND.NPK.EQ.0.AND.TC(KG,IE).GT.TB(KBM,JM))
*GO TO 485
INDX=IATR(LPCEL,1)-TC(KG,IE)-1
INDX=INDX
390 IF (NPK.GT.0)INDX=IATR(NPK,1)-TC(KG,IE)-1
IF (INDX.LE.INDX)GO TO 4212
NGH=1
NPCEL=NPK
IND=INDX
INDX=IND
GO TO 4213
4212 IF (INDX.LT.0)GO TO 481
NPCEL=LPCEL

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D-39

AD-A057 153

ENVIRONMENTAL RESEARCH AND TECHNOLOGY INC CONCORD MASS F/G 4/2
DEVELOPMENT OF TECHNIQUES FOR SHORT-RANGE PRECIPITATION FORECAS--ETC(U)
DEC 77 R K CRANE F19628-77-C-0058

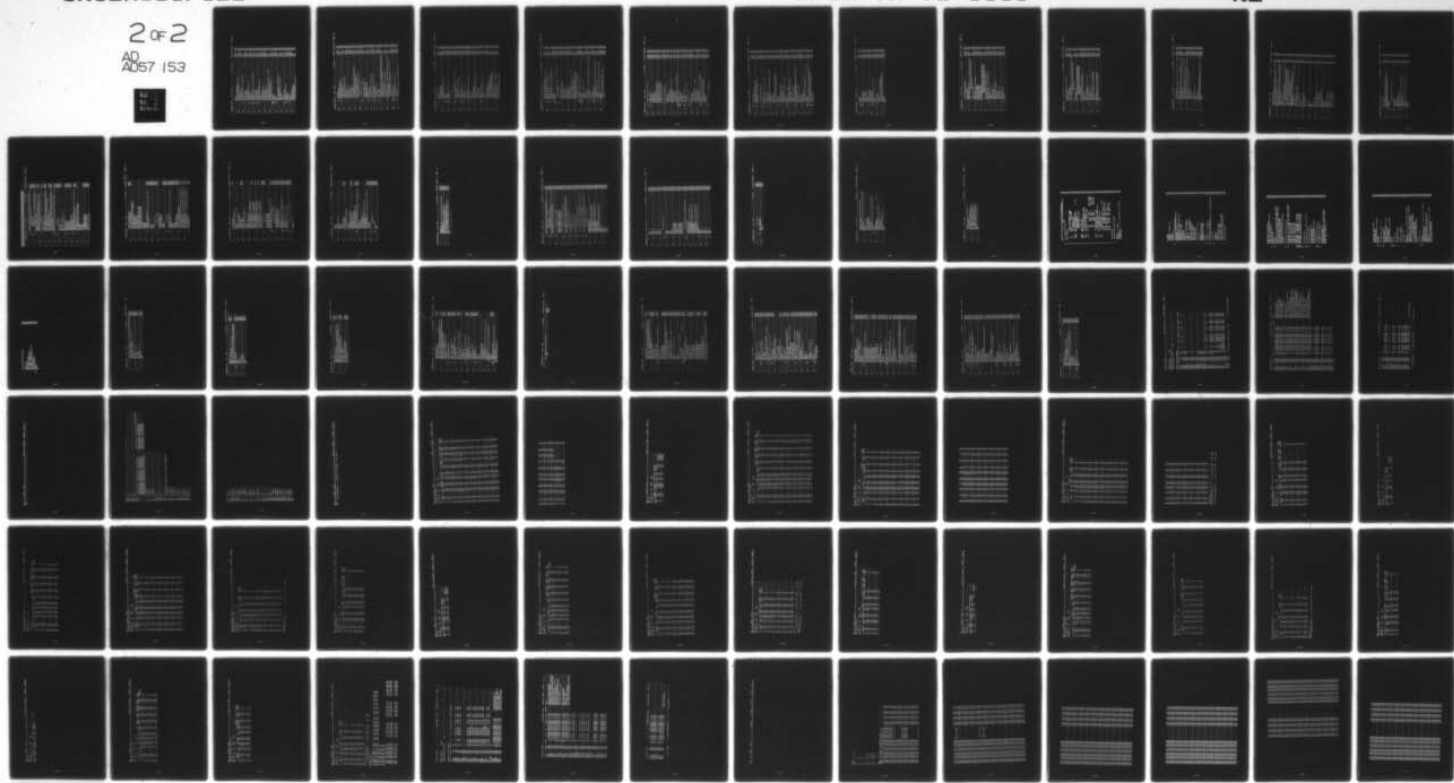
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      INS=2
      IPG=0
      TATR(LPCEL,1)=TG(KC,1E)+1
      TATR(LPCEL,NUMP)=ASS(1AT,1101,11)
      IF (INDX-GE,100)GO TO 482
      IND=L08-INDX
      DO 4832 I=INDX,L08H
      IF (TATR(LPCEL,IDX+I-1)*LM.E3,NA)IPG=IPG+1
      4832 CONTINUE
      DO 483 I=1,IND
      DO 483 J=1,LM
      IN=1+J+(L08-I)*LM
      IM=1+J+IND-I)*LM
      TATR(LPCEL,IN)=TATR(LPCEL,IM)
      IND=INDX*LM+I
      INDP=INDX
      483 DO 4835 I=1,L08
      IF (TATR(LPCEL,IDX+(I-1)*LM).EQ,NA)IPG=IPG+1
      4835 CONTINUE
      DO 484 I=INS,IND
      TATR(LPCEL,I)=0.
      484 DO 4841 I=1,INDP
      TATR(LPCEL,I)=0.
      4841 TATR(LPCEL,I)=0.
      IF (IPG.EQ,0)OR,IE,IE,1)50 TO 488
      IE=IE-1
      IF (I=1)GO TO 4831
      IF (I=1)GO TO 4831
      DO 4833 KI=1,IPIT
      NPCT=IPCT/KI
      IF (NPCT.LE,0)GO TO 4833
      DO 4834 LPCT,NPCT
      IF (LPCEL.NE,100)IPG3,LP,1,1,IR,JR)) GO TO 4834
      INDY=TATR(LPCEL,I)-TG(KC,I)-I
      IF (INDY.LT,L08)GO TO 4834
      CALL IPKTPCS,IZERO,LP,1,1,IR,JR)
      4834 CONTINUE
      4833 CONTINUE
      4831 CONTINUE
      IPG=0
      488 IN=0
      IF (LPCEL.LE,0)OR,LPCEL.GT,NHX)GO TO 931
      TATR(LPCEL,IDX)=NA
      CALL IPKTPCS,LPCEL,IPE,KC,IE,IR,JR)
      NPCEL=LPCEL
      NMH=0
      GO TO 512
      485 DO 485 I=1,N10P
      IF (I=1)OR,IE,IE,1)50 TO 487
      485 CONTINUE
      WRITE(6,644)
      GO TO 931
      487 LPCEL=I
      TACTY=I
      NMH=NA*(NMH,I+1)
      IF (NMH.GT,N10P)NMH=N10P
      TATR(LPCEL,1)=TG(KC,1E)+1
      TATR(LPCEL,NUMP)=ASS(1AT,1101,11)

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      YATR(NPCEL,ND+I)=0.
      CONTINUE
      YATR(NPCEL,ND+LW)=0.
      YATR(NPCEL,ND+1)=LPCEL
      YATR(NPCEL)=LPCEL
      CALL IPK(IPB3,LPCEL,JPE,C3+JE,IP,JR)
      575  CONTINUE
      461  CONTINUE
      471  CONTINUE
      481  CONTINUE
      580  IF (NPA.LE.0) GO TO 562
      NPCEL=LPCEL
      GO TO 566
      C
      C      UNASSOCIATED
      C
      585  631  IF (NA.EQ.1.AND. ISCANF.EQ.0) GO TO 539
      IF (NA.EQ.1) GO TO 533
      GO 641 IF=MB,IPD
      IF (MB(1).EQ.-999) GO TO 541
      IF (MB(1).GT. TC(KC,IE)) GO TO 931
      590  CONTINUE
      541  CONTINUE
      639  GO 642 IF=NIOP
      IF (ACT(1).EQ.0) GO TO 543
      642  CONTINUE
      WRITE(6,644)
      644  FORMAT(5X,' TOO MANY CE--S')
      GO TO 531
      630  NCCEL=NCCEL+1
      CALL IPK(IPB3,NCCEL,IPD,C3+JE,IP,JR)
      600  GO TO 531
      NPCEL=J
      IACT(J)=1
      IMKPAVE(NM,J+1)
      IF (NM.GT.NIOP) NM=NIOP
      635  CALL IPK(IPB3,NPCEL,IPD,C3+JE,IP,JR)
      IN=IDB-3)LM+INI
      GO 671 IF=INI,IN
      YATR(NPCEL,I)=0.0
      610  CONTINUE
      591  YATR(NPCEL,I)=Y(MG,IE)+1
      YATR(NPCEL,NUMP)=ABS(YATR(IAT,IID),1)
      125=IE
      135=IMC
      615  DO 621 IF=IST,ICP
      R=SCONC*(FLOAT(I-1)-S)
      R=RWEST*(FLOAT(I)-S)
      YATR(NPCEL,2)=CAZ*2+YATR(NPCEL,2)
      YATR(NPCEL,3)=CAZ*2+YATR(NPCEL,3)
      YATR(NPCEL,4)=CAZ*2+YATR(NPCEL,4)
      YATR(NPCEL,5)=YATR(NPCEL,5)+CAZ*2+YATR(NPCEL,5)
      IF (IY.EQ.0) GO TO 621
      IF (IY(1).NE.-999)
      * YATR(NPCEL,6)=YATR(NPCEL,6)+CAZ*2+YATR(NPCEL,6)
      IF (IY(2).EQ.0) GO TO 621
      IF (IY(1).EQ.-999) GO TO 621
      YATR(NPCEL,9)=YATR(NPCEL,9)+CAZ*2+YATR(NPCEL,9)
      TEST 416
      EXTRAD 1927
      TEST 417
      TEST 418
      EXTRAD 1930
      EXTRAD 1931
      EXTRAD 1932
      EXTRAD 1933
      EXTRAD 1934
      EXTRAD 1935
      EXTRAD 1936
      EXTRAD 1937
      EXTRAD 1938
      EXTRAD 1939
      EXTRAD 1940
      EXTRAD 1941
      EXTRAD 1942
      EXTRAD 1943
      EXTRAD 1944
      EXTRAD 1945
      EXTRAD 1946
      EX1 113
      EXTRAD 1948
      EXTRAD 1949
      EXTRAD 1950
      EXTRAD 1951
      EXTRAD 1952
      EXTRAD 1953
      EXTRAD 1954
      EXTRAD 1955
      EXTRAD 1956
      EXTRAD 1957
      EXTRAD 1958
      EX1 114
      EXTRAD 1959
      EXTRAD 1961
      EXTRAD 1962
      EXTRAD 1963
      TEST 419
      EXTRAD 1965
      TEST 420
      TEST1 238
      TEST1 239
      TEST1 240
      EXTRAD 1971
      EXTRAD 1972
      TEST 422
      TEST 423
      TEST 424
      TEST 425
      TEST1 241
      EX2 168
      TEST 427
      TEST 428
      TEST 429
      EXTRAD 1978
      TEST 430

```

[illegible]


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685 C COMBINE LAST TO FIRST CELL ATTR.
686 C
687 DO 9591 I=1, IEM
688   IPT=IP(I, IEM)
689   DO 9591 LGRT, LPT
690     KC=IPT-LG+1
691     KC=IPRT(KC, IEM)
692     DO 9591 IPE=1, NPG
693       NPCEL=IUPRT(IPE, IEM)
694       IF (NPCEL .LE. 0) GO TO 9591
695       LPEL=IUPRT(IPE, IEM)
696       IF (LPEL .LE. 0) GO TO 9591
697       INDX=IUPRT(IPE, IEM)
698       IF (INDX .LT. 0) GO TO 958
699       IF (INDX .GE. LGB) GO TO 955
700 C PEAK LPEL .GE. PEAK NPCEL.
701 C
702   INDELS=INDX
703   INDELS=INDX
704   DO 9592 I=1, IND
705     IN=I+J*(LGB-I)*M
706     IF (IAT(I, NPCEL, IN) .GE. 0.150 TO 9592
707       IN=I+J*(LGB-I)*M
708       TATR(LPEL, IN)=MAX-1
709       DO 9593 J=1, LHM
710       IN=I+J*(LGB-I)*M
711       IN=I+J*(LGB-I)*M
712       IN=I+J*(LGB-I)*M
713       IN=I+J*(LGB-I)*M
714       IN=I+J*(LGB-I)*M
715       IN=I+J*(LGB-I)*M
716       IN=I+J*(LGB-I)*M
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719       IN=I+J*(LGB-I)*M
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[illegible]

SUBROUTINE	PRN2	74/74	OPT=2	FTN 4.64428	05/04/78	21.36.09	PAGE	2
5	IC(1)=ICODES(IY)				EX2	259		
6	I=1+1				EX2	260		
60	IF (C.LY.NCOL.AND.C.LY.NIC.AND.I.LT.64) GO TO 3				TEST1	265		
	WRITE(IU,100)AZMUTH(NAB),ELEVAT,IDAY,IMOUR,IMIN,ISEC,IC				EX2	262		
100	FORMAT(IY,F5.1,F6.1,I4,IX,Z12,13,5X,6NAB)				EX2	263		
20	CONTINUE				EX2	264		
	RETURN				EX2	265		
65	C				EX2	266		
	C				EX2	267		
	C				EX2	268		
30	DO 35 K=2,3				EX2	269		
	IU=IUNIT(K)				EX2	270		
31	REWIND IU				EX2	271		
	CALL PAGE				EX2	272		
	WRITE(I6,101)TYPE(K)				EX2	273		
101	FORMAT(940 MAP OF ,A10)				EX2	274		
	CALL PERNG				EX2	275		
34	READ(IU,100)AZMUT2,ELEVAT,IDAY,IMOUR,IMIN,ISEC,IC				EX2	276		
355	CONTINUE				EX2	277		
	IF (ICOF(IU)) 35,355,35				EX2	278		
	WRITE(I6,100)AZMUT2,ELEVAT,IDAY,IMOUR,IMIN,ISEC,IC				EX2	279		
	GO TO 34				EX2	280		
35	CONTINUE				EX2	281		
	RETURN				EX2	282		
	END				EX2	283		

Year	1990	1991	1992	1993	1994	1995	1996	1997	1998	1999	2000	2001	2002	2003	2004	2005	2006	2007	2008	2009	2010	2011	2012	2013	2014	2015	2016	2017	2018	2019	2020	2021	2022	2023	2024	2025	2026	2027	2028	2029	2030	2031	2032	2033	2034	2035	2036	2037	2038	2039	2040	2041	2042	2043	2044	2045	2046	2047	2048	2049	2050	2051	2052	2053	2054	2055	2056	2057	2058	2059	2060	2061	2062	2063	2064	2065	2066	2067	2068	2069	2070	2071	2072	2073	2074	2075	2076	2077	2078	2079	2080	2081	2082	2083	2084	2085	2086	2087	2088	2089	2090	2091	2092	2093	2094	2095	2096	2097	2098	2099
1990	1991	1992	1993	1994	1995	1996	1997	1998	1999	2000	2001	2002	2003	2004	2005	2006	2007	2008	2009	2010	2011	2012	2013	2014	2015	2016	2017	2018	2019	2020	2021	2022	2023	2024	2025	2026	2027	2028	2029	2030	2031	2032	2033	2034	2035	2036	2037	2038	2039	2040	2041	2042	2043	2044	2045	2046	2047	2048	2049	2050	2051	2052	2053	2054	2055	2056	2057	2058	2059	2060	2061	2062	2063	2064	2065	2066	2067	2068	2069	2070	2071	2072	2073	2074	2075	2076	2077	2078	2079	2080	2081	2082	2083	2084	2085	2086	2087	2088	2089	2090	2091	2092	2093	2094	2095	2096	2097	2098	2099	

[illegible]

64	<pre> XK2=1,2,3,4,5,6,7,8,9,10,11,12,13,14,15,16,17,18,19,20,21,22,23,24,25,26,27,28,29,30,31,32,33,34,35,36,37,38,39,40,41,42,43,44,45,46,47,48,49,50,51,52,53,54,55,56,57,58,59,60,61,62,63,64,65,66,67,68,69,70,71,72,73,74,75,76,77,78,79,80,81,82,83,84,85,86,87,88,89,90,91,92,93,94,95,96,97,98,99,100,101,102,103,104,105,106,107,108,109,110,111,112,113,114,115,116,117,118,119,120,121,122,123,124,125,126,127,128,129,130,131,132,133,134,135,136,137,138,139,140,141,142,143,144,145,146,147,148,149,150,151,152,153,154,155,156,157,158,159,160,161,162,163,164,165,166,167,168,169,170,171,172,173,174,175,176,177,178,179,180,181,182,183,184,185,186,187,188,189,190,191,192,193,194,195,196,197,198,199,200,201,202,203,204,205,206,207,208,209,210,211,212,213,214,215,216,217,218,219,220,221,222,223,224,225,226,227,228,229,230,231,232,233,234,235,236,237,238,239,240,241,242,243,244,245,246,247,248,249,250,251,252,253,254,255,256,257,258,259,260,261,262,263,264,265,266,267,268,269,270,271,272,273,274,275,276,277,278,279,280,281,282,283,284,285,286,287,288,289,290,291,292,293,294,295,296,297,298,299,300,301,302,303,304,305,306,307,308,309,310,311,312,313,314,315,316,317,318,319,320,321,322,323,324,325,326,327,328,329,330,331,332,333,334,335,336,337,338,339,340,341,342,343,344,345,346,347,348,349,350,351,352,353,354,355,356,357,358,359,360,361,362,363,364,365,366,367,368,369,370,371,372,373,374,375,376,377,378,379,380,381,382,383,384,385,386,387,388,389,390,391,392,393,394,395,396,397,398,399,400,401,402,403,404,405,406,407,408,409,410,411,412,413,414,415,416,417,418,419,420,421,422,423,424,425,426,427,428,429,430,431,432,433,434,435,436,437,438,439,440,441,442,443,444,445,446,447,448,449,450,451,452,453,454,455,456,457,458,459,460,461,462,463,464,465,466,467,468,469,470,471,472,473,474,475,476,477,478,479,480,481,482,483,484,485,486,487,488,489,490,491,492,493,494,495,496,497,498,499,500,501,502,503,504,505,506,507,508,509,510,511,512,513,514,515,516,517,518,519,520,521,522,523,524,525,526,527,528,529,530,531,532,533,534,535,536,537,538,539,540,541,542,543,544,545,546,547,548,549,550,551,552,553,554,555,556,557,558,559,560,561,562,563,564,565,566,567,568,569,570,571,572,573,574,575,576,577,578,579,580,581,582,583,584,585,586,587,588,589,590,591,592,593,594,595,596,597,598,599,600,601,602,603,604,605,606,607,608,609,610,611,612,613,614,615,616,617,618,619,620,621,622,623,624,625,626,627,628,629,630,631,632,633,634,635,636,637,638,639,640,641,642,643,644,645,646,647,648,649,650,651,652,653,654,655,656,657,658,659,660,661,662,663,664,665,666,667,668,669,670,671,672,673,674,675,676,677,678,679,680,681,682,683,684,685,686,687,688,689,690,691,692,693,694,695,696,697,698,699,700,701,702,703,704,705,706,707,708,709,710,711,712,713,714,715,716,717,718,719,720,721,722,723,724,725,726,727,728,729,730,731,732,733,734,735,736,737,738,739,740,741,742,743,744,745,746,747,748,749,750,751,752,753,754,755,756,757,758,759,760,761,762,763,764,765,766,767,768,769,770,771,772,773,774,775,776,777,778,779,780,781,782,783,784,785,786,787,788,789,790,791,792,793,794,795,796,797,798,799,800,801,802,803,804,805,806,807,808,809,810,811,812,813,814,815,816,817,818,819,820,821,822,823,824,825,826,827,828,829,830,831,832,833,834,835,836,837,838,839,840,841,842,843,844,845,846,847,848,849,850,851,852,853,854,855,856,857,858,859,860,861,862,863,864,865,866,867,868,869,870,871,872,873,874,875,876,877,878,879,880,881,882,883,884,885,886,887,888,889,890,891,892,893,894,895,896,897,898,899,900,901,902,903,904,905,906,907,908,909,910,911,912,913,914,915,916,917,918,919,920,921,922,923,924,925,926,927,928,929,930,931,932,933,934,935,936,937,938,939,940,941,942,943,944,945,946,947,948,949,950,951,952,953,954,955,956,957,958,959,960,961,962,963,964,965,966,967,968,969,970,971,972,973,974,975,976,977,978,979,980,981,982,983,984,985,986,987,988,989,990,991,992,993,994,995,996,997,998,999,1000,1001,1002,1003,1004,1005,1006,1007,1008,1009,1010,1011,1012,1013,1014,1015,1016,1017,1018,1019,1020,1021,1022,1023,1024,1025,1026,1027,1028,1029,1030,1031,1032,1033,1034,1035,1</pre>
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YEAR=YE
IO=KA
GO TO 53
175 500 IF (.NOT. LK) GO TO 3
YEAR=YE
YEAR=YE
IO=KB
GO TO 53
180 51 READ(2)YBAR,YBAR,IO
IF (.NOT. (2)) 999, 52
52 IF (TIME. - 999) GO TO 53
CALL LABEL(IXR, IYR, ELEVAT, XSIZ)
GO TO 3
185 53 CONTINUE
YBAR=YBAR-4.4*5*YLEN*YIN
YBAR=YBAR-4.4*5*YLEN*YIN
IF (.NOT. LSTGO) TO 60
YBAR=(YBAR-XI)*SF*YIN
YBAR=YBAR-YII*SF*YIN
60 WRITE(6,103)YBAR,YBAR,IO,XBAR,YBAR
103 FORMAT(IX,2Y7.3,I5,I5,I5,2F8.3)
IF (XBAR5.LT.X1.OR.XBAR5.GT.X2.OR.YBAR5.LT.Y1.OR.YBAR5.GT.Y2)
GO TO 51
IO=IO-1
IO=IO-1
195 IO=IO-1
JINDEX=JINDEX-3
IF (.NOT. IPLT(JINDEX)) GO TO 51
ISYM=JSYM(JINDEX)
CALL SYMBOL(XBAR,YBAR,SSIZ,ISYM,XMETA,0)
IF (JINDEX-6E-3) GO TO 51
FIO=IO-1
FIO=IO-1
CALL NUMBER(YBAR5,SYCSIZ,YBAR5,SYCSIZ,FIO,XMETA,-1)
GO TO 51
205 61 WRITE(6,IUI)
IO=IO-1
IO=IO-1
C TERMINATE PLOT
C
999 CALL ENOPLT
STOP
END
001360
001370
001440
001450
001460
001470
001510
001520
001530
001540
001550
001560
001570
001580
001590

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1	BLOCK DATA	001678
	COMMON/HEAD/TITLE (6), ICODE, VERS, LEVEL, DAT, IIRUN, NPAGE, MLOG	001618
	COMMON/LINUM/LINE	001628
	COMMON/EXPAN/X1,X2,Y1,Y2,XMIN,XMAX,YMIN,YMAX	001638
3	DATA X1/X2/Y1/Y2/XMIN/XMAX/YMIN/YMAX	001648
	DATA XMIN/1.0, XMAX/9.0, YMIN/1.0, YMAX/9.0	001658
	DATA TITLE/PROGRAM,7M EXPAND,IN ,IN ,IN /,	001668
	IIRUN/0, NPAGE/0, ICODE/175, VERS/1.0, LEVEL/770331/	001678
	END	001688

SUBROUTINE	EXPAN1	74/76	OPT=1	FTM 4.6426	05/03/76	16.00.13	PAGE
1	C	SUBROUTINE EXPAN1(XA,YA,XB,YB,RETURNS,INI,NZ,N3)					001698
	C	VERSION 1.0 LEVEL 7778337					001700
	C	AFGL C056600					001718
	C	SPECIAL EXPANDET TWICE PLOTTING.					001720
	C	COMMON/EXPAN1,X1,X2,Y1,Y2,XMIN,XMAX,YMIN,YMAX					001730
	C						001740
	C						001750
	C						001760
10	C	TEST IF LINE IS IN THE AREA					001770
	C						001780
	C						001790
	C	IF(XA-LT-X1-AND-XB-LT-Y1)RETURN N1					001800
	C	IF(YA-GT-Y2-AND-YB-GT-X2)RETURN N1					001810
	C	IF(YA-LT-Y1-AND-YB-LT-Y1)RETURN N1					001820
15	C	IF(YA-GT-Y2-AND-YB-GT-Y2)RETURN N1					001830
	C						001840
	C	TEST IF LINE IS TOTALLY IN THE AREA					001850
	C						001860
20	C	IF(XA-GE-X1-AND-XA-LE-X2-AND-YB-GE-Y1-AND-YB-LE-X2-AND- 1YA-GE-Y1-AND-YA-LE-Y2-AND-Y3-GE-Y1-AND-Y3-LE-Y2)GO TO 49					001870
	C						001880
	C	TEST IF SLOPE IS INFINITE					001890
	C						001900
	C	IF((XB-XA).EQ.0.0)GO TO 17					001910
	C						001920
25	C	TEST IF SLOPE IS ZERO					001930
	C						001940
	C	IF((YB-YA).EQ.0.0)GO TO 18					001950
	C						001960
	C	TEST IF POINT A IS IN THE AREA					001970
	C						001980
30	C	IF(YA-GE-X1-AND-XA-LE-X2-AND-YA-GE-Y1-AND-YA-LE-Y2)GO TO 20					001990
	C						002000
	C	TEST IF POINT B IS IN THE AREA					002010
	C						002020
35	C	IF(XB-GE-X1-AND-XB-LE-X2-AND-YB-GE-Y1-AND-YB-LE-Y2)GO TO 10					002030
	C						002040
	C	RESET POINTS TO CLOSEST SIDES					002050
	C						002060
	C						002070
	C						002080
40	C	SLOPB=(YB-YA)/(XB-XA)					002090
	C	BYB=SLOPB*(YB-Y1)					002100
	C	IF(B-GT-Y1-AND-B-LE-Y2-AND-XB-LT-X1)GO TO 4					002110
	C	IF(B-GE-Y1-AND-B-LE-Y2-AND-XB-LT-X1)GO TO 5					002120
	C	9=YB-SLOPB*(XB-X2)					002130
	C	IF(B-GE-Y1-AND-B-LE-Y2-AND-XB-GT-X2)GO TO 8					002140
	C	IF(B-GE-Y1-AND-B-LE-Y2-AND-XA-GT-X2)GO TO 9					002150
	C	SLOPA=X1/SLOPB					002160
	C	A=XB-SLOPA*(YB-Y1)					002170
	C	IF(A-GE-X1-AND-A-LE-X2-AND-YB-LT-Y1)GO TO 6					002180
	C	IF(A-GE-X1-AND-A-LE-X2-AND-YA-LT-Y1)GO TO 7					002190
	C	RETURN N3					002200
	4	XB=X1					002210
		YB=B					002220
	5	GO TO 10					002230
		XA=X1					002240
		YA=B					002250
		GO TO 20					002260

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6      YB=Y1      002260
      XB=A        002270
      GO TO 10    002280
7      YA=Y1      002290
      XB=B        002300
      GO TO 28    002310
      XB=XZ       002320
      YB=B        002330
65     GO TO 18    002340
      XA=X2       002350
      YB=B        002360
      GO TO 20    002370
78     C          002380
      C          002390
      C          002400
      C          002410
10     XS=XA      002420
      YS=YA       002430
      XA=XB       002440
      YA=YB       002450
      XB=XS       002460
      YB=YS       002470
      GO TO 20    002480
80     17 IF(YA.LT.Y1)YA=Y1 002490
      IF(YB.LT.Y1)YB=Y1 002500
      IF(YA.GT.Y2)YA=Y2 002510
      IF(YB.GT.Y2)YB=Y2 002520
      GO TO 49    002530
85     18 IF(XA.LT.X1)XA=X1 002540
      IF(XB.LT.X1)XB=X1 002550
      IF(XA.GT.X2)XA=X2 002560
      IF(XB.GT.X2)XB=X2 002570
      GO TO 49    002580
90     C          002590
      C          002600
      C          002610
20     SLOP8=(YB-YA)/(XB-XA) 002620
      B=YB-SLOP8*(XB-X1) 002630
      IF(B.GE.Y1.AND.B.LE.Y2.AND.XB.LT.X1)GO TO 22 002640
      B=YB-SLOP8*(XB-X2) 002650
      IF(B.GE.Y1.AND.B.LE.Y2.AND.XB.GT.X2)GO TO 24 002660
      SLOPA=1.0/SLOP8 002670
      A=XB-SLOPA*(YB-Y1) 002680
      IF(A.GE.X1.AND.A.LE.X2.AND.YB.LT.Y1)GO TO 26 002690
      A=XB-SLOPA*(YB-Y2) 002700
      IF(A.GE.X1.AND.A.LE.X2.AND.YB.GT.Y2)GO TO 28 002710
      RETURN M3 002720
22     YB=B      002730
      XB=X1      002740
      GO TO 49    002750
24     YB=B      002760
      XB=X2      002770
      GO TO 49    002780
26     YB=B      002790
      XB=X1      002800
      GO TO 49    002810
28     XB=A      002820
      YB=Y2

```


SUBROUTINE	EXPAN1	74/74	OPT=1	FTN 4.64428	05/02/78	14.00.13	PAGE	3
115	C							
	C		PLOT THE LINE					
	C							
	49		CALL PLOT(XA,YA,3)					
			CALL PLOT(XB,YB,2)					
120			RETURN M2					
			END					

```

1  SUBROUTINE MUSCAL(X1,X2,XLEN,XSTART,XEND,DELY)
   DIMENSION DELTA(15)
   DATA DELTA /1.,2.,5.,10.,20.,25.,40.,50.,75.,100.,150.,200.,
   *250.,350.,500./
   XMAX=X2
   XMIN=X1
   IF (X2.LT.X1) XMAX=X1
   IF (X2.LT.X1) XMIN=X2
   DIFF=(XMAX-XMIN)/XLEN
   DO 10 J=2,15
   IF (DIFF.GT.DELTA(J-1).AND.DIFF.LE.DELTA(J)) GO TO 20
   10 CONTINUE
   J=15
   DELY=DELTA(J)
   ISTART=XMIN/DELY
   ISTART=ISTART*DELY
   IF (XMIN.LT.0.) ISTART=(ISTART-1)*DELY
   IEND=XMAX/DELY
   IEND=(IEND+1)*DELY
   IF (XMAX.LT.0.) IEND=IEND*DELY
   RETURN
   END

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1  SUBROUTINE LABEL(IX,IY,ELEVAT,XSIZ)
   DIMENSION LABL(3)
   DATA LABL/4MDAY,4NTHME,4REL /
   CALL SYMBOL(1,5,01,XSIZ,LABL(1),0,0,4)
   CALL NUMBER(2,0,0,01,XSIZ,LABL(2),0,0,4)
   CALL SYMBOL(3,0,0,01,XSIZ,LABL(3),0,0,4)
   CALL NUMBER(4,0,0,01,XSIZ,IY,0,0,4)
   CALL SYMBOL(5,0,0,01,XSIZ,LABL(3),0,0,4)
   CALL NUMBER(6,5,0,01,XSIZ,ELEVAT,0,0,4)
   RETURN
10  END

```



```

100 SUBROUTINE LINLOG (X,Y,BCD,N,PLTEN,NUMBUS,BEGNUM,ENDNUM,
110 DEL , NUMDEC, THETA, BCDSZ,DRAM,XMOD,ITYPE)
120
130 PLOT LABELED LINEAR OR LOG AXIS
140
150 INPUT PARAMETERS
160
170 X X CORD OF POINT BEGNUM IN INCHES
180 Y Y CORD OF POINT ENDNUM IN INCHES
190 BCD TITLE
200 N NUMB. CHARACTERS IN BCD
210 N NCHARS TITLE
220 PLTEN LENGTH IN INCHES ENTIRE AXIS
230 NUMBUS NUMB. SUBDIV. BETWEEN MAJOR DIV. (N.A. LOG)
240 NUMBUS <=NO SUBDIVISIONS
250 NUMBUS 2=DIVIDE MAJOR DIV. IN 1/2
260 NUMBUS 3=DIVIDE MAJOR DIV. IN 1/3
270 ETC
280
290 VALUE AT AXIS ORIGIN
300 VALUE AT AXIS END
310 ABS OF DELTA VALUE BETWEEN MAJOR DIV.
320 -DEL = START DIVISIONS AT ENDNUM
330 NUMDEC NUMB. PLACES AFTER DEC. PT.
340 THETA AXIS ANGLE
350 X-AXIS BOTTOM LEFT TO RIGHT
360 X-AXIS TOP LEFT TO RIGHT
370 X-AXIS USED AS Y LEFT TO RIGHT
380 Y-AXIS LEFT BOT TO TOP
390 Y-AXIS RIGHT BOT TO TOP
400 Y-AXIS USED AS X BOT TO TOP
410
420 BCDSZ LETTER SIZE IN INCHES
430 CLEARANCE NEEDED 3.1 *BCDSZ
440 DRAM LENGTH IN INCHES OF MAJOR DIVISION LINES
450 XMOD MODULO VALUE FOR MAJOR DIVISION
460 0.0=NON-CYCLICAL
470 1= LINEAR AXIS NORMAL TITLE EXP ONLY
480 2= LOG AXIS NORMAL TITLE EXP ONLY
490 3= LOG AXIS NORMAL TITLE BASE 10 & EXP
500 4= LOG AXIS NORMAL TITLE BASE E & EXP
510 -1= LINEAR AXIS VERT TITLE
520 -2= LOG AXIS VERT TITLE EXP ONLY
530 -3= LOG AXIS VERT TITLE BASE 10 & EXP
540 -4= LOG AXIS VERT TITLE BASE E & EXP
550
560 DIMENSION BCD(1)
570
580 SET ORIENTATION AND SIZE PARAMETERS
590
600 ISPEC=0
610 IF(DEL .LT. 0.0) ISPEC=1
620 KIND=ITYPE
630 IF((IABS(ITYPE) .LT. 1) .OR. (IABS(ITYPE) .GT. 4)) KIND=1
640 DELNUM=ABS(DEL)

```

```

650 ON #BEGNUM
660 ON #ENDNUM
670 IF(BEGNUM .LT. ENDNUM) GO TO 5
680 ON #ENDNUM
690 OFF#BEGNUM
700 DELNUMS=DELNUM
710
720
730
740
750
760
770
780
790
800
810
820
830
840
850
860
870
880
890
900
910
920
930
940
950
960
970
980
990
1000
1010
1020
1030
1040
1050
1060
1070
1080
1090
1100
1110
1120
1130
1140
1150
1160
1170
1180
1190

C 5
  NUMDIV=ABS((ENDNUM-BEGNUM)/DELNUM)
  DIVLEN=PLTLEN/ ABS((ENDNUM-BEGNUM)/DELNUM)
  HEIGHT=CDI2*0.75
  VRT2=CDI2*(0.25*CDI2)
  SUPERHEIGHT/2.0 * 9 9127ENHEIGHT*0.75
  SINANG=91N(THETA/37.2950)
  COSANG=COS(THETA/37.2950)
  SIN1=ABS(SINANG)
  COS1=ABS(COSANG)
  THETA2=THETA
  IF(THETA .EQ. -180.0) THETA2=0.0
  IF(THETA .EQ. 270.0) THETA2=90.0
  SIGNER1=0
  IF(THETA .LE. 45.0) SIGNER=-1.0
  IF(THETA .EQ. -90.0) SIGNER=1.0
  TICANG=THETA*(90.0*SIGNER)
  TIC812 = (0.20 * HEIGHT) * .10
  SIZIC = 0.50 * TIC812
  XENDX=(PLTLEN*COS1)
  YENDY=(PLTLEN*SIN1)
  IF(IABS(XEND) .GE. 2) GO TO 10
  IF(IABS(YEND) .GE. 2) GO TO 10
  SUBDIV = 0
  IF(NUMSUB .LE. 0) GO TO 99
  SUBDIV=DIVLEN/FLOAT(NUMSUB)
  SUBNUM=DELNUM/FLOAT(NUMSUB)
  GO TO 99
  NUMTIC=1
  IF(DIVLEN .LT. 1.0) NUMTIC=2
  DIVOFF=HEIGHT*((1.25*SIGNER)-0.5)
  IF((THETA .EQ. -180.) .OR. (THETA .EQ. 270.)) DIVOFF=DIVOFF+HEIGHT
  CYCLING LOOP
  N1=NUMDIV +1
  DO 999 I=1,N1
  CYCLES=I-1
  DIVTIC = CYCLES * DIVLEN
  TICC = X *(DIVTIC * COS1)
  TICY = Y *(DIVTIC * SIN1)
  IF(ISPEC .EQ. 1) TICC=XEND-(DIVTIC*COS1)
  IF(ISPEC .EQ. 1) TICY=YEND-(DIVTIC*SIN1)
  DRAW DIVISION NUMBERS
  C
  C
  C

```

```

1209 IF (NUMDEC .LT. (-1)) GO TO 101
1210 DIVNUM = BEGNUM + (CYCLES * DELNUM)
1220 IF (ISPEC .EQ. 1) DIVNUM=ENDNUM-(CYCLES*DELNUM)
1230 IF (IMOD .EQ. 0.0) GO TO 102
1240 IF (DIVNUM .LT. XM00) GO TO 102
1250 DIVNUM=DIVNUM-XM00
1260 GO TO 101
1270
1280 PLACES = 0.
1290 IF (DIVNUM .NE. 0.) PLACES = AINT (ALOG10 (ABS (DIVNUM)))
1300 OFFSET = -.50 * HEIGHT * (PLACES + FLOAT (NUMDEC) * 1.25)
1310 IF ((THETA.EQ.-180.) .OR. (THETA.EQ. 270.)) OFFSET=OFFSET
1320 XP=TIC*(OFFSET+COSANG)-(DIVOFF+SINANG)
1330 YP=TIC*(OFFSET+SINANG)+(DIVOFF+COSANG)
1340 IF (IABS(KIND) .GT. 2) GO TO 201
1350 CALL NUMBER (XP,YP,HEIGHT,DIVNUM,THET2,NUMDEC)
1360 GO TO 301
1370
1380 SPECIAL LABEL LOG BASE 10 OR E & EXP
1390
1400 IF (IABS(KIND) .EQ. 3) CALL NUMBER (XP,YP,SIZTEN,10.,THET2,-1)
1410 IF (IABS(KIND) .EQ. 4) CALL SYMBOL (XP,YP,SIZTEN,1ME,THET2, 1)
1420 IF (THETA .EQ. 0.0) GO TO 202
1430 IF (THETA .EQ. -180.0) GO TO 202
1440 IF (THETA .EQ. 90.0) GO TO 203
1450 IF (THETA .EQ. 270.0) GO TO 203
1460 IF (THETA .EQ. 180.0) GO TO 204
1470 IF (THETA .EQ. -90.0) GO TO 205
1480 XP=XP+HEIGHT * YPSYTP*HEIGHT * 60 TO 299
1490 YP=YP+HEIGHT * YPSYTP*HEIGHT * 60 TO 299
1500 XP=XP+HEIGHT * YPSYTP*HEIGHT * 60 TO 299
1510 YP=YP+HEIGHT * YPSYTP*HEIGHT * 60 TO 299
1520 CALL NUMBER (XP,YP,SUPER,DIVNUM,THET2,NUMDEC)
1530
1540
1550
1560
1570
1580
1590
1600
1610
1620
1630
1640
1650
1660
1670
1680
1690
1700
1710
1720
1730
1740

```

```

C
C
C
201
C
C
C
202
203
204
205
299
C
C
C
C
301
C
C
C
C
C
C
C
302
C
C
C
C

```


2300
2310
2320
2330
2340
2350
2360
2370
2380
2390
2400
2410
2420
2430
2440

```

C      IC=I*(OFFCEN+SIGN3)+(BCDOFF+COS3)
      II=1
      DO 1002 I=1,N
      JCM=MOD(I,10)
      IF(JCM.EQ.0) JCM=10
      ISIGHT=NGETX (BCD(II),JCM,1)
      LEFT  =NGPUTX (ISIGHT,LEFT,1)
      CALL SYMSON (IC,VC,BCOSIZ,LEFT,TIME3,1)
      IF(MOD(I,10).EQ.0) II=II+1
      IC=IC+(VTSIZ+SIGN3)
      VC=VC-(VTSIZ+COS3)
1002  CONTINUE
      RETURN
      END

```

```

1  PROGRAM ASOCC L (INPUT,OUTPUT,TAPE1,TAPE2,TAPE5=INPUT,TAPE6=OUTPUT) 000100
   LOGICAL PR1,PR2,PR3,PR4
   COMMON /PLG3/ ITYPE,PR1,PR2,PR3,PR4,ISTOP
   COMMON /INPUT/ ID1,ID2
   CALL INIT
   CALL PR1
   5  CALL PR2
   IF (ISTOP .EQ. 1) STOP
   CALL INPUT
   CALL TRACK
   IF (ITYPE .NE. 6) GO TO 5
   REMIND IDEV2
   GO TO 5
   END
000110
000120
000125
000131
000136
000137
000140
000143
000147
000148
000149

```



```

1      SUBROUTINE INIT
      LOGICAL PR1,PR2,PR3,PR4,PR5,PR6
      COMMON /FLGS/ ITYPE,PR1,PR2,PR3,PR4,PR5,PR6,ISTOP
      COMMON /CNTRS/ IELSCN,IIVLSCN,IAXIS1,MAXR,IUCLMX,IJOMMX,ICMOMX
      COMMON /DATA/ VCL(13,100,3),ECL(10,200),IMVCL(25),ICMPL(10)
      IEXBRL=0
      100  FORMAT(1X,'INIT')
      ISTOP=0
      IELSCN=0
      IIVLSCN=0
      DO 10 IX=1,3
      DO 10 IY=1,100
      DO 10 KX=1,13
      100  KCLMX=IX,IY=0
      10  RETURN
      END

```

```

1      BLOCK DATA
      LOGICAL PR1,PR2,PR3,PR4
      COMMON /DATA/ VOL(13,180,3),ECL(18,200),IMVCL(25),ICMPRI(13)
      COMMON/PR1S/ INCL,INCL1,INCL2,INCL3,INCL4,INCL5,INCL6,INCL7,INCL8,INCL9,INCL10,INCL11,INCL12,INCL13,INCL14,INCL15,INCL16,INCL17,INCL18,INCL19,INCL20,INCL21,INCL22,INCL23,INCL24,INCL25
      COMMON /CNTR/ IELSON,IELSON,IATRI(5),MAYR,IWCLWY,IMPMX,ICMPMX
      COMMON/ANCL/ ELANG,IOAF,IMM,MIN,ISEC
      COMMON /FLGS/ ITYPE,PR1,PR2,PR3,PR4,ISTOP
      COMMON /INPUT/ IDEX1,IDEX2
      DATA IATRI/3,7,9,7,5/
      DATA IIEEX1/,IIEEX2/,IIEEX3/,IIEEX4/,IIEEX5/,IIEEX6/,IIEEX7/,IIEEX8/,IIEEX9/,IIEEX10/,IIEEX11/,IIEEX12/,IIEEX13/,IIEEX14/,IIEEX15/,IIEEX16/,IIEEX17/,IIEEX18/,IIEEX19/,IIEEX20/,IIEEX21/,IIEEX22/,IIEEX23/,IIEEX24/,IIEEX25/
      DATA PR1/.F./,PR2/.F./,PR3/.F./
      DATA IDEX1/,IDEX2/,IDEX3/,IDEX4/,IDEX5/
      DATA ICMPMX/10/
      END
  
```


SUBROUTINE INPUT	IN/TA	OPER	FTN A-64420	34/28/7A	12-58-52	PAGE
238	FORMAT(2X, *EOF REACHED ON TAPE1*)					2
60	RETURN					
	END					
				000790		
				000800		
				000810		


```

115      Y2=VCL(1,INEM,ITYPE)      001520
      Y2=VCL(2,INEM,ITYPE)      001521
      DIS1=SQRT((ELXS-X1)**2+(ELYS-Y1)**2) 001522
      DIS2=SQRT((ELXS-X2)**2+(ELYS-Y2)**2) 001523
      IF(8152 .LT. DIS1) ICMPR=INEM 001524
      K42=K42+1 001525
      IF(ICMPR(K42) .EQ. 8) GOTO 35 001526
      GOTO 222 001527
      C NEW VOL. CELL-ADD TO LIST 001528
22      IF(221) PRINT A50,2M4,IX,MCLOS,XS1,XS2,XS1,Y52 001529
      VCL(1,IVCLS,ITYPE)=ELXS 001530
      VCL(2,IVCLS,ITYPE)=ELYS 001531
      VCL(3,IVCLS,ITYPE)=RS 001532
      VCL(4,IVCLS,ITYPE)=MT 001533
      VCL(5,IVCLS,ITYPE)=ECL(2,JX) 001534
      VCL(6,IVCLS,ITYPE)=IDMF 001535
      VCL(7,IVCLS,ITYPE)=IHR 001536
      VCL(8,IVCLS,ITYPE)=MIN 001537
      VCL(9,IVCLS,ITYPE)=ISEC 001538
      VCL(10,IVCLS,ITYPE)=AREAS 001539
      VCL(11,IVCLS,ITYPE)=ECL(1,JX) 001540
      VCL(12,IVCLS,ITYPE)=ECL(7,JX) 001541
      IVCLS=IVCLS+1 001542
      C CHECK FOR OVERFLOW OF VC 001543
      IF(IVCLS .LE. IVCLMX) GOTO 40 001544
      PRINT 316 001545
      IVCLS=IVCLMX 001546
      GOTO 48 001547
      C ELEV. CELLS COMPARE UPDATE ATTRIBUTES 001548
      C REPLACE WITH NEW HEIGHT 001549
      35 CONTINUE 001550
      IF(221) PRINT A50,IX,IX,MT,AREAS 001551
      FORMAT(1Y,UPDATE VCL°,IX,IX,IX,° WITH ECL°,IX,IX 001552
      1,2X,2E12.4) 001553
      VCL(3,IX,ITYPE)=RS 001554
      IF(AREAS .LE. VCL(8,IX,ITYPE)) GOTO 48 001555
      VCL(4,IX,ITYPE)=MT 001556
      VCL(5,IX,ITYPE)=AREAS 001557
      48 CONTINUE 001558
      NEZ 001559
      IF(222) PRINT 320,N,IVC.S,((VCL(IX,JX,ITYPE),IX=1,17, JX=1,IVCLS) 001560
      C AFTER COMPARING ALL NEW ELEV. CELLS MOVE UP SEGMENT END ENTP 001561
      IVCL=IVCLS-1 001562
      ELANG=ELANG 001563
      GOTO 188 001564
      C PROCESS VOL TRACK BEFORE PROCESSING NEW ELEVATION CELLS 001565
      45 IVCL=IVCL+1 001566
      IF(IVCL .GT. 1) GOTO 188 001567
      C CREATE VOL LIST HEAD TABLE 001568
      IVCL=IVCL 001569
      IF(IVCL .LE. IMOPX) GOTO 49 001570
      PRINT 330,IMOPX 001571
      330 FORMAT(2X,IVCLC ,GT.,°,2X,15) 001572
      IVCLC=IMOPX 001573
      49 00 47 IV=1,IVCLC1 001574
      47 IMVCLC(IV)=IV 001575
      IVCLC=IVCLC1+1 001576

```


1	SUBROUTINE PRM	002560
	LOGICAL PR1,PR2,PR3,PR4	002570
	COMMON /FLGS/ ITYPE, PR1, PR2, PR3, PR4, ISTOP	002580
	COMMON /INPUT1/ IOEV1,IOEV2	002590
5	NAMELIST /PARAM/ PR1,PR2,PR3,PR4,IOEV1,IOEV2,ISTOP	002600
	PRINT 100	002610
100	FORMAT(IX,'INPUT...PR1,PR2,PR3,PR4,IOEV1,IOEV2,I(TOP*)	002620
	READ(5,PARAM)	002630
	IF(EOF(5))15,3	002640
10	WRITE(6,PARAM)	002650
	GOTO 20	002660
15	PRINT 110	002670
	FORMAT(IX,'EOF ON UNIT 3')	002680
110	RETURN	002690
20	END	002700
15		002710

FMA OF THE LOAD 111
LMA+1 OF THE LOAD 227071

TRANSFER ADDRESS -- EXTRAD 14574

PROGRAM AND BLOCK ASSIGNMENTS.

BLOCK	ADDRESS	LENGTH	FILE	DATE	PROCESSOR LEVEL	MARKING	COMMENTS
/PRM/	111	64					
EXTRAD	175	14506	LGO	05/04/78	FTN	4.6 428	666X 1 OPT=2
/INSUB/	16703	24					
/I2M/	16727	720					
/I02N7/	15647	6008					
/VALHA/	23647	13					
/ADATA/	23662	10					
/HEAD/	23672	15					
/LTDUM/	23707	1					
/MGRED/	23710	5					
/STORE/	23735	7					
/EJPM/	23724	10					
/ERRDP/	23734	1					
/FILPE/	23735	3					
/HELPM/	23740	1					
/QUANTX/	23741	3					
/PMORE/	23745	22158					
/FIXEO/	46114	3413					
/PESTOPE/	51527	31876					
/PWSTORE/	103425	20212					
/PESTOPE/	135337	26526					
/REFL/	162365	1272					
BCPORT.	163557	0	LGO	05/04/78	FTN	4.6 428	666X 1 OPT=2
/LOOKUP/	163657	172					
INPMP	164951	460	LGO	05/04/78	FTN	4.6 428	666X 1 OPT=2
/DEL/	164531	2550					
/I22/	167301	5					
EXTRAY	167306	1136	LGO	05/04/78	FTN	4.6 428	666X 1 OPT=2
COMP7	170445	1555	LGO	05/04/78	FTN	4.6 428	666X 1 OPT=2
CONTOR	172221	11803	LGO	05/04/78	FTN	4.6 428	666X 1 OPT=2
PEKRO	203524	4270	LGO	05/04/78	FTN	4.6 428	666X 1 OPT=2
/MSKVAL/	210014	6					
TUPK	210022	103	LGO	05/04/78	FTN	4.6 428	666X 1 OPT=2
IPK	210125	104	LGO	05/04/78	FTN	4.6 428	666X 1 OPT=2
PRANG	210231	50	LGO	05/04/78	FTN	4.6 428	666X 1 OPT=2
PAN2	210311	362	LGO	05/04/78	FTN	4.6 428	666X 1 OPT=2
PAGE	210573	33	UL-EXTLIB	02/16/78	FTN	4.6 428	666X 1 OPT=1
LINES	210726	44	UL-EXTLIB	02/16/78	FTN	4.6 428	666X 1 OPT=1
DAY	211772	10	UL-EXTLIB	02/16/78	FTN	4.6 428	666X 1 OPT=1
ERSA	211802	25	UL-EXTLIB	02/16/78	FTN	4.6 428	666X 1 OPT=1
INE	211827	125	UL-EXTLIB	02/16/78	FTN	4.6 428	666X 1 OPT=1
/STP.END/	211154	1					
/FCL.G./	211155	23					
/P.LO./	211200	133					
CHYBY=	211333	0	SL-FOOTRAN	04/12/77	COMPASS	3. 3-428	FCL INITIALIZATION ROUTINE.

BLOCK	ADDRESS	LENGTH	FILE	DATE	PROCESSOR	VER	LEVEL	HARDWARE	COMMENTS
BUFTN=	21133	46	SL-FORTAN	05/12/77	COMPASS	3.	3-428		BUFFERED INPUT PROCESSOR.
FECHSK=	211401	41	SL-FORTAN	05/12/77	COMPASS	3.	3-428		INITIALIZE CONSTANTS.
FLROUTE=	211462	311	SL-FORTAN	05/12/77	COMPASS	3.	3-428		COMMON FLOATING OUTPUT CODE
FORPYS=	211753	603	SL-FORTAN	05/12/77	COMPASS	3.	3-428		FORTAN OBJECT LIBRARY UTILITIES.
INCOME=	212556	276	SL-FORTAN	05/12/77	COMPASS	3.	3-428		COMMON INPUT FORMATTING CODE
INPC=	213054	160	SL-FORTAN	05/12/77	COMPASS	3.	3-428		FORMATTED READ FORTRAN RECORD.
KODER=	213234	456	SL-FORTAN	05/12/77	COMPASS	3.	3-428		OUTPUT FORMAT INTERPRETER.
NAMOUT=	213712	274	SL-FORTAN	05/12/77	COMPASS	3.	3-428		NAMLIST OUTPUT ROUTINE.
214206	227								
OUTB=	214435	203	SL-FORTAN	05/12/77	COMPASS	3.	3-428		BINARY WRITE FORTRAN RECORD.
OUTCOM=	214580	154	SL-FORTAN	05/12/77	COMPASS	3.	3-428		COMMON OUTPUT CODE
REWIND=	215014	37	SL-FORTAN	05/12/77	COMPASS	3.	3-428		POSITION FILE AT BEGINNING-OF- INFORMATION.
UNIT=	215053	50	SL-FORTAN	05/12/77	COMPASS	3.	3-428		STATUS OF BUFFER I/O FILE.
CLOCK=	215123	31	SL-FORTAN	05/12/77	COMPASS	3.	3-428		ACCESS SYSTEM CLOCKS FOR FORTRAN.
OUTOPE=	215154	14	SL-FORTAN	05/12/77	COMPASS	3.	3-428		COMPUTED GO TO ERROR PROCESSOR.
ALOG=	215170	73	SL-FORTAN	05/12/77	COMPASS	3.	3-428		COMPUTE COMMON AND NATURAL LOGARITHMS. OPT=ALL.
EXP=	215263	75	SL-FORTAN	05/12/77	COMPASS	3.	3-428		EXPONENTIAL FUNCTION. E TO POWER X. OPT=ALL.
ITOU=	215360	16	SL-FORTAN	05/12/77	COMPASS	3.	3-428		INTEGER TO INTEGER EXPONENTIATION.
SYNGOS=	215376	66	SL-FORTAN	05/12/77	COMPASS	3.	3-428		TRIGONOMETRIC SINE OR COSINE OF X. OPT=ALL.
SYSDIO=	215464	1	SL-FORTAN	05/12/77	COMPASS	3.	3-428		LINK BETWEEN SYS-AID AND INITIALIZATION CODE.
POFIC=	215465	125	SL-FORTAN	05/12/77	COMPASS	3.	3-428		COMMON SET-UP ROUTINE FOR BUFIN/BUPOUT.
COMIC=	215512	64	SL-FORTAN	05/12/77	COMPASS	3.	3-428		COMMON CODED I/O ROUTINES AND CONSTANTS.
FOF=	215576	16	SL-FORTAN	05/12/77	COMPASS	3.	3-428		TEST FOR END OF FILE STATUS.
FLTN=	215714	154	SL-FORTAN	05/12/77	COMPASS	3.	3-428		COMMON FLOATING INPUT CONVERTER.
FMPE=	216370	352	SL-FORTAN	05/12/77	COMPASS	3.	3-428		CRACK APLIST AND FORMAT FOR KODER/KRAKER.
FOPLT=	216442	16	SL-FORTAN	05/12/77	COMPASS	3.	3-428		FOR MISC. UTILITIES.
GFPLT=	216520	42	SL-FORTAN	05/12/77	COMPASS	3.	3-428		LOCATE EN FIT GIVEN A FILE NAME.
KRAKER=	216522	406	SL-FORTAN	05/12/77	COMPASS	3.	3-428		PROCESS FORMATTED FORTRAN INPUT.
NAMIN=	217130	523	SL-FORTAN	05/12/77	COMPASS	3.	3-428		NAMLIST INPUT ROUTINE.
OUTC=	217653	172	SL-FORTAN	05/12/77	COMPASS	3.	3-428		FORMATTED WRITE FORTRAN RECORD.
SORT=	220045	43	SL-FORTAN	05/12/77	COMPASS	3.	3-428		COMPUTE THE SQUARE ROOT OF X. OPT=ALL.
SYSLST=	220110	62	SL-FORTAN	05/12/77	COMPASS	3.	3-428		MATH LIBRARY LINK TO ERROR MESSAGE PROCESSOR.
XTOVE=	220172	7	SL-FORTAN	05/12/77	COMPASS	3.	3-428		REAL TO REAL EXPONENTIATION.
SXF.SQ	220201	2	SL-SYSIO	05/03/76	COMPASS	3.	2-414		
CON.PM	220203	6							
CIO.PM	220211	40	SL-SYSIO	05/03/76	COMPASS	3.	2-414		
AOB.PM	220251	10							
MOVE.PM	220261	64	SL-SYSIO	05/03/76	COMPASS	3.	2-414		
WCT.PM	220345	233	SL-SYSIO	05/03/76	COMPASS	3.	2-414		
CHEK.PM	220360	107	SL-SYSIO	05/03/76	COMPASS	3.	2-414		
OSUB.PM	220707	71	SL-SYSIO	05/03/76	COMPASS	3.	2-414		
JMPS.PM	221000	11							
JPEF.FO	221011	7							
OPEN.SQ	221020	254	SL-SYSIO	05/03/76	COMPASS	3.	2-414		
CPRE.SQ	221274	14	SL-SYSIO	05/03/76	COMPASS	3.	2-414		
PUT.PM	221310	11							
PLEG.PM	221321	42	SL-SYSIO	05/03/76	COMPASS	3.	2-414		
CLSF.FO	221363	7							
CLSF.SQ	221372	134	SL-SYSIO	05/03/76	COMPASS	3.	2-414		
CLSA.FO	221526	7							
CLVA.SQ	221535	137	SL-SYSIO	05/03/76	COMPASS	3.	2-414		
REM.FO	221674	7							
PEH.SQ	221703	33	SL-SYSIO	05/03/76	COMPASS	3.	2-414		
ATPP.PM	221736	1							
GET.FO	221737	7							

LOAD MAP - EXTRAD

GET.BY/	221746	5		
GET.RT/	221753	11		
GET.SQ	221764	1134	SL-SVSIO	09/03/76 COMPASS 3. 2-414
	221820	101	SL-SVSIO	09/03/76 COMPASS 3. 2-414
F50.SQ	221821	106	SL-SVSIO	09/03/76 COMPASS 3. 2-414
SVFL.FQ/	221837	7		
SVSF.FQ/	221838	1		
SVSF.SQ/	221837	50	SL-SVSIO	09/03/76 COMPASS 3. 2-414
SVRL.FQ/	221840	7		
SVSR.FQ/	221846	1		
SVSR.SQ	221847	101	SL-SVSIO	09/03/76 COMPASS 3. 2-414
ERG.PH	221850	404	SL-SVSIO	09/03/76 COMPASS 3. 2-414
CHRG.PH	221874	7	SL-SVSIO	09/03/76 COMPASS 3. 2-414
MEMG.PH	224133	3		
70PES.FQ/	224136	1		
OPEN.PH	224137	237	SL-SVSIO	09/03/76 COMPASS 3. 2-414
OPES.SQ	224176	121	SL-SVSIO	09/03/76 COMPASS 3. 2-414
PUT.FQ/	224517	7		
PUT.SQ	224526	1400	SL-SVSIO	09/03/76 COMPASS 3. 2-414
WAR.SQ	224626	260	SL-SVSIO	09/03/76 COMPASS 3. 2-414
CLSF.PH	224606	25	SL-SVSIO	09/03/76 COMPASS 3. 2-414
GTWR.SQ	224633	41	SL-SVSIO	09/03/76 COMPASS 3. 2-414
BTPT.SQ	224674	115	SL-SVSIO	09/03/76 COMPASS 3. 2-414
WEXA.SQ	224681	150	SL-SVSIO	09/03/76 COMPASS 3. 2-414
SVFL.SQ	224761	51	SL-SVSIO	09/03/76 COMPASS 3. 2-414
SYS.RM	224732	37	SL-NUCLEUS	04/15/77 COMPASS 3. 2-414

PROCESS SYSTEM REQUEST.

1.348 CP SECONDS	2437003 CM STORAGE USED	129 TABLE MOVES
------------------	-------------------------	-----------------

162 0 PROGRAM EXTRAD VERSION 2.0 (780501) 05/06/78 PAGE 1
PARA

3INPUT	
PRINT1 = F,	
PRINT2 = F,	
PRINT3 = F,	
COPLOT = I,	
ICODES = -329406144173304950, 30001026016254029, 40996224525736413,	66910623035219797, 04525021544700781, 102939420054102765
120953310563664749, 136960217073146733, 156902615802620717,	174997014092110701, 193011412601592645,
211025011111074669, 229040209520556653, 247054608130030637,	26506900653932021, 283023405159002605,
301097003650444509, 319112202167966573, 33712660677444557,	355140999106930541, 373155397696412525,
391169706205994509, 409181194715375543, 42719859322405877,	445212391734340561, 463227392438224455,
481241780753304429, 51727054572268397, 535204904261759381,	553293362741232365, 571313761300714349,
-563593324796650642, -545578926257160633, -527564527777686674,	-509550125268204690, -491535730758722706,
X1 = .443E+00,	
B1 = .56E+00,	
A2 = .86E+00,	
B2 = .186E+02,	
CONTRZ = I,	
CONTRV = I,	
CONTR5 = I,	
WHILE = U,	
MONF = 30,	
AC = -.10776555E+03, .19767838E+01, -.34297323E-01, .10226310E-03,	
CALM = .332E+00,	
CALB = -.983E+02,	
XCUT = .1E+02,	
CK = .1E+02,	
ZMAX = 0.0,	
VMAX = 0.0,	
NREC = 1,	
MONR = 99999,	
TRUN = 0,	
INC = 0,	
PI = -.000000,	

YOW	= 0.0,
DN	= 0.0,
STARTM	= .2E+02,
STOPR	= .15E+03,
IMPRF	= 7%,
SCALE	= .1E+01,
XE	= .121E+01,
YA	= .4E+03,
BB	= .14E+01,
IX	= 0.0,
XZ	= .0E+01,
YA	= 0.0,
YZ	= .0E+01,
AL	= 35,
ASL	= 1000000,
LDV	= 3,
LYD	= 3,
LSV	= 3,
LCOMP	= 6,
AMIN	= 0.0,
SMIN	= 0.0,
MEANM	= .1E+01,
WAVEL	= .542E+01,
POURNT	= .1E+02,
SOURNT	= .5E+01,
WOURNT	= .1E+01,
VOLYMP	= 1,
DAZN	= .1E+01,
ESTYNT	= .15E+01,
DELY	= .5E+00,
RENO	

162	0	PROGRAM	EXTRAD	VERSION	2.0	(700501)	05/04/76	PAGE	2
EXEC		NO OF RECORDS/RECORD	6	CELL WIDTH	937.2	METERS	PMF	795.0	

FIXED CONTOUR ATTRIBUTES

DAY	MM	SS	ELE	ARM1	ARM2
226	133	40	1.2	118.2	116.2
FIXED CONTOUR ATTRIBUTES					
THRESHOLD	AREA	REFLECTIVITY	EAST	LOCATION	
10	10821	10821	10821	10821	10821
1	20	1.27	26.1	12.6	-15.7
2	20	1.85	32.3	15.8	-19.3
3	20	2.34	35.9	14.6	-18.3
4	20	1.85	29.6	22.3	-33.1
5	20	3.95	21.0	-36.7	-47.8
6	20	6.68	21.6	-37.9	-53.7
7	20	3.30	36.0	-18.4	-13.7
8	20	1.61	38.3	-18.8	-9.7
9	20	14.93	25.5	-132.1	-67.3
10	20	6.88	29.8	-36.7	-3.3
11	20	8.14	34.0	-35.1	-10.1
12	20	1.40	21.0	-84.5	-26.3
13	20	326.28	36.0	-127.6	-44.5
14	20	2.89	38.6	-37.0	5
15	20	2.15	21.0	-147.8	-22.5
16	20	326.32	28.8	-17.3	11.3
17	20	25.33	26.1	-132.3	6.7
18	20	397.33	41.7	-25.4	22.1
19	20	10.18	41.0	-33.3	9.4
20	20	2.08	21.0	-54.5	11.7
21	20	9.11	24.7	-182.7	24.3
22	20	2.29	21.0	-128.7	31.3
23	20	2.50	21.0	-140.6	34.7
24	20	3.53	21.0	-124.7	34.7
25	20	9.42	22.7	-118.6	48.1
26	20	2.88	24.0	-133.4	39.3
27	20	1.49	21.0	-83.8	26.3
28	20	1.76	37.6	-25.6	12.3
29	20	4.30	21.5	-114.1	96.3
30	20	2.24	22.0	-83.2	73.5
31	20	2.89	27.4	-51.3	51.4
32	20	4.15	21.0	-76.6	76.3
33	20	4.28	21.0	-84.1	123.3
34	20	1.88	24.0	-32.6	58.3
35	20	31.27	24.2	-75.1	126.3
36	20	5.34	22.0	-83.2	78.3
37	20	9.85	23.2	-69.1	86.3
38	20	1.66	22.0	-45.8	94.4
39	20	118.95	29.7	-34.8	89.1
40	20	2.51	21.5	-35.2	79.3
41	20	34.65	32.4	-27.4	70.7
42	20	1.33	21.8	-7.2	18.3
43	20	1.52	21.0	-24.3	32.3
44	20	77.46	25.0	-4.7	38.8
45	20	1.30	21.5	-3.2	19.3
46	20	14.45	21.7	-9.0	62.3
47	20	8.95	23.4	-15.2	93.8
48	20	5.75	22.1	-14.5	89.3
49	20	3.97	21.8	-3.3	62.7
50	20	1.55	25.2	-3	23.3
51	20	2.98	21.6	3.8	22.3

22	28	2.55	0.227	2.55	17.53	0.002	0.1	1.004	0.21	-7.0
23	28	7.56	26.4	12.2	59.1	40.9	1.3	5.43	.75	73
24	28	6.87	22.1	17.3	56.7	57.5	4.7	2.33	.52	74
25	28	12.50	21.7	35.7	71.3	92.1	9.3	6.18	.69	81
26	28	1.53	21.5	38.3	98.1	97.5	1.1	.74	.46	76
27	28	11.62	22.0	37.2	57.6	74.6	5.5	5.95	.51	82
28	28	13.59	22.5	37.2	57.6	109.1	13.9	1.89	.88	72
29	28	1.12	21.0	44.8	64.2	70.3	.9	.49	.66	83
30	28	2.64	21.5	52.1	17.1	88.2	1.9	1.22	.88	86
31	28	59.0	31	32.3	59.5	87.2	413.8	1315.98	2.23	85
32	28	2.1	25.6	17.7	72.1	27.5	3.1	1.28	1.87	95
33	28	4.55	22.2	80.8	114.3	145.3	1.9	2.37	.82	87
34	28	1.27	28.6	17.3	19.4	20.1	3.3	1.83	1.88	-96
35	28	95.83	29.1	100.4	108.1	147.5	35.6	125.63	1.66	-90
36	28	3.38	33.3	31.1	-6.3	36.8	6.3	18.53	2.77	99
37	1	13.52	43.1	-124.7	-49.5	134.2	6.2		18	18
38	2	13.1	41.1	-10.3	-36.1	107.8	7.6		18	18
39	3	3.99	41.5	-130.8	-68.3	138.6	1.8		18	18
40	4	33.3	42.3	-31.3	-56.9	162.1	13.2		18	18
41	5	2.19	41.4	-133.2	-36.3	138.2	1.8		18	18
42	6	3.1	42.2	-14.0	-36.7	146.7	.9		18	18
43	7	2.2	41.4	-33.2	6.5	34.4	4.6		35	35
44	8	194.6	46.3	-27.6	28.4	34.3	18.67		36	36
45	9	31.5	43.0	-1.55	28.5	32.6	6.53		36	36
46	10	15.33	42.5	55.3	50.7	82.1	12.5		85	85

WIND DATA

DAY MONTH SS ELE AZM1 AZM2
226 1933 68 1.2 118.2 118.2

HEIGHT	AVERAGE	TOTAL	AVERAGE	AVERAGE	VELOCITY	DEL
(M)	REFLECTIVITY	REFLECTIVITY	U	V	(M/SEC)	
(DBZ)	(DBZ)	(DBZ)	(M/SEC)	(M/SEC)	(M/SEC)	
1	22.0	67.3	0.0	0.0	112.4	-0.44409E-15
2	27.1	9289.0	12.6	-18.1	60.3	0.57697E988
3	35.0	671779.4	5.1	-10.1	61.0	0.39223E+01
4	31.8	219615.2	-38.6	26.8	76.6	0.21589E-21
5	23.4	21683.5	-5.8	-8.5	69.9	0.80681E+01
6	28.1	75385.5	-7.1	-7.9	91.8	0.54582E988

PEAK DETECTED CELL ATTRIBUTES

DAY MONTH SS ELE AZM1 AZM2
226 1977 40 1.2 118.2 118.2

IO	REFLECTIVITY (DBZ)	AREA (KM ²)	LOCATION EAST NORTH (KM)	RANGE (KM)	AREA ELEMENTS	VELOCITY SPEED (M/S)	AVERAGE RADIAL SHEAR (M/S/KM)	AVERAGE TANGENTIAL SHEAR (M/S/KM)	AVERAGE RADIAL VELOCITY (M/S)	FIXED VELOCITY CONTOUR REFERENCE	MEAN
1	32.5	5.8	-110.9	-44.5	119.5	2.8	1.93	.06	-4.64	12	12
2	44.0	6.3	-124.1	-48.8	133.6	3.2	2.45	-.21	-3.13	18	18
3	51.5	6.5	-135.2	-57.9	143.8	1.9	1.98	-.27	-1.35	18	18
4	44.5	13.0	-131.3	-36.8	187.7	7.4	1.60	-.32	-.09	16	16
5	48.0	2.4	-131.9	-44.3	139.2	1.1	1.83	-.84	-.20	10	10
6	37.6	1.8	-135.1	-11.8	37.0	3.0	1.34	.14	0.00	19	19
7	41.0	8.3	-132.6	-35.6	137.3	3.7	2.07	-.88	-.51	18	18
8	41.0	4.2	-142.4	-36.9	147.1	1.8	1.50	.16	-.45	18	18
9	37.8	5.5	-139.3	-38.5	143.5	2.8	1.98	-.28	-.41	12	12
10	33.5	5.0	-143.2	-29.6	146.2	2.1	.92	-.85	-2.35	14	14
11	33.1	15.5	-129.4	-23.7	131.5	5.8	1.81	.11	-.13	18	18
12	25.0	2.1	-134.5	2.5	134.5	1.0	0.80	1.32	0.00	31	31
13	32.8	2.7	-132.4	6.3	132.6	1.2	.50	.11	0.00	31	31
14	27.0	3.5	-182.6	24.4	185.4	2.1	.33	-.37	-.50	30	30
15	27.5	35.1	-139.1	24.5	65.5	31.7	1.20	-.32	-3.45	34	34
16	22.6	9.4	-135.7	40.0	142.4	4.0	.75	.32	-.15	42	42
17	25.0	2.4	-135.4	39.8	139.2	1.2	.17	0.00	-.50	43	43
18	43.5	1.5	-135.6	13.2	36.0	2.5	2.20	-1.32	-.45	36	36
19	43.0	1.3	-136.4	15.4	37.7	3.2	1.54	-.66	-2.73	36	36
20	49.6	9.8	-26.0	20.0	33.5	17.8	1.74	-.35	-.26	36	36
21	27.4	2.1	-51.3	51.4	72.5	1.8	.43	0.00	0.00	42	42
22	50.0	1.7	-23.2	25.6	34.5	5.1	1.50	-1.31	-.22	36	36
23	27.0	6.3	-74.2	125.5	145.7	2.3	.61	-.37	-5.03	53	53
24	24.5	3.7	-63.4	89.9	101.7	2.2	.08	0.00	-.19	55	55
25	25.0	1.4	-33.5	79.3	88.6	1.0	.87	0.00	-.20	54	54
26	45.0	1.5	-12.3	30.6	31.0	3.0	.74	-.34	-.17	36	36
27	38.0	2.4	-28.0	78.8	75.3	1.3	.92	-.38	-10.25	53	53
28	38.4	4.8	-32.5	84.9	94.8	3.1	1.21	-.53	-10.16	57	57
29	23.5	1.1	-8.7	32.1	33.3	1.3	1.08	-.27	-11.60	36	36
30	25.5	2.4	-10.1	36.6	38.0	3.3	.75	-.16	-12.13	36	36
31	27.3	5.0	-16.3	53.0	34.4	3.3	.38	-.35	-11.57	65	65
32	22.0	5.7	-14.5	84.8	90.9	3.9	.29	-.12	-11.35	66	66
33	23.3	9.4	-5.5	40.3	43.7	15.2	1.05	-.35	-12.74	62	62
34	25.9	5.9	-4.5	40.2	40.5	9.1	1.37	-.32	-12.23	62	62
35	25.0	1.1	13.4	39.5	41.7	1.7	1.65	-.31	-15.13	73	73
36	25.5	13.4	45.0	106.2	116.9	7.2	.63	.13	-6.93	78	78
37	25.8	7.3	43.7	87.4	92.7	5.5	1.35	-.31	-6.61	78	78
38	26.8	5.3	47.8	91.8	103.5	3.7	1.35	-.22	-7.23	72	72
39	21.6	12.5	33.7	71.8	182.1	9.3	1.61	-.53	-1.21	51	51
40	25.8	22.4	54.7	97.0	111.4	12.3	1.26	-.34	-7.06	78	78
41	31.9	11.5	37.2	64.9	74.5	9.5	1.13	-.33	-1.42	82	82
42	37.0	1.1	49.7	56.4	74.5	.9	1.67	-.53	2.40	85	85
43	37.5	6.3	45.1	53.7	75.2	6.8	1.67	-.57	-6.13	85	85
44	41.8	7.7	54.5	63.4	81.3	5.8	2.19	-.23	-2.70	85	85
45	38.0	2.3	181.3	136.7	147.5	1.8	2.83	-.11	-11.70	90	90
46	25.5	3.9	88.5	86.4	123.7	1.9	1.83	-.30	-9.15	85	85
47	32.5	6.3	71.2	68.5	98.5	3.3	2.73	1.03	-7.37	85	85
48	27.9	23.7	97.0	93.0	134.4	11.5	1.56	-.55	-11.67	85	85

TANGENTIAL SHEAR MAXIMA ATTRIBUTES

DAY HHMM SS ELE AZM1 AZM2
226 1933 40 1.2 118.2 118.2

ID	MAGNITUDE SHEAR (M/S/KM)	LOCATION		RANGE (KM)	AREA RESOLUTION ELEMENTS (M/S)	AVERAGE		FIXED CONTOUR REFERENCE
		AREA (KM*2)	NORTH (KM)			VELOCITY SPREAD (M/S/KM)	AVERAGE SHEAR (M/S/KM)	
1	1.7	2.3	-132.0	-57.1	151.3	1.0	1.3	13
2	1.6	2.1	-125.2	-51.6	135.4	1.0	2.3	16
3	1.8	4.4	-126.9	-51.6	137.7	1.9	2.4	18
4	1.5	1.9	-111.3	-45.9	128.4	1.0	1.9	18
5	1.8	6.8	-129.5	-53.4	148.1	3.0	2.7	15
6	2.6	1.6	-101.5	-37.7	108.2	.9	1.3	18
7	2.7	1.6	-105.8	-39.0	112.3	.9	2.0	18
8	2.4	3.3	-107.2	-39.9	114.4	1.8	2.0	18
9	1.8	3.6	-117.7	-43.8	125.5	1.8	.5	18
10	.5	9.4	-97.6	-35.4	103.3	5.5	1.2	18
11	2.0	2.2	-132.9	-47.1	151.3	1.0	1.6	18
12	1.2	4.7	-128.0	-42.9	135.3	2.1	1.5	18
13	1.5	1.7	-102.3	-32.3	107.3	1.0	1.2	18
14	.5	1.6	-95.2	-30.0	99.3	1.0	2.3	15
15	1.9	2.2	-134.5	-42.4	151.3	1.0	3.2	18
16	2.2	1.8	-100.2	-29.7	104.5	1.1	0.0	18
17	1.1	2.3	-129.8	-38.5	135.5	1.1	2.3	18
18	1.3	4.4	-134.6	-37.3	139.7	1.9	2.5	18
19	1.9	1.5	-98.8	-25.1	96.2	1.0	0.8	18
20	1.1	2.1	-139.3	-36.0	143.3	.9	1.7	18
21	.8	2.5	-142.2	-31.9	145.7	1.0	2.7	18
22	.3	11.7	-137.4	-29.1	140.5	5.1	1.5	18
23	.8	2.0	-124.8	-23.4	127.3	1.0	1.5	18
24	.9	4.6	-143.7	-27.0	146.2	1.9	0.0	18
25	.5	7.8	-131.4	-20.6	133.3	3.6	2.5	18
26	.9	2.2	-128.6	-17.7	129.1	1.1	0.0	18
27	.9	2.2	-125.8	-17.3	127.3	1.1	0.0	18
28	.5	4.0	-66.1	3.4	66.2	3.7	1.7	34
29	1.0	6.2	-131.4	9.7	131.7	2.9	0.0	31
30	.4	3.1	-69.2	5.4	69.4	2.7	1.4	34
31	.3	3.4	-68.6	5.4	68.5	3.4	1.7	34
32	.4	6.7	-67.5	8.8	68.3	6.0	1.4	34
33	.8	1.0	-57.3	18.0	58.2	1.1	1.5	34
34	.3	2.0	-75.4	13.2	76.5	1.6	1.3	34
35	.3	3.2	-58.9	12.6	78.1	2.8	1.1	34
36	.9	1.0	-57.8	14.3	59.5	1.1	1.7	34
37	1.8	1.8	-182.4	25.3	185.4	1.1	.7	38
38	.3	12.3	-67.4	18.0	69.3	10.7	1.3	34
39	.9	5.7	-136.5	40.7	142.4	2.5	0.0	42
40	.6	2.0	-76.2	76.9	108.2	1.1	.3	49
41	.3	4.7	-76.5	127.7	148.5	1.9	.3	53
42	1.1	1.1	-17.2	29.0	33.7	1.9	.4	36
43	.2	7.7	-72.4	126.0	165.3	3.3	.7	53
44	.4	3.5	-46.3	89.0	181.2	2.1	.5	55
45	.5	2.7	-19.5	37.6	122.3	3.9	.8	36
46	.6	2.4	-27.6	69.7	75.3	1.9	1.1	59
47	.7	1.6	-32.5	87.2	93.2	1.1	.8	57
48	.5	1.5	-38.1	89.2	94.2	1.0	.8	57
49	.2	7.3	-23.7	72.8	76.3	5.8	1.5	55
50	.5	1.4	-13.7	89.4	90.4	1.0	0.8	66

51	4	1.4	-7.6	64.7	65.1	1.8	-1.4	64
52	-6	1.4	-4	41.2	41.2	2.1	0	62
53	8	2.1	-1	36.8	36.8	3.7	-1.7	62
54	2.4	1.7	39.8	91.9	99.8	1.1	8.0	70
55	1.6	1.8	39.8	93.6	101.7	1.1	3	70
56	-9	1.5	42.3	94.5	103.6	.9	1.3	-9
57	1.5	1.6	46.1	103.1	112.9	.9	-1.5	70
58	-8	3.4	48.6	95.1	106.3	1.9	1.0	-8
59	8	1.4	47.8	88.9	108.7	.9	1.3	-8
60	-9	1.7	56.6	106.3	120.4	.9	-7	-9
61	-9	3.5	54.6	114.7	118.1	1.8	1.0	-9
62	2.1	2.9	44.6	85.6	96.5	1.8	1.3	-2.1
63	3.1	1.4	39.8	71.8	82.3	1.1	1.3	3.1
64	1.1	2.1	53.1	92.1	106.4	1.2	.2	-1.1
65	2.7	1.3	56.6	93.4	109.2	.7	0.0	-2.7
66	2.5	1.3	57.5	95.0	111.1	.7	0.0	-2.5
67	3.3	1.1	48.1	58.1	64.2	1.1	2.7	-3.3
68	3.6	1.3	46.8	57.4	73.6	1.1	1.7	3.6
69	2.9	1.1	38.9	82.7	82.3	1.1	0.0	2.9
70	2.8	1.4	52.4	63.1	82.4	1.1	2.7	-2.8
71	3.4	1.3	48.2	58.8	75.4	1.1	1.7	-3.4
72	3.9	1.8	45.6	52.9	69.3	.9	2.0	-3.9
73	1.2	1.6	55.8	62.7	83.3	1.1	1.3	-1.2
74	.7	5.4	96.5	108.5	145.2	2.3	1.8	-7
75	-9	2.7	64.3	69.4	94.5	1.8	2.5	-9
76	4.4	1.8	48.1	51.9	70.5	.9	0.0	4.4
77	1.2	2.9	68.1	73.6	100.3	1.8	1.3	-1.2
78	1.2	1.1	50.6	54.7	74.5	.9	2.2	1.2
79	1.0	1.5	69.7	75.3	102.5	.9	1.0	-1.0
80	3.5	1.3	56.6	59.3	82.3	1.0	2.3	3.5
81	.5	6.7	61.9	65.6	90.3	4.6	1.2	-5
82	3.1	1.3	55.0	55.7	78.3	1.1	0.0	-3.1
83	2.8	1.3	53.7	54.3	76.4	1.1	1.0	-2.8
84	1.1	3.2	67.6	69.5	97.0	2.0	2.8	-1.1
85	2.9	1.3	68.7	59.2	84.5	1.8	1.0	-2.9
86	1.1	1.7	76.1	74.3	106.4	1.0	2.5	1.1
87	1.1	5.6	84.9	82.8	118.5	2.9	.9	-1.1
88	1.8	1.4	63.7	68.1	97.3	1.0	.8	-1.8
89	1.5	1.5	67.8	64.0	93.2	1.0	0.0	-1.5
90	1.8	4.8	92.0	86.8	126.5	1.9	0.0	-1.8
91	1.9	2.0	93.7	88.4	128.3	1.0	0.0	-1.9
92	1.7	2.1	96.5	91.0	132.6	1.0	0.0	1.7
93	1.7	2.2	99.2	93.6	136.4	1.8	1.0	1.7
94	2.8	1.6	75.8	69.1	102.6	1.0	2.3	-2.8
95	2.3	1.6	73.1	66.6	98.3	1.0	1.8	-2.3

VELOCITY SPREAD MAXIMA ATTRIBUTES

DAY MONTH SS ELE AZM1 AZM2
226 1933 40 1.2 116.2 116.2

ID	SPREAD (M/3)	AREA (KM2)	EAST (KM)	NORTH (KM)	RANGE (KM)	AREA ELEMENTS	FIXED CONTOUR REFERENCE
1	1.2	1.6	14.1	-19.3	23.9	6.0	5
2	1.7	1.5	-16.1	-51.4	62.8	1.6	9
3	1.9	2.8	-18.5	-53.7	66.0	2.5	0
4	1.3	2.5	-131.9	-68.2	148.5	1.1	13
5	2.2	1.9	-122.4	-57.9	135.4	.9	18
6	1.5	4.5	-117.7	-53.5	129.3	2.1	13
7	2.9	9.9	-129.0	-55.0	140.5	3.9	18
8	1.8	2.0	-115.7	-50.0	126.0	1.0	18
9	2.2	1.6	-103.5	-42.7	112.0	1.0	18
10	1.3	1.3	-79.1	-38.6	105.4	1.1	18
11	2.8	9.3	-131.6	-51.1	141.2	4.0	18
12	2.8	3.3	-108.0	-40.2	115.3	1.8	18
13	2.4	13.9	-112.8	-43.7	121.0	7.0	18
14	2.1	14.5	-95.8	-30.8	108.6	6.8	18
15	3.1	6.6	-133.6	-42.1	148.1	2.9	18
16	2.3	17.6	-101.7	-34.5	107.4	10.0	18
17	2.8	21.6	-136.8	-45.9	144.3	9.1	18
18	1.8	1.3	-16.7	-10.7	36.4	3.0	19
19	2.7	4.6	-139.1	-38.5	144.3	1.9	18
20	1.6	7.5	-129.7	-31.5	127.6	3.6	18
21	2.6	19.2	-132.4	-30.7	135.9	8.6	18
22	2.6	15.2	-131.0	-32.3	134.6	6.9	18
23	2.7	5.7	-130.2	-19.9	151.7	2.6	19
24	1.9	1.9	-37.0	-2.6	37.1	3.1	25
25	2.2	6.3	-133.1	4.0	133.2	2.9	31
26	1.3	2.5	-138.6	6.8	138.7	1.2	31
27	1.7	4.7	-67.1	8.1	67.6	4.2	34
28	1.7	2.1	-56.5	13.7	58.8	2.3	37
29	1.6	5.6	-103.1	24.9	106.8	3.2	38
30	1.5	4.8	-76.8	39.3	77.2	3.8	34
31	1.8	1.7	-124.0	35.1	128.9	.8	41
32	1.9	3.7	-137.1	36.8	142.5	1.6	42
33	2.7	1.1	-17.2	13.0	33.4	1.7	36
34	1.4	3.5	-59.3	24.7	73.6	4.7	34
35	1.1	1.1	-26.7	12.6	29.5	2.2	45
36	1.9	6.9	-33.6	17.1	37.7	11.2	36
37	2.5	3.5	-10.4	20.5	37.8	5.8	36
38	1.2	2.2	-87.2	73.6	111.1	1.2	47
39	1.1	2.2	-16.7	75.7	107.7	1.2	49
40	1.7	1.4	-51.1	51.6	72.5	1.1	48
41	2.3	1.3	-21.9	25.7	33.9	2.3	36
42	2.0	2.6	-18.7	24.8	31.0	5.2	36
43	2.2	7.0	-76.8	125.0	146.7	2.9	53
44	1.6	3.0	-15.5	25.4	29.4	6.2	35
45	1.0	1.7	-46.0	68.6	108.7	1.1	55
46	1.7	1.4	-38.5	72.3	58.6	1.0	54
47	1.7	1.2	-16.3	76.3	56.7	.9	58
48	2.0	3.3	-12.1	77.4	29.9	6.8	36
49	1.2	2.5	-10.5	71.1	77.3	2.0	59
50	1.8	3.1	-35.0	65.9	92.8	2.8	57
51	1.7	7.5	-31.5	82.8	88.6	5.2	57

52	1.4	7.4	-24.0	63.2	67.6	6.7	60
53	1.6	4.5	-9.9	30.3	31.9	9.7	36
54	1.7	9.7	-24.4	73.1	77.0	7.7	53
55	1.7	1.0	-8.1	30.0	31.0	1.9	36
56	1.6	2.9	-14.5	90.2	91.4	1.9	66
57	2.2	1.5	-14.3	93.1	94.2	1.0	65
58	1.8	1.0	-7.6	64.7	65.1	1.0	64
59	1.3	9.4	-8.5	62.6	63.2	0.1	64
60	1.3	2.0	-3.4	53.2	53.3	1.9	67
61	1.7	1.2	-4.4	23.6	23.6	3.1	68
62	2.0	1.1	3.3	25.7	25.7	2.7	69
63	1.9	3.0	3.8	22.5	22.5	5.0	70
64	2.4	1.8	12.1	35.7	35.5	2.7	73
65	1.9	4.5	17.7	54.8	57.5	4.7	74
66	1.7	1.6	37.6	92.4	99.8	9.9	78
67	1.7	1.7	36.3	90.1	47.9	1.1	76
68	1.7	5.3	54.5	104.7	113.8	3.2	78
69	1.8	1.4	38.6	85.8	95.1	9.9	78
70	1.7	1.7	48.8	109.1	119.5	9.9	78
71	1.8	3.4	52.1	106.0	118.1	1.8	76
72	1.5	3.6	49.2	104.5	115.5	4.6	78
73	1.9	7.3	45.0	98.0	48.9	4.6	78
74	2.2	3.0	48.4	91.0	103.1	1.8	78
75	2.3	3.1	40.9	72.2	82.9	2.3	81
76	1.7	25.3	52.3	98.2	111.5	13.9	78
77	1.7	1.3	38.5	65.1	75.7	2.6	82
78	1.0	1.1	44.8	64.2	78.3	9.9	83
79	1.0	2.4	52.2	71.0	86.1	1.9	84
80	3.0	1.1	42.1	54.5	58.9	1.0	55
81	3.0	2.1	40.1	50.8	64.7	2.0	85
82	2.9	12.7	95.1	111.4	147.1	5.3	90
83	2.6	12.4	51.2	62.0	80.5	9.4	85
84	1.9	3.9	58.5	77.0	103.1	2.3	85
85	2.7	2.6	57.6	60.3	43.4	1.9	85
86	2.5	2.3	100.0	104.7	144.8	1.0	50
87	2.4	12.6	95.7	96.7	121.9	6.3	85
88	2.8	4.9	73.4	71.7	102.6	2.9	85
89	2.3	8.4	94.6	92.3	132.1	3.9	85
90	2.5	2.0	30.3	68.7	127.0	1.0	85
91	2.5	2.3	92.2	50.0	120.9	1.0	85
TOTAL IDS= 101 15 29 28							
TOP RECORD UNITS							
NO OF RECORDS/RADIAL 4							
CELL WIDTH 937.2 METERS							
PRF 794.0							
TOTAL IDS= 1 1 1 1							
NO OF RECORDS/RADIAL 4							
CELL WIDTH 937.2 METERS							
PRF 794.0							

FIXED CONTOUR ATTRIBUTES

DAY	HHMM	SS	FLE	42M1	42M2	THRESHOLD	AREA (KM ²)	REFLECTIVITY (DBZ)	LOCATION	APX	TOTAL	AVERAGE	FIXED
226	1914	38	6.1	160.1	111.0								
TO	THRESHOLD	AREA (KM ²)	REFLECTIVITY (DBZ)	EAST (KM)	NORTH (KM)	RANGE RESOLUTION (KM)	ELEMENTS	PRECIP (TONS/HRI)	PRECIP (MM/HRI)	CONTOUR	REFERENCE		
1	20	17.32	21.4	-31.0	-50.1	59.0	18.9	3.2		1			
2	20	2.96	21.0	-34.6	-45.0	56.8	3.2			3			
3	20	1.10	21.0	-50.7	6.8	51.1	1.3			4			
4	20	548.58	43.0	-25.8	21.2	33.3	1005.8			7			
5	20	31.69	22.1	1.6	22.3	22.3	86.8			-1			
6	20	1.15	21.0	-3.5	56.3	67.0	1.1			15			
7	20	12.57	21.1	-6.3	67.0	67.4	11.4			12			
8	20	1.47	21.5	-4.1	42.4	62.6	2.1			13			
9	20	11.22	21.1	-1.3	64.0	64.0	10.7			14			
10	20	15.17	21.9	5.1	47.3	47.8	20.7			17			
11	20	1.50	21.5	6.4	25.1	25.9	3.5			18			
12	20	2.61	21.3	10.2	20.3	22.7	7.0			20			
13	20	11.93	22.5	22.0	43.5	40.9	14.9			21			
14	20	2.19	21.8	14.5	21.3	26.2	5.1			23			
15	20	111.17	28.3	70.4	67.3	97.8	69.5			27			
16	20	20.35	22.3	65.4	76.7	100.3	12.5			28			
17	20	341.36	34.3	44.3	53.3	70.1	297.8			26			
18	20	1.05	21.0	22.2	20.3	30.5	2.1			33			
19	20	15.07	22.7	34.3	38.5	52.1	17.7			30			
20	20	2.13	22.0	96.8	31.2	136.5	1.8			34			
21	20	67.00	26.6	73.3	79.3	106.0	49.2			32			
1	40	145.21	43.1	-27.0	20.1	33.6	269.5			7			
2	40	11.12	46.0	-10.9	31.4	33.2	20.4			7			
3	40	9.74	45.6	41.0	50.1	64.8	9.2			28			

WIND DATA

DAY HMM SS FLE AZM1 AZM2
226 1314 38 4.1 160.1 111.0

AVERAGE		TOTAL	AVERAGE		VELOCITY		JEL
HEIGHT	REFLECTIVITY	REFLECTIVITY	U	V	VARIANCE		
(MM)	(DBZ)	(DBZ-KM**2)	(M/SEC)	(M/SEC)	(M/SEC)**2)		
4	22.0	78.7	0.0	0.0	.1		-.08819E-19
5	21.5	209.2	-2.7	-7.1	4.8		.76765E-01
7	21.6	1161.1	0.0	1.6	.3		-.35827E-14
9	33.3	258537.7	6.4	0.0	11.2		-.35827E-14

PEAK DETECTED CELL ATTRIBUTES

DAY NAME SS FLE 2701 42M2
226 1984 38 6.1 163.1 111.0

ID	REFLECTIVITY (DBZ)	AREA (KM ²)	LOCATION (LAT, LONG)	AREA RESOLUTION ELEMENTS	AVERAGE VELOCITY SPREAD (M/S)	AVERAGE RADIAL VELOCITY SPREAD (M/S)	AVERAGE TANGENTIAL VELOCITY SPREAD (M/S)	MEAN FIXED CONTOUR REFERENCE
1	21.4	15.4	-52.2 16.3	16.3	1.91	-0.76	-0.13	1
2	21.3	15.4	-52.2 16.3	16.3	1.91	-0.76	-0.13	1
3	21.3	15.4	-52.2 16.3	16.3	1.91	-0.76	-0.13	1
4	21.3	15.4	-52.2 16.3	16.3	1.91	-0.76	-0.13	1
5	21.3	15.4	-52.2 16.3	16.3	1.91	-0.76	-0.13	1
6	21.3	15.4	-52.2 16.3	16.3	1.91	-0.76	-0.13	1
7	21.3	15.4	-52.2 16.3	16.3	1.91	-0.76	-0.13	1
8	21.3	15.4	-52.2 16.3	16.3	1.91	-0.76	-0.13	1
9	21.3	15.4	-52.2 16.3	16.3	1.91	-0.76	-0.13	1
10	21.3	15.4	-52.2 16.3	16.3	1.91	-0.76	-0.13	1
11	21.3	15.4	-52.2 16.3	16.3	1.91	-0.76	-0.13	1
12	21.3	15.4	-52.2 16.3	16.3	1.91	-0.76	-0.13	1
13	21.3	15.4	-52.2 16.3	16.3	1.91	-0.76	-0.13	1
14	21.3	15.4	-52.2 16.3	16.3	1.91	-0.76	-0.13	1
15	21.3	15.4	-52.2 16.3	16.3	1.91	-0.76	-0.13	1
16	21.3	15.4	-52.2 16.3	16.3	1.91	-0.76	-0.13	1
17	21.3	15.4	-52.2 16.3	16.3	1.91	-0.76	-0.13	1
18	21.3	15.4	-52.2 16.3	16.3	1.91	-0.76	-0.13	1
19	21.3	15.4	-52.2 16.3	16.3	1.91	-0.76	-0.13	1
20	21.3	15.4	-52.2 16.3	16.3	1.91	-0.76	-0.13	1
21	21.3	15.4	-52.2 16.3	16.3	1.91	-0.76	-0.13	1
22	21.3	15.4	-52.2 16.3	16.3	1.91	-0.76	-0.13	1

YANGTSE RIVER MAXIMA ATTRIBUTES

DAY HMMH SS ELE AZM1 AZM2
226 1934 38 5.1 168.1 111.8

ID	MAGNITUDE		LOCATION		AREA		RANGE		RESOLUTION		AREA		VELOCITY		AVERAGE		SHEAR		FIXED	
	SHEAR (M/S/KM)	AREA (KM*2)	FIRST (KM)	NORTH (KM)	AREA (KM)	AREA (KM)	RANGE (KM)	RANGE (KM)	RESOLUTION (KM)	RESOLUTION (KM)	AREA (KM)	AREA (KM)	VELOCITY (M/S)	VELOCITY (M/S)	AVERAGE (M/S)	AVERAGE (M/S)	SHEAR (M/S/KM)	SHEAR (M/S/KM)	FIXED REFERENCE	FIXED REFERENCE
1	3.2	1.5	-31.1	-48.8	35.7	35.7	37.2	37.2	1.6	1.6	1.6	1.6	2.1	2.1	-1.2	-1.2	-1.4	-1.4	7	7
2	1.4	1.0	-25.5	25.5	35.7	35.7	37.2	37.2	1.6	1.6	1.6	1.6	2.1	2.1	-1.2	-1.2	-1.4	-1.4	7	7
3	1.4	1.0	-25.5	25.5	35.7	35.7	37.2	37.2	1.6	1.6	1.6	1.6	2.1	2.1	-1.2	-1.2	-1.4	-1.4	7	7
4	1.4	1.0	-25.5	25.5	35.7	35.7	37.2	37.2	1.6	1.6	1.6	1.6	2.1	2.1	-1.2	-1.2	-1.4	-1.4	7	7
5	1.4	1.0	-25.5	25.5	35.7	35.7	37.2	37.2	1.6	1.6	1.6	1.6	2.1	2.1	-1.2	-1.2	-1.4	-1.4	7	7
6	1.4	1.0	-25.5	25.5	35.7	35.7	37.2	37.2	1.6	1.6	1.6	1.6	2.1	2.1	-1.2	-1.2	-1.4	-1.4	7	7
7	1.4	1.0	-25.5	25.5	35.7	35.7	37.2	37.2	1.6	1.6	1.6	1.6	2.1	2.1	-1.2	-1.2	-1.4	-1.4	7	7
8	1.4	1.0	-25.5	25.5	35.7	35.7	37.2	37.2	1.6	1.6	1.6	1.6	2.1	2.1	-1.2	-1.2	-1.4	-1.4	7	7
9	1.4	1.0	-25.5	25.5	35.7	35.7	37.2	37.2	1.6	1.6	1.6	1.6	2.1	2.1	-1.2	-1.2	-1.4	-1.4	7	7
10	1.4	1.0	-25.5	25.5	35.7	35.7	37.2	37.2	1.6	1.6	1.6	1.6	2.1	2.1	-1.2	-1.2	-1.4	-1.4	7	7
11	1.4	1.0	-25.5	25.5	35.7	35.7	37.2	37.2	1.6	1.6	1.6	1.6	2.1	2.1	-1.2	-1.2	-1.4	-1.4	7	7
12	1.4	1.0	-25.5	25.5	35.7	35.7	37.2	37.2	1.6	1.6	1.6	1.6	2.1	2.1	-1.2	-1.2	-1.4	-1.4	7	7
13	1.4	1.0	-25.5	25.5	35.7	35.7	37.2	37.2	1.6	1.6	1.6	1.6	2.1	2.1	-1.2	-1.2	-1.4	-1.4	7	7
14	1.4	1.0	-25.5	25.5	35.7	35.7	37.2	37.2	1.6	1.6	1.6	1.6	2.1	2.1	-1.2	-1.2	-1.4	-1.4	7	7
15	1.4	1.0	-25.5	25.5	35.7	35.7	37.2	37.2	1.6	1.6	1.6	1.6	2.1	2.1	-1.2	-1.2	-1.4	-1.4	7	7
16	1.4	1.0	-25.5	25.5	35.7	35.7	37.2	37.2	1.6	1.6	1.6	1.6	2.1	2.1	-1.2	-1.2	-1.4	-1.4	7	7
17	1.4	1.0	-25.5	25.5	35.7	35.7	37.2	37.2	1.6	1.6	1.6	1.6	2.1	2.1	-1.2	-1.2	-1.4	-1.4	7	7
18	1.4	1.0	-25.5	25.5	35.7	35.7	37.2	37.2	1.6	1.6	1.6	1.6	2.1	2.1	-1.2	-1.2	-1.4	-1.4	7	7
19	1.4	1.0	-25.5	25.5	35.7	35.7	37.2	37.2	1.6	1.6	1.6	1.6	2.1	2.1	-1.2	-1.2	-1.4	-1.4	7	7
20	1.4	1.0	-25.5	25.5	35.7	35.7	37.2	37.2	1.6	1.6	1.6	1.6	2.1	2.1	-1.2	-1.2	-1.4	-1.4	7	7
21	1.4	1.0	-25.5	25.5	35.7	35.7	37.2	37.2	1.6	1.6	1.6	1.6	2.1	2.1	-1.2	-1.2	-1.4	-1.4	7	7
22	1.4	1.0	-25.5	25.5	35.7	35.7	37.2	37.2	1.6	1.6	1.6	1.6	2.1	2.1	-1.2	-1.2	-1.4	-1.4	7	7
23	1.4	1.0	-25.5	25.5	35.7	35.7	37.2	37.2	1.6	1.6	1.6	1.6	2.1	2.1	-1.2	-1.2	-1.4	-1.4	7	7
24	1.4	1.0	-25.5	25.5	35.7	35.7	37.2	37.2	1.6	1.6	1.6	1.6	2.1	2.1	-1.2	-1.2	-1.4	-1.4	7	7
25	1.4	1.0	-25.5	25.5	35.7	35.7	37.2	37.2	1.6	1.6	1.6	1.6	2.1	2.1	-1.2	-1.2	-1.4	-1.4	7	7
26	1.4	1.0	-25.5	25.5	35.7	35.7	37.2	37.2	1.6	1.6	1.6	1.6	2.1	2.1	-1.2	-1.2	-1.4	-1.4	7	7
27	1.4	1.0	-25.5	25.5	35.7	35.7	37.2	37.2	1.6	1.6	1.6	1.6	2.1	2.1	-1.2	-1.2	-1.4	-1.4	7	7
28	1.4	1.0	-25.5	25.5	35.7	35.7	37.2	37.2	1.6	1.6	1.6	1.6	2.1	2.1	-1.2	-1.2	-1.4	-1.4	7	7
29	1.4	1.0	-25.5	25.5	35.7	35.7	37.2	37.2	1.6	1.6	1.6	1.6	2.1	2.1	-1.2	-1.2	-1.4	-1.4	7	7
30	1.4	1.0	-25.5	25.5	35.7	35.7	37.2	37.2	1.6	1.6	1.6	1.6	2.1	2.1	-1.2	-1.2	-1.4	-1.4	7	7
31	1.4	1.0	-25.5	25.5	35.7	35.7	37.2	37.2	1.6	1.6	1.6	1.6	2.1	2.1	-1.2	-1.2	-1.4	-1.4	7	7
32	1.4	1.0	-25.5	25.5	35.7	35.7	37.2	37.2	1.6	1.6	1.6	1.6	2.1	2.1	-1.2	-1.2	-1.4	-1.4	7	7
33	1.4	1.0	-25.5	25.5	35.7	35.7	37.2	37.2	1.6	1.6	1.6	1.6	2.1	2.1	-1.2	-1.2	-1.4	-1.4	7	7
34	1.4	1.0	-25.5	25.5	35.7	35.7	37.2	37.2	1.6	1.6	1.6	1.6	2.1	2.1	-1.2	-1.2	-1.4	-1.4	7	7
35	1.4	1.0	-25.5	25.5	35.7	35.7	37.2	37.2	1.6	1.6	1.6	1.6	2.1	2.1	-1.2	-1.2	-1.4	-1.4	7	7
36	1.4	1.0	-25.5	25.5	35.7	35.7	37.2	37.2	1.6	1.6	1.6	1.6	2.1	2.1	-1.2	-1.2	-1.4	-1.4	7	7
37	1.4	1.0	-25.5	25.5	35.7	35.7	37.2	37.2	1.6	1.6	1.6	1.6	2.1	2.1	-1.2	-1.2	-1.4	-1.4	7	7
38	1.4	1.0	-25.5	25.5	35.7	35.7	37.2	37.2	1.6	1.6	1.6	1.6	2.1	2.1	-1.2	-1.2	-1.4	-1.4	7	7
39	1.4	1.0	-25.5	25.5	35.7	35.7	37.2	37.2	1.6	1.6	1.6	1.6	2.1	2.1	-1.2	-1.2	-1.4	-1.4	7	7
40	1.4	1.0	-25.5	25.5	35.7	35.7	37.2	37.2	1.6	1.6	1.6	1.6	2.1	2.1	-1.2	-1.2	-1.4	-1.4	7	7
41	1.4	1.0	-25.5	25.5	35.7	35.7	37.2	37.2	1.6	1.6	1.6	1.6	2.1	2.1	-1.2	-1.2	-1.4	-1.4	7	7
42	1.4	1.0	-25.5	25.5	35.7	35.7	37.2	37.2	1.6	1.6	1.6	1.6	2.1	2.1	-1.2	-1.2	-1.4	-1.4	7	7

102 0 PROGRAM EXTRAC

VELOCITY SPREAD MAXIMA ATTRIBUTES

DAY MONTH SS ELF AZMI AZPZ
226 1974 36 6.1 165.1 111.0

ID	SPEED (KPH)	AREA (KPH)	LOCATION		RANGE (KM)	RESOLUTION ELEMENTS	AREA ELEMENTS	FIXED CONTOUR REFERENCE
			EAST (KPH)	NORTH (KPH)				
1	2.0	5.2	-10.7	-43.1	57.9	6.5	1	1
2	2.2	1.1	-36.2	-46.3	57.6	1.1	3	3
3	1.2	1.1	-53.7	6.0	51.1	1.3	4	4
4	2.4	3.6	-33.2	13.9	36.5	6.2	7	7
5	2.7	3.6	-32.2	19.0	37.9	5.2	7	7
6	2.2	3.6	-27.6	17.6	32.7	5.8	7	7
7	2.4	2.7	-28.5	21.0	35.4	4.7	7	7
8	1.4	6.3	-34.7	24.3	42.4	9.1	7	7
9	2.2	1.1	-25.1	21.9	33.3	2.1	7	7
10	1.8	6.5	-25.6	28.9	35.5	7.5	7	7
11	2.6	2.1	-15.7	25.3	33.3	2.0	7	7
12	2.3	1.1	-18.2	35.1	44.1	4.0	7	7
13	1.2	2.3	-18.5	40.9	33.4	5.3	7	7
14	1.3	3.2	-10.4	21.8	33.4	5.3	7	7
15	2.1	1.1	-17.3	32.3	33.3	1.9	7	7
16	1.6	7.3	-25.1	35.1	35.5	12.1	7	7
17	1.1	1.5	-8.1	42.4	42.5	2.1	13	13
18	1.7	5.2	-3.5	66.9	67.3	1.1	15	15
19	1.2	11.7	-2.4	33.6	30.6	23.2	7	7
20	1.4	5.4	-5	23.7	23.8	13.8	13	13
21	1.1	2.2	2.4	4.6	47.9	2.8	17	17
22	1.2	3.6	7.3	47.4	46.9	12.0	17	17
23	1.6	1.5	6.3	25.1	25.3	3.5	18	18
24	1.3	7.3	22.5	47.5	48.9	9.8	21	21
25	1.0	1.6	10.4	20.3	22.8	4.3	20	20
26	1.4	2.2	14.5	22.0	26.3	5.1	23	23
27	2.7	4.6	50.2	55.0	63.3	3.4	26	26
28	2.5	7.2	63.0	58.3	71.4	2.7	26	26
29	2.7	1.4	66.2	78.4	102.5	1.1	28	28
30	3.0	1.4	68.6	81.3	105.4	1.1	32	32
31	2.6	10.0	42.3	50.3	65.7	5.3	25	25
32	2.2	3.6	57.0	74.6	109.3	2.1	28	28
33	2.6	11.6	53.5	81.5	115.3	9.7	26	26
34	2.4	7.3	77.1	90.9	134.4	4.0	30	30
35	3.0	33.4	75.3	85.3	110.1	16.5	32	32
36	2.8	1.1	22.2	20.4	33.5	2.1	33	33
37	2.3	10.3	71.2	87.4	98.0	10.2	27	27

TOTAL IDS= 34 11 16 17
FOR RECD ON UNIT 1

NO OF RECORDS/RADIAL 4

CELL WIDTH 937.2 METERS

PDF

794.0

FIXED CONTOUR ATTRIBUTES

DAY HMM SS ELE AZM1 AZM2
226 1975 34 7.3 115.0 115.0

ID	THRESHOLD	AREA (KM ²)	REFLECTIVITY (DBZ)	LOCATION		RANGE (KM)	RESOLUTION (KM)	PRECIP (TONS/HR)	TOTAL PRECIP (MM/HR)	AVERAGE PRECIP (MM/HR)	FIXED CONTOUR REFERENCE
				EAST (KM)	NORTH (KM)						
1	20	2.29	21.0	-27.1	-47.1	54.9	2.5	2.5			1
2	20	575.39	42.5	-24.3	21.3	32.7	1074.8	7			7
3	20	1.44	22.0	-4.3	38.3	38.4	2.3	2.3			9
4	20	1.27	21.0	-24.3	-32.1	45.3	1.9	1.9			5
5	20	2.04	21.5	0	20.3	20.3	6.2	6.2			-11
6	20	23.35	23.8	15.3	22.2	27.0	53.8	19			19
7	20	11.33	22.1	4.5	46.3	47.0	14.7	13			13
8	20	14.33	23.0	22.8	42.3	48.1	19.0	20			20
9	20	18.75	22.1	8.3	45.4	46.2	24.5	16			16
10	20	4.51	22.2	26.2	38.3	45.3	5.3	21			21
11	20	31.12	23.1	5.1	24.3	24.8	76.7	-18			-18
12	20	144.52	33.0	44.2	53.3	59.3	127.5	22			22
13	20	51.71	25.9	55.2	63.3	82.1	46.0	23			23
14	20	4.35	22.6	35.5	37.0	53.3	5.2	25			25
15	20	1.72	21.0	32.2	39.7	54.4	1.9	26			26
1	40	144.10	45.0	-25.3	20.1	32.8	258.5	7			7
2	40	8.66	45.9	-10.4	31.5	33.2	15.9	7			7
3	40	2.63	44.6	42.1	53.3	55.6	2.5	22			22

WIND DATA

DAY	HR	SS	ELE	AZM1	AZM2
226	1935	38	7.3	115.0	115.0

HEIGHT	AVERAGE	TOTAL	AVERAGE	AVERAGE	VELOCITY	DEL
REFLECTIVITY	DEFLECTIVITY	U	V	VARIANCE		
(DBZ)	(DBZ-KM ²)	(M/SEC)	(M/SEC)	(M/SEC ²)		
5	21.0	1337.0	3.2	0.0	1.5	-.00019E-15
6	22.0	854.5	1.5	-8.3	11.8	-.59763E-01
7	21.0	216.4	0.0	1.6	1.1	-.00018E-15
10	31.2	122873.5	215.5	-155.3	27.6	.38193E-02

PEAK DETECTED CELL ATTRIBUTES

DAY MONTH SS ELE AZM1 AZM2
226 1985 38 7.8 115.0 115.0

ID	REFLECTIVITY (DBZ)	AREA (KM*2)	LOCATION		RANGE (KM)	AREA RESOLUTION ELEMENTS	AVERAGE VELOCITY SPREAD (M/S)	AVERAGE		AVERAGE RADIAL VELOCITY (M/S)	MEAN FIXED CONTOUR REFERENCE
			EAST (KM)	NORTH (KM)				TANGENTIAL SHEAR (M/S/KM)	RADIAL SHEAR (M/S/KM)		
1	52.7	3.1	-32.3	13.0	34.0	5.4	2.21	-.34	-.50	-2.06	7
2	52.4	2.0	-32.0	18.6	37.0	3.3	2.33	-1.32	.36	.23	7
3	52.0	6.2	-26.8	18.6	32.6	11.5	2.20	2.12	-1.07	-.53	7
4	54.5	2.0	-24.1	21.6	32.3	3.8	1.72	2.36	1.43	2.06	7
5	50.4	3.6	-18.6	24.6	31.0	7.1	1.71	.85	1.27	1.93	7
6	50.0	1.1	-11.1	31.4	33.3	2.0	1.43	2.21	.41	1.44	7
7	22.7	5.9	8.6	47.0	47.2	8.9	.98	-.19	-.29	-.28	13
8	22.1	18.7	8.8	45.3	46.2	24.8	1.02	-.11	-.21	-.59	16
9	25.5	2.4	8.2	24.9	25.7	5.3	.82	-.15	-.35	-0.53	16
10	24.0	7.8	23.1	42.2	40.1	9.9	.70	-.13	.08	1.01	20
11	22.7	4.5	26.2	38.8	46.8	5.9	.76	-.02	-.11	.87	21
12	36.6	3.0	46.0	56.4	72.8	2.5	2.56	-.30	2.07	1.64	22
13	25.5	6.0	16.4	22.4	27.8	13.2	.63	-.28	-.26	.74	13
14	33.5	2.9	52.9	62.1	61.5	2.1	2.25	.42	-2.50	-4.03	23
15	27.3	4.1	56.8	64.2	85.7	2.9	2.23	-.96	-.00	-8.18	23
16	22.6	4.3	35.4	37.0	51.2	5.2	1.32	.12	-.15	-.62	25
17	24.3	14.0	59.3	56.1	61.7	10.5	1.51	.16	-.33	-5.21	23

TANGENTIAL SHEAR MAXIMA ATTRIBUTES

DAY HMM SS ELE AZMI A7M2
226 1936 38 7.0 115.0 115.0

ID	MAGNITUDE (M/S/KM)	XPEA (KM*2)	LOCATION		RANGE (KM)	AREA RESOLUTION ELEMENTS (M/S)	AVERAGE VELOCITY SPREAD	AVERAGE SHEAR (M/S/KM)	FIXED CONTOUR REFERENCE
			EAST	NORTH					
1	2.8	1.9	-33.4	25.3	40.7	2.0	1.6	-2.8	7
2	2.7	2.8	-28.7	25.4	39.4	4.4	1.6	-2.7	7
3	2.9	2.6	-26.5	26.8	37.7	4.2	1.6	-2.9	7
4	3.6	1.6	-19.3	24.3	31.1	3.2	1.6	3.6	7
5	2.6	1.1	-17.5	25.2	30.3	2.1	2.1	-2.3	7
6	2.7	2.0	-23.6	35.2	42.6	2.9	1.1	-2.7	7
7	2.9	1.3	-21.2	35.4	41.2	1.9	1.5	-2.9	7
8	2.0	1.1	-18.3	30.0	35.1	1.9	1.5	-2.1	7
9	2.1	1.5	-11.9	30.1	32.4	2.3	1.3	-2.1	7
10	2.7	1.4	-10.7	26.5	24.5	3.1	1.1	-2.7	7
11	2.9	7.4	-14.2	36.1	38.7	11.7	1.1	-2.9	7
12	1.9	1.2	-11.8	36.5	38.4	1.9	1.1	-1.9	7
13	1.8	1.3	-6.4	36.0	36.5	2.1	1.2	1.6	7
14	1.9	1.1	-4.4	33.0	33.1	2.0	1.3	1.9	7
15	2.6	1.6	1.1	24.1	24.1	4.0	1.3	-2.6	19
16	2.7	1.1	7.1	24.5	25.3	2.7	1.0	-2.7	18
17	2.5	1.8	14.5	22.8	27.1	4.0	1.5	-2.5	19
18	2.3	1.5	27.0	30.3	46.3	1.5	1.0	-2.3	21
19	2.7	1.3	16.6	22.7	24.1	3.5	1.7	-2.7	19
20	3.1	1.1	45.0	58.2	73.5	1.9	2.3	-3.1	22
21	2.5	1.3	41.8	52.4	67.3	1.1	2.0	-2.5	22
22	2.7	1.4	53.2	62.4	62.0	1.1	2.3	-2.7	23
23	2.3	1.0	43.1	46.8	65.1	1.0	2.1	-2.3	22
24	1.8	1.3	52.5	55.3	79.2	1.0	2.5	-1.8	23
25	2.8	1.3	56.2	63.5	84.9	1.0	1.8	-2.8	23
26	3.3	1.3	45.9	50.1	67.3	1.1	2.2	3.3	22
27	2.3	1.3	38.5	52.9	71.7	1.1	2.2	-2.3	22
28	2.3	1.0	19.5	21.3	29.1	2.2	1.0	-2.3	19
29	1.1	1.3	56.3	57.0	88.1	1.0	1.7	-1.1	23
30	1.4	1.6	36.1	36.6	51.4	1.9	1.3	1.4	25
31	1.9	1.1	45.7	50.3	70.9	1.0	2.2	1.9	22
32	1.0	1.2	60.2	57.0	82.3	1.9	1.9	-1.0	23

VELOCITY SPREAD MAXIMA ATTRIBUTES

DAY HHMM SS				ELE		AZM1		AZM2	
226 1935 38				7.0		115.0		115.0	
ID	SPREAD (M/ST)	AREA (KM2)	LOCATION		RANGE (KM)	RESOLUTION ELEMENTS	AREA		FIXED CONTOUR REFERENCE
			EAST (KM)	NORTH (KM)			NORTH ELEMENTS	WEST ELEMENTS	
1	1.7	1.6	-28.1	-47.6	55.3	1.8			1
2	2.6	3.3	-33.6	13.6	36.3	5.4			7
3	2.5	2.9	-28.4	18.2	33.7	5.2			7
4	2.6	3.3	-38.1	20.4	36.4	5.6			7
5	2.4	4.7	-25.2	20.3	32.4	3.0			7
6	2.0	1.5	-23.9	23.1	33.3	2.6			7
7	2.0	7.0	-20.9	24.5	32.2	13.3			7
8	1.4	7.9	-25.9	36.8	43.3	11.2			7
9	1.8	7.5	-19.3	29.8	35.5	12.9			7
10	2.0	1.0	-14.3	29.6	32.8	1.9			7
11	1.8	6.1	-9.4	32.3	33.7	11.1			7
12	1.5	1.4	-3.3	35.3	38.4	2.3			9
13	1.8	1.6	-3.0	29.1	29.2	3.2			7
14	1.3	2.2	5.7	46.0	46.4	2.9			13
15	1.0	3.3	3.0	25.5	25.6	7.6			18
16	1.3	4.5	8.3	43.2	43.3	6.3			16
17	1.0	1.6	6.8	24.4	25.3	3.9			18
18	1.0	2.5	2.6	25.6	27.8	5.6			18
19	1.0	5.6	23.7	41.7	48.0	7.2			20
20	1.0	2.8	12.8	21.6	25.1	6.9			19
21	1.0	1.1	14.3	21.4	25.7	2.6			19
22	1.0	1.5	27.0	39.3	46.3	1.9			21
23	2.7	5.5	46.4	57.6	74.1	4.6			22
24	2.6	2.3	56.2	65.5	86.7	2.0			23
25	2.7	14.1	44.1	51.0	67.5	12.7			22
26	2.5	14.3	53.1	61.2	81.8	11.3			23
27	1.2	3.4	35.9	57.0	51.5	4.0			25
28	.7	1.7	36.2	58.6	54.3	1.9			26
29	2.5	2.6	58.9	57.7	82.4	1.9			23

TOTAL IDO= 20 9 10 12 NO OF PECOFDS/RADIAL 4 CELL WIDTH 337.2 METERS PRF 794.0

TOTAL IDO= 1 1 1 1 NO OF PECOFDS/RADIAL 4 CELL WIDTH 337.2 METERS PRF 794.0

FIXED CONTOUR ATTRIBUTES

DAY	HHMM	SS	ELE	AZM1	AZM2
226	1936	41	8.0	167.2	132.1
FIXED CONTOUR ATTRIBUTES					
THRESHOLD	AREA	REFLECTIVITY	LOCATION		FIXED
(DBZ)	(KM ²)	(DBZ)	EAST	NORTH	
10	20	30	(KM)	(KM)	CONTOUR
1	1.87	21.0	-24.6	-45.3	1
2	1.01	21.0	-25.3	-47.2	2
3	509.18	42.5	-23.2	22.0	5
4	13.18	21.7	-22.9	-33.3	5
5	2.38	21.8	-2	36.8	4
6	2.35	21.4	2.5	28.5	9
7	23.51	21.5	4.3	23.3	-13
8	38.84	22.5	8.5	43.0	12
9	15.19	22.7	13.2	21.3	14
10	5.24	22.3	25.8	43.3	17
12	96.90	30.6	44.0	53.2	18
1	167.07	48.0	-23.8	21.7	20
2	8.01	43.1	-9.1	31.3	5
					5

WIND DATA

DAY	MM	SS	ELE	AZM1	AZM2
226	1936	41	8.0	147.2	132.1
WEIGHT REFLECTIVITY REFLECTIVITY U V VARIANCE DEL					
TOTAL			AVERAGE		
AVERAGE			TOTAL		
REFLECTIVITY			REFLECTIVITY		
10821			10821		
28.7			28.7		
22.3			22.3		
885.4			885.4		
-8.6			-8.6		
-5.5			-5.5		
34.3			34.3		
24.8			24.8		
.76157E+00			.76157E+00		
.32030E-01			.32030E-01		

PEAK DETECTED CELL ATTRIBUTES

DAY MONTH SS ELE AZM1 AZM2
226 1936 41 5.3 167.2 132.1

ID	REFLECTIVITY (DBZ)	AREA (KM*2)	LOCATION		RANGE (KM)	RESOLUTION ELEMENTS	AVERAGE VELOCITY		SHEAR (M/S/KM)	AVERAGE VELOCITY		SHEAR (M/S/KM)	FIXED CONTOUR
			EAST (KM)	NORTH (KM)			SPREAD (M/S)	RADIAL (M/S)		TANGENTIAL (M/S)	RADIAL (M/S)		
1	21.6	13.2	-22.9	-33.3	40.4	19.9	1.38	-2.22	-3.38	-1.18	-4.17	5	
2	49.6	5.0	-30.9	13.7	33.9	9.1	1.97	-1.16	-1.15	-1.18	-4.17	5	
3	28.9	4.3	-35.2	23.7	42.9	7.0	1.02	-1.70	-1.06	-1.18	-4.17	5	
4	53.8	2.3	-26.6	18.6	32.4	4.4	2.35	3.15	1.35	3.05	3.05	5	
5	57.0	1.1	-25.2	18.7	31.4	2.1	2.05	2.52	-1.15	2.14	2.14	5	
6	55.6	1.3	-22.5	23.2	32.3	2.4	1.77	2.02	-1.90	-1.90	-1.90	5	
7	44.9	2.2	-9.7	31.3	32.8	6.1	1.21	-3.94	-5.3	-10.50	-10.50	5	
8	21.7	2.4	-1.1	36.8	36.8	4.0	.93	-1.11	-1.13	-2.55	-2.55	5	
9	29.8	2.0	2.0	24.6	24.7	4.3	.80	.59	3.76	-3.02	-3.02	12	
10	22.8	30.2	8.4	42.9	43.7	42.2	1.04	-5.33	.33	-5.78	-5.78	14	
11	22.2	5.2	25.8	48.5	48.0	6.7	.85	.32	-1.06	-9.46	-9.46	18	
12	40.6	2.9	42.5	51.4	66.7	2.6	2.22	1.36	1.21	-6.72	-6.72	20	
13	32.9	2.2	47.0	57.3	74.1	1.8	2.62	.23	1.21	-9.05	-9.05	20	
14	25.6	3.5	47.0	51.1	69.5	3.1	2.17	-1.61	-1.05	-7.94	-7.94	20	

TANGENTIAL SHEAR MAXIMA ATTRIBUTES

DAY HMMH SS ELE AZMI AZM2
226 1536 41 6.3 147.2 132.1

ID	MAGNITUDE		AREA (K+K*2)	LOCATION		RANGE (KM)	RESOLUTION		AREA VELOCITY		AVERAGE SHEAR (M/S/KM)	CONTOUR REFERENCE
	SHEAR (M/S/KM)	SPR (K+K*2)		EAST (KM)	NORTH (KM)		ELEMENTS	SPREAD (M/S)	SPREAD (M/S)			
1	1.4	1.2	16.4	23.0	17.7	37.5	1.9	1.9	.7	1.4	-1.4	5
2	.4	1.3	16.6	25.3	25.3	44.5	1.8	1.8	1.2	.4	-.4	5
3	5.3	1.2	25.3	28.9	28.9	38.4	1.5	1.5	1.4	1.4	1.4	5
4	2.1	1.4	27.2	31.6	31.6	41.7	2.0	2.0	1.2	.1	.1	5
5	7.3	2.4	27.3	28.9	28.9	35.5	4.0	4.0	.9	7.3	7.3	5
6	5.0	1.1	18.7	24.7	24.7	31.0	2.1	2.1	1.8	5.0	5.0	5
7	2.5	1.1	18.5	27.9	27.9	32.7	1.9	1.9	1.7	-2.5	-2.5	5
8	.9	1.5	22.4	35.7	35.7	42.1	2.1	2.1	1.2	-.9	-.9	5
9	2.2	1.1	16.3	27.4	27.4	31.3	2.0	2.0	1.7	-2.2	-2.2	5
10	1.9	1.1	13.2	34.1	34.1	36.5	1.6	1.6	.3	-1.0	-1.0	5
11	.6	1.8	15.0	33.9	33.9	41.7	2.6	2.6	1.2	-.6	-.6	5
12	.9	1.1	10.6	36.9	36.9	39.4	1.6	1.6	1.3	-.9	-.9	5
13	1.3	1.1	6.8	35.9	35.9	35.5	1.8	1.8	.9	-1.3	-1.3	5
14	1.1	1.1	11.3	45.4	45.4	46.3	1.4	1.4	1.2	-1.1	-1.1	14
15	2.2	2.0	6.3	22.4	22.4	27.3	2.6	2.6	.7	-.9	-.9	12
16	2.2	2.6	44.9	60.0	60.0	75.0	2.1	2.1	2.1	-2.2	-2.2	20
17	3.8	1.2	43.3	53.6	53.6	64.3	1.1	1.1	2.8	-3.8	-3.8	20

VELOCITY SPREAD MAXIMA ATTRIBUTES

DAY MMH SS ELE AZM1 AZM2
226 1536 41 9.0 147.2 132.1

ID	SPREAD (M/S)	LOCATION		RANGE (KM)	RESOLUTION ELEMENTS	AREA ELEMENTS	CONTOUR REFERENCE
		ASCA	EAST				
		(M/S)	(M/S)				
1	2.0	1.3	-24.6	-45.8	52.0	2.2	1
2	2.2	1.0	-25.9	-47.2	53.3	1.1	2
3	1.8	4.2	-22.9	-35.2	42.0	6.1	4
4	2.7	4.1	-33.9	15.2	37.1	6.7	5
5	1.9	1.4	-35.1	17.5	39.2	2.1	5
6	2.2	1.7	-28.0	16.9	32.7	3.3	5
7	2.7	1.1	-26.4	18.0	31.3	1.9	5
8	2.6	3.6	-26.6	20.6	33.7	12.4	5
9	2.2	1.3	-17.3	31.1	35.6	2.3	5
10	1.7	1.6	-14.2	28.7	32.0	3.0	5
11	2.4	1.0	-10.6	29.5	31.4	2.0	5
12	1.4	15.1	-12.9	36.5	40.6	24.3	5
13	1.6	3.6	-9.7	32.0	33.1	15.0	5
14	1.9	3.9	-6.1	33.4	33.9	7.1	5
15	1.3	1.9	-3.9	28.3	28.6	4.0	5
16	1.1	1.8	.1	35.7	36.7	3.1	9
17	.9	2.7	2.2	20.5	20.6	7.9	13
18	.3	5.4	2.9	24.5	25.0	15.7	12
19	1.1	2.2	7.2	21.8	22.3	5.9	12
20	1.1	2.8	11.9	21.1	24.2	5.9	17
21	1.1	1.6	27.1	39.9	48.3	2.3	19
22	1.0	1.8	15.6	21.7	26.7	4.2	17
23	2.6	11.4	44.3	52.0	68.3	10.2	20
24	2.6	18.3	48.0	56.4	74.0	15.6	20

TOTAL LIDS 21 6 5 9
 EOF RELO ON UNIT 1
 NO OF RECORDS/PAIR 4 CELL WIDTH 937.2 METERS PRF 794.0

FIXED CONTOUR ATTRIBUTES

DAY MMM 55 ELE AZM1 AZM2
226 1977 37 9.0 135.2 112.9

ID	THRESHOLD	AREA (KM ²)	AREA REFLECTIVITY (DBZ)	AVERAGE REFLECTIVITY (DBZ)	LOCATION EAST NORTH (KM)	RANGE RESOLUTION (KM)	RANGE (KM)	PRECIP (TMS/HR)	TOTAL PRECIP (TMS/HR)	AVERAGE PRECIP (MM/HR)	FIXED CONTOUR REFERENCE
1	20	39.07	22.0	22.0	-21.7	33.1	39.0	61.3			1
2	20	64.71	43.5	22.5	-22.5	22.7	31.6	1256.9			2
3	20	4.78	22.3	22.3	3.5	28.3	21.2	13.8			-7
4	20	9.70	21.8	21.8	7.5	19.3	21.3	16.8			-12
5	20	2.13	21.0	21.0	6.1	48.4	44.8	2.9			9
6	20	1.60	21.8	21.8	10.1	19.3	22.2	4.4			13
7	20	25.41	28.6	28.6	43.8	51.4	67.6	23.0			14
8	20	2.35	22.0	22.0	48.5	55.3	75.5	1.3			15
1	40	4.75	43.2	43.2	-8.0	32.3	33.0	8.9			2
2	40	137.18	49.9	49.9	-22.9	21.3	31.9	266.5			2

WIND DATA

DAY	MM	SS	ELE	AZM1	AZM2
226	1937	37	9.0	135.2	112.9
AVERAGE			TOTAL	AVERAGE	AVERAGE
HEIGHT REFLECTIVITY			REFLECTIVITY	U	V
(DBZ)			(DBZ)	(M/SEC)	(M/SEC)
					DEL

PEAK DETECTED CELL ATTRIBUTES

DAY MM:MM SS ELE AZMI AZM2
226 1977 37 9.0 135.2 112.9

ID	REFLECTIVITY (DBZ)	RPER (KM*2)	LOCATION			AREA RESOLUTION ELEMENTS	AVERAGE VELOCITY		AVERAGE TANGENTIAL SHEAR		AVERAGE RADIAL VELOCITY		PEAK FIXED COSTOUR REFERENCE
			EAST (KM)	NORTH (KM)	RANGE (KM)		SPREAD (M/S)	SHEAR (M/S/KM)	SHEAR (M/S/KM)	SHEAR (M/S/KM)	VELOCITY (M/S)	VELOCITY (M/S)	
1	22.3	26.9	-20.7	-33.5	33.4	61.6	1.94	-0.82	-0.41	-0.95	-2.22	-0.95	1
2	41.8	1.3	-33.6	17.7	36.0	2.1	2.53	3.41	-3.08	-2.22	-2.22	-2.22	2
3	48.0	1.2	-30.7	18.9	35.1	2.0	2.11	-2.92	3.37	-0.78	-0.78	-0.78	2
4	59.7	2.1	-24.4	18.8	38.9	4.2	2.21	3.30	.25	-6.19	-6.19	-6.19	2
5	47.6	2.8	-27.2	23.2	35.7	6.7	2.33	-0.37	3.48	-5.49	-5.49	-5.49	2
6	58.9	1.0	-21.6	24.9	32.3	1.9	1.65	-1.27	-0.54	-1.05	-1.05	-1.05	2
7	53.0	1.3	-18.2	23.5	23.8	3.3	1.83	-0.36	-0.52	-1.23	-1.23	-1.23	2
8	51.4	1.4	-16.6	25.6	30.5	2.9	1.81	1.49	-0.13	2.11	2.11	2.11	2
9	23.2	8.8	-11.7	35.0	40.7	13.3	1.85	-0.28	-0.17	.07	.07	.07	2
10	44.2	2.1	-8.2	31.5	32.5	3.9	1.29	1.12	-0.19	.44	.44	.44	2
11	24.5	2.5	5.8	37.7	33.2	4.0	.95	3.50	3.31	-4.33	-4.33	-4.33	2
12	22.8	3.0	3.8	21.1	21.4	8.6	.77	-1.10	1.68	-4.47	-4.47	-4.47	7
13	21.8	5.7	7.5	19.9	21.3	15.3	.83	-0.31	.06	-7.30	-7.30	-7.30	12
14	21.7	1.6	10.2	19.4	22.3	4.4	1.94	-0.14	-0.26	-6.18	-6.18	-6.18	13
15	13.0	4.3	43.7	51.4	67.5	3.9	2.24	-0.31	-1.69	-8.92	-8.92	-8.92	14

TANGENTIAL SHEAR MAXIMA ATTRIBUTES

DAY HHMM SS ELE AZM1 AZM2
226 1377 37 9.0 135.2 112.9

ID	MAGNITUDE (M/S/KM)	SHEAR (M/S/KM)	LOCATION		RANGE (KM)	RESOLUTION ELEMENTS	AREA ELEMENTS	AVERAGE VELOCITY SPREAD (M/S)	AVERAGE SHEAR (M/S/KM)	FIXED CONTOUR REFERENCE
			EAST (KM)	NORTH (KM)						
1	1.3	1.3	-26.8	32.9	41.3	1.9	1.4	1.4	-1.3	2
2	4.7	1.1	-18.0	25.2	30.3	2.1	2.1	2.1	4.7	2
3	2.1	1.5	-18.9	25.9	29.3	3.2	1.3	1.3	-1.7	2
4	1.0	1.4	-17.7	36.2	40.3	2.1	1.8	1.8	-1.0	2
5	.9	1.8	-15.5	34.6	37.3	2.9	1.3	1.3	.4	2
6	1.6	4.1	-18.1	39.2	41.7	6.0	1.0	1.0	-1.6	2
7	1.6	1.5	-5.9	29.6	30.1	3.0	1.6	1.6	-1.6	2
8	3.8	1.1	-6.3	33.2	31.7	1.9	2.2	2.2	-3.8	2
9	1.6	1.1	-6.3	31.6	31.3	2.0	1.7	1.7	-1.6	2
10	.9	1.1	.1	34.2	34.2	1.9	1.1	1.1	-1.9	2

VELOCITY SPEED MAXIMA ATTRIBUTES

DAY MONTH SS ELE AZM1 AZM2
226 1937 37 9.0 135.2 112.3

ID	SPEED (M/S)	LOCATION		AREA (KM2)	RANGE (KM)	RESOLUTION ELEMENTS	AREA CONTOUR REFERENCE	FIVE
		EAST (KM)	NORTH (KM)					
1	2.4	2.4	-23.0	36.8	41.4	4.0	1	
2	1.6	3.1	-23.7	29.5	37.3	5.1	1	
3	2.3	2.5	-35.1	17.3	37.4	4.0	2	
4	2.6	2.5	-30.8	19.7	36.8	4.4	2	
5	2.6	13.4	-25.9	21.2	33.5	19.7	2	
6	1.9	5.7	-23.5	28.3	36.3	10.0	2	
7	2.7	1.1	-18.6	26.3	32.3	2.1	2	
8	2.5	1.3	-25.9	32.2	38.4	2.1	2	
9	2.6	1.1	-17.4	28.7	33.4	1.9	2	
10	2.1	3.2	-16.5	38.2	35.0	6.1	2	
11	2.0	5.1	-15.3	27.2	31.2	12.0	2	
12	1.8	7.0	-17.1	37.4	41.2	10.5	2	
13	1.9	1.1	-10.9	32.0	33.8	2.0	2	
14	2.8	4.3	-5.9	33.2	33.7	7.6	2	
15	1.0	4.2	4.6	31.6	32.3	7.5	7	
16	1.3	13.5	7.0	38.9	39.5	21.0	2	
17	1.8	3.4	7.8	19.9	21.4	9.7	12	
18	1.3	1.5	16.2	19.8	22.3	4.4	13	
19	1.2	1.1	45.1	56.0	74.5	.5	15	
20	2.3	14.3	44.5	51.5	68.1	12.0	14	
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PWA OF THE LOAD 111
LWA OF THE LOAD 34170

TRANSFER ADDRESS -- EXPAND 6315

PROGRAM AND BLOCK ASSIGNMENTS.

BLOCK	ADDRESS	LENGTH	FILE	DATE	PROCESSOR VER LEVEL	HARDWARE	COMMENTS
/HEAD/	111	15					
/EXPAN/	126	10					
/EXPAN/	136	7463	LGO	85/03/78	FTN	4.5 428	666X I OPT=1
/LINUM/	7621	1					
BLKOUT.	7622	8	LGO	85/03/78	FTN	4.5 428	666X I OPT=1
EXPAN1	7622	343	LGO	05/03/78	FTN	4.5 428	666X I OPT=1
MUSCAL	18165	77	LGO	85/03/78	FTN	4.5 428	666X I OPT=1
LABEL	10264	125	LGO	05/03/78	FTN	4.5 428	666X I OPT=1
/NAME/	10511	6					
/NAMIT/	10417	1					
/CHEXP/	10528	1					
/TAGIT/	10421	1					
/SAVORG/	10522	5					
PLT103	10427	171	UL-PEN	10/14/76	FTN	4.5 414	666X I OPT=2
BLKOUT	10620	54	UL-PEN	10/14/76	FTN	4.5 414	666X I OPT=2
PLOT1	10674	325	UL-PEN	10/14/76	FTN	4.5 414	666X I OPT=2
ENDPLY	11221	160	UL-PEN	10/14/76	FTN	4.5 414	666X I OPT=2
CHEXIT	11401	11	UL-PEN	10/14/76	COMPASS	3. 2-414	
FACTOR	11512	16	UL-PEN	10/14/76	FTN	4.5 414	666X I OPT=2
SYMBOL	11530	387	UL-PEN	10/14/76	FTN	4.5 414	666X I OPT=2
PLOT00	11737	432	UL-PEN	10/14/76	FTN	4.5 414	666X I OPT=2
PLC000E	12171	425	UL-PEN	10/14/76	FTN	4.5 414	666X I OPT=2
PLT01	13016	41	UL-PEN	10/14/76	FTN	4.5 414	666X I OPT=2
WHERE	13102	52	UL-PEN	10/14/76	FTN	4.5 414	666X I OPT=2
EXP1T	13154	235	UL-PEN	10/14/76	FTN	4.5 414	666X I OPT=2
NUMBER	13511	233	UL-PEN	10/14/76	FTN	4.5 414	666X I OPT=2
MEMPEN	13644	66	UL-PEN	10/14/76	FTN	4.5 414	666X I OPT=2
PLT05	13732	75	UL-PEN	10/14/76	FTN	4.5 414	666X I OPT=2
BUFF	14027	467	UL-PEN	10/14/76	COMPASS	3. 2-414	
ABORTS	14516	4	UL-PEN	10/14/76	COMPASS	3. 2-414	
LINLOG	14922	1115	UL-LIB	02/16/78	FTN	4.5 428	666X I OPT=1
DAY	15637	10	UL-LIB	02/16/78	FTN	4.5 428	666X I OPT=1
PAGE	15647	33	UL-LIB	02/16/78	FTN	4.5 428	666X I OPT=1
/STP.END/	15702	1					
/FCL.C./	15703	23					
/Q8.10./	15726	133					
Q8TRY=	16061	0	SL-FORTRAN	08/12/77	COMPASS	3. 3-428	FCL INITIALIZATION ROUTINE.
FECHSK	16061	51	SL-FORTRAN	08/12/77	COMPASS	3. 3-428	INITIALIZE CONSTANTS.
FLTOUT=	16122	311	SL-FORTRAN	08/12/77	COMPASS	3. 3-428	COMMON FLOATING OUTPUT CODE
FORKSYS=	16433	603	SL-FORTRAN	08/12/77	COMPASS	3. 3-428	FORTRAN OBJECT LIBRARY UTILITIES.
INCOM=	17236	276	SL-FORTRAN	08/12/77	COMPASS	3. 3-428	COMMON INPUT FORMATTING CODE
INROUTE=	17534	274	SL-FORTRAN	08/12/77	COMPASS	3. 3-428	NAMELIST OUTPUT ROUTINE.
OUTC=	20030	172	SL-FORTRAN	08/12/77	COMPASS	3. 3-428	FORMATTED WRITE FORTRAN RECORD.
SYSTEMC	20222	487	SL-FORTRAN	08/12/77	COMPASS	3. 3-428	EXTENDED ERROR HANDLING OPTION.

BLOCK	ADDRESS	LENGTH	FILE	DATE	PROCESSOR VER LEVEL	HARDWARE	COMMENTS
CLOCK=	20631	31	SL-FORTRAN	08/12/77	COMPASS 3. 3-428		ACCESS SYSTEM CLOCKS FOR FORTRAN.
GOITER=	20662	14	SL-FORTRAN	08/12/77	COMPASS 3. 3-428		COMPUTED GO TO ERROR PROCESSOR.
RCOG	20676	73	SL-FORTRAN	08/12/77	COMPASS 3. 3-428		COMPUTE COMMON AND NATURAL LOGARITHMS. OPTIMEL.
SINCO5=	20771	66	SL-FORTRAN	08/12/77	COMPASS 3. 3-428		TRIGONOMETRIC SINE OR COSINE OF X. OPT-ALL.
SYSAIO=	21057	1	SL-FORTRAN	08/12/77	COMPASS 3. 3-428		LINK BETWEEN SYSAIO AND INITIALIZATION CODE.
BACKSP=	21060	56	SL-FORTRAN	08/12/77	COMPASS 3. 3-428		BACKSPACE LOGICAL RECORD.
COMIO=	21136	65	SL-FORTRAN	08/12/77	COMPASS 3. 3-428		COMMON CODED I/O ROUTINES AND CONSTANTS.
EOF	21222	16	SL-FORTRAN	08/12/77	COMPASS 3. 3-428		TEST FOR END OF FILE STATUS.
FLINE=	21248	154	SL-FORTRAN	08/12/77	COMPASS 3. 3-428		COMMON FLOATING INPUT CONVERTER.
FRAP=	21414	352	SL-FORTRAN	08/12/77	COMPASS 3. 3-428		CRACK APLIST AND FORMAT FOR KODEA/KRAKER.
FORUTL=	21766	16	SL-FORTRAN	08/12/77	COMPASS 3. 3-428		FCL MISC. UTILITIES.
GETFIT=	22804	42	SL-FORTRAN	08/12/77	COMPASS 3. 3-428		LOCATE AN FIT GIVEN A FILE NAME.
/IO.BUF./	22846	227					
INPB=	22275	314	SL-FORTRAN	08/12/77	COMPASS 3. 3-428		BINARY READ FORTRAN RECORD.
KODE=	22611	556	SL-FORTRAN	08/12/77	COMPASS 3. 3-428		OUTPUT FORMAT INTERPRETER.
NAMEIN=	23267	523	SL-FORTRAN	08/12/77	COMPASS 3. 3-428		NAMELIST INPUT ROUTINE.
OUTCON=	24812	154	SL-FORTRAN	08/12/77	COMPASS 3. 3-428		COMMON OUTPUT CODE
SYSTEM	24866	21	SL-FORTRAN	08/12/77	COMPASS 3. 3-428		COMMON OUTPUT CODE
SYSEIST	24887	52	SL-FORTRAN	08/12/77	COMPASS 3. 3-428		USER CALLABLE ERROR PROCESSOR.
XIOI=	24871	18	SL-FORTRAN	08/12/77	COMPASS 3. 3-428		MATH LIBRARY LINK TO ERROR MESSAGE PROCESSING.
/CON.RM/	24301	6					REAL TO INTEGER EXPONENTIATION.
CIO.RM	24387	40	SL-SYSIO	09/03/76	COMPASS 3. 2-414		
/RUB.RM/	25347	10					
MOVE.RM	24857	64	SL-SYSIO	09/03/76	COMPASS 3. 2-414		
WCT.RM	24853	233	SL-SYSIO	09/03/76	COMPASS 3. 2-414		
/JHPS.RM/	24876	11					
/RENG.RM/	24787	3					
/OPES.FO/	24712	1					
/OPEN.FO/	24713	7					
OPEN.RM	24722	237	SL-SYSIO	09/03/76	COMPASS 3. 2-414		
/PUT.RT/	25161	11					
PLEO.RM	25172	42	SL-SYSIO	09/03/76	COMPASS 3. 2-414		
/CLSF.FO/	25238	7					
CLSF.SO	25243	134	SL-SYSIO	09/03/76	COMPASS 3. 2-414		
/CLSV.FO/	25377	7					
CLSV.SO	25406	137	SL-SYSIO	09/03/76	COMPASS 3. 2-414		
/REW.FO/	25545	7					
REW.SQ	25554	33	SL-SYSIO	09/03/76	COMPASS 3. 2-414		
/TERM.PM/	25687	1					
/GET.FO/	25618	7					
/GET.BT/	25617	5					
/GET.RT/	25624	11					
GET.SQ	25635	1134	SL-SYSIO	09/03/76	COMPASS 3. 2-414		
Z.SQ	26771	101	SL-SYSIO	09/03/76	COMPASS 3. 2-414		
W.SQ	27872	58	SL-SYSIO	09/03/76	COMPASS 3. 2-414		
F.SQ	27142	106	SL-SYSIO	09/03/76	COMPASS 3. 2-414		
/KBL.FO/	27250	7					
/KSB.FO/	27257	1					
SKSB.SQ	27268	181	SL-SYSIO	09/03/76	COMPASS 3. 2-414		
EP.RM	27161	404	SL-SYSIO	09/03/76	COMPASS 3. 2-414		
CHWR.SQ	27765	7					
OSUB.RM	27774	71	SL-SYSIO	09/03/76	COMPASS 3. 2-414		
OPEN.SQ	33065	254	SL-SYSIO	09/03/76	COMPASS 3. 2-414		
OPEN.SQ	33041	14	SL-SYSIO	09/03/76	COMPASS 3. 2-414		
/PUT.FO/	33355	7					

LOAD MAP - EXPAND		CYBER LOADER 1.1-420		05/03/70	10.00.41.	PAGE	3
PUT.RM	30364	2	SL-SYSTO	09/03/76	COMPASS	3.	2-414
PUT.SD	30366	1400	SL-SYSTO	09/03/76	COMPASS	3.	2-414
MAP.SD	31766	260	SL-SYSTO	09/03/76	COMPASS	3.	2-414
CLSF.RM	32246	25	SL-SYSTO	09/03/76	COMPASS	3.	2-414
BTFT.SD	32273	115	SL-SYSTO	09/03/76	COMPASS	3.	2-414
WFOX.SD	32410	150	SL-SYSTO	09/03/76	COMPASS	3.	2-414
/SKFL.FD/	32560	7	SL-SYSTO	09/03/76	COMPASS	3.	2-414
SKFL.SD	32567	51	SL-SYSTO	09/03/76	COMPASS	3.	2-414
SKBL.SD	32640	1026	SL-SYSTO	09/03/76	COMPASS	3.	2-414
MXGET	33666	33	SL-NUCLEUS	02/05/74	COMPASS	3.	73269
MYPUT	33721	22	SL-NUCLEUS	02/05/74	COMPASS	3.	73269
RECOMR	33743	166	SL-NUCLEUS	04/15/77	COMPASS	3.	2-414
SYS.RM	34131	37	SL-NUCLEUS	04/15/77	COMPASS	3.	2-414
		REPRIEVE INTERFACE PROCESS SYSTEM REQUEST.					

1.85M CP SECONDS 674003 24 STORAGE USED 105 TABLE MOVES

175 0 PROGRAM EXPAND 19.80.42. VERSION 1.0 (770331) 05/03/78 PAGE 1

1.937	3.097	3001	2.089	3.168	2001	4.103	1.157	4.218	1.270
2.031	3.512	3001	2.823	3.531	2001	5.532	1.613	5.519	1.951
2.765	3.475	3001	2.692	3.479	2001	5.336	1.762	5.310	1.768
2.344	3.340	3001	2.300	3.323	2001	4.753	1.565	4.684	1.518
2.268	3.276	3001	2.256	3.206	2001	4.633	1.444	4.614	1.491
2.182	3.240	3001	2.189	3.271	2001	4.495	1.386	4.475	1.435
2.189	3.271	3001	2.126	3.254	2001	4.475	1.435	4.455	1.407
2.126	3.254	3001	2.138	3.222	2001	4.405	1.407	4.425	1.457
2.009	3.168	3001	1.995	3.201	2001	4.213	1.270	4.196	1.324
2.823	3.531	3001	2.816	3.549	2001	5.513	1.651	5.504	1.880
2.692	3.479	3001	2.684	3.499	2001	5.310	1.768	5.296	1.800
2.344	3.340	3001	2.334	3.366	2001	4.753	1.566	4.737	1.587
2.300	3.323	3001	2.290	3.349	2001	4.684	1.518	4.667	1.560
2.256	3.306	3001	2.246	3.332	2001	4.614	1.491	4.597	1.533
1.995	3.201	3001	1.983	3.232	2001	4.196	1.324	4.177	1.373
2.816	3.549	3001	2.809	3.569	2001	5.506	1.680	5.496	1.912
2.684	3.499	3001	2.632	3.506	2001	5.298	1.800	5.214	1.810
2.334	3.366	3001	2.323	3.394	2001	4.737	1.587	4.721	1.632
2.279	3.349	3001	2.279	3.378	2001	4.667	1.550	4.650	1.606
2.246	3.332	3001	2.235	3.362	2001	4.597	1.533	4.580	1.581
2.058	3.298	3001	2.054	3.282	2001	4.298	1.479	4.227	1.453
1.983	3.232	3001	1.926	3.251	2001	4.177	1.373	4.086	1.402
2.809	3.569	3001	2.801	3.590	2001	5.496	1.912	5.485	1.944
2.713	3.559	3001	2.668	3.544	2001	5.343	1.836	5.272	1.871
2.632	3.506	3001	2.624	3.529	2001	5.214	1.810	5.201	1.847
2.446	3.468	3001	2.402	3.453	2001	4.917	1.750	4.847	1.726
2.323	3.394	3001	2.313	3.422	2001	4.721	1.632	4.705	1.677
2.279	3.378	3001	2.269	3.407	2001	4.650	1.606	4.634	1.653
2.269	3.407	3001	2.224	3.352	2001	4.634	1.653	4.563	1.623
2.224	3.392	3001	2.235	3.362	2001	4.553	1.629	4.580	1.561
2.180	3.377	3001	2.136	3.362	2001	4.492	1.604	4.421	1.580
2.058	3.298	3001	2.047	3.331	2001	4.298	1.479	4.279	1.531
2.014	3.282	3001	1.958	3.301	2001	4.227	1.453	4.137	1.483
1.926	3.251	3001	1.914	3.266	2001	4.086	1.402	4.066	1.453
2.801	3.590	3001	2.751	3.594	2001	5.485	1.944	5.404	1.951
2.713	3.559	3001	2.706	3.579	2001	5.343	1.836	5.132	1.927
2.706	3.579	3001	2.661	3.565	2001	5.332	1.927	5.261	1.904
2.661	3.565	3001	2.668	3.544	2001	5.261	1.904	5.272	1.871
2.624	3.529	3001	2.617	3.550	2001	5.201	1.847	5.190	1.881
2.446	3.468	3001	2.483	3.506	2001	4.917	1.750	4.976	1.811
2.402	3.453	3001	2.394	3.477	2001	4.847	1.726	4.833	1.765
2.394	3.477	3001	2.304	3.448	2001	4.833	1.765	4.691	1.719
2.306	3.448	3001	2.313	3.422	2001	4.631	1.719	4.705	1.677
2.260	3.434	3001	2.215	3.419	2001	4.620	1.695	4.548	1.672
2.180	3.377	3001	2.171	3.405	2001	4.592	1.606	4.477	1.589
2.171	3.405	3001	2.126	3.390	2001	4.477	1.649	4.406	1.626
2.126	3.390	3001	2.136	3.362	2001	4.406	1.626	4.421	1.580
2.047	3.331	3001	2.037	3.361	2001	4.279	1.531	4.263	1.579
1.958	3.301	3001	1.992	3.347	2001	4.137	1.483	4.192	1.556
1.914	3.286	3001	1.946	3.332	2001	4.066	1.459	4.120	1.533
2.013	3.697	3001	2.968	3.683	2001	5.823	2.116	5.751	2.094
2.751	3.594	3001	2.739	3.620	2001	5.404	1.951	5.465	2.006
2.617	3.550	3001	2.609	3.573	2001	5.190	1.881	5.178	1.918
2.443	3.506	3001	2.475	3.532	2001	4.976	1.811	4.963	1.852
2.430	3.518	3001	2.385	3.505	2001	4.691	1.830	4.620	1.808
2.250	3.434	3001	2.251	3.463	2001	4.620	1.695	4.605	1.742
2.251	3.463	3001	2.206	3.450	2001	4.605	1.742	4.533	1.720
2.206	3.450	3001	2.215	3.419	2001	4.533	1.720	4.548	1.672
2.286	3.450	3001	2.161	3.436	2001	4.533	1.720	4.461	1.698
2.037	3.361	3001	2.026	3.394	2001	4.263	1.573	4.246	1.633
2.026	3.394	3001	1.981	3.381	2001	4.266	1.633	4.175	1.611
1.981	3.381	3001	1.992	3.347	2001	4.175	1.611	4.192	1.556
1.948	3.332	3001	1.981	3.381	2001	4.120	1.589	4.175	1.611
1.443	3.216	3001	1.398	3.202	2001	3.315	1.347	3.243	1.325
3.013	3.697	3001	3.053	3.728	2001	5.823	2.116	5.867	2.166
2.968	3.683	3001	2.918	3.650	2001	5.751	2.094	5.670	2.104

2.789	3.620	3001	2.737	3.630	2001	5.465	2.006	5.302	2.021
2.689	3.573	3001	2.557	3.506	2001	5.170	1.910	5.094	1.939
2.879	3.532	3001	2.666	3.568	2001	4.983	1.852	4.950	1.897
2.630	3.510	3001	2.621	3.547	2001	4.691	1.830	4.670	1.677
2.385	3.505	3001	2.376	3.534	2001	4.820	1.808	4.806	1.856
2.268	3.509	3001	2.136	3.483	2001	4.661	1.815	4.517	1.773
2.206	3.558	3001	2.136	3.483	2001	4.533	1.720	4.517	1.773
2.196	3.483	3001	2.151	3.470	2001	4.517	1.773	4.445	1.753
2.151	3.478	3001	2.151	3.470	2001	4.445	1.753	4.445	1.753
1.941	3.301	3001	1.925	3.405	2001	4.175	1.611	4.005	1.649
1.443	3.216	3001	1.429	3.263	2001	3.315	1.347	3.292	1.422
1.429	3.263	3001	1.390	3.202	2001	3.292	1.422	3.243	1.325
1.893	3.728	3001	3.068	3.764	2001	5.887	2.166	5.879	2.192
2.918	3.690	3001	2.912	3.708	2001	5.678	2.104	5.662	2.133
2.737	3.630	3001	2.731	3.659	2001	5.382	2.021	5.373	2.055
2.557	3.566	3001	2.550	3.611	2001	5.094	1.939	5.083	1.970
2.558	3.611	3001	2.459	3.586	2001	5.083	1.978	4.938	1.939
2.558	3.566	3001	2.466	3.560	2001	4.938	1.939	4.950	1.897
2.821	3.547	3001	2.814	3.574	2001	4.878	1.877	4.866	1.919
2.414	3.574	3001	2.369	3.562	2001	4.866	1.919	4.793	1.980
2.389	3.562	3001	2.376	3.534	2001	4.793	1.980	4.806	1.856
2.286	3.589	3001	2.278	3.538	2001	4.661	1.815	4.649	1.861
2.278	3.538	3001	2.187	3.513	2001	4.649	1.861	4.504	1.822
2.187	3.513	3001	2.196	3.483	2001	4.504	1.822	4.517	1.773
1.925	3.585	3001	1.961	3.452	2001	4.085	1.649	4.162	1.725
3.040	3.744	3001	3.044	3.761	2001	5.879	2.192	5.873	2.217
2.912	3.708	3001	2.953	3.738	2001	5.662	2.133	5.727	2.181
2.731	3.659	3001	2.726	3.681	2001	5.373	2.055	5.364	2.090
2.687	3.681	3001	2.362	3.589	2001	4.855	1.962	4.782	1.945
1.861	3.652	3001	1.997	3.498	2001	4.142	1.725	4.200	1.798
3.044	3.761	3001	2.995	3.764	2001	5.873	2.217	5.794	2.224
2.925	3.738	3001	2.949	3.754	2001	5.727	2.181	5.721	2.207
2.726	3.681	3001	2.675	3.698	2001	5.364	2.090	5.283	2.104
2.487	3.601	3001	2.481	3.625	2001	4.855	1.962	4.845	2.001
2.382	3.549	3001	2.355	3.615	2001	4.782	1.964	4.772	1.984
1.997	3.490	3001	1.938	3.529	2001	4.200	1.798	4.108	1.847
2.995	3.764	3001	2.991	3.791	2001	5.795	2.225	5.861	2.267
2.949	3.754	3001	2.991	3.781	2001	5.721	2.207	5.780	2.251
2.675	3.698	3001	2.716	3.722	2001	5.283	2.104	5.348	2.156
2.491	3.625	3001	2.395	3.652	2001	4.845	2.001	4.835	2.045
2.395	3.652	3001	2.349	3.642	2001	4.635	2.055	4.762	2.029
2.349	3.642	3001	2.355	3.615	2001	4.762	2.029	4.772	1.984
2.128	3.593	3001	2.074	3.583	2001	4.396	1.949	4.323	1.933
1.990	3.529	3001	2.028	3.573	2001	4.189	1.847	4.249	1.918
3.837	3.791	3001	3.834	3.808	2001	5.861	2.257	5.856	2.293
2.991	3.781	3001	2.988	3.799	2001	5.780	2.251	5.782	2.270
2.715	3.722	3001	2.711	3.744	2001	5.348	2.156	5.341	2.190
2.128	3.593	3001	2.113	3.625	2001	4.396	1.949	4.385	2.000
2.113	3.625	3001	2.067	3.615	2001	4.385	2.000	4.312	1.985
2.067	3.615	3001	2.074	3.583	2001	4.312	1.985	4.323	1.933
2.028	3.573	3001	2.067	3.615	2001	4.249	1.918	4.312	1.985
3.834	3.808	3001	3.831	3.821	2001	5.856	2.293	5.852	2.314
2.985	3.799	3001	2.985	3.813	2001	5.782	2.270	5.782	2.300
2.711	3.744	3001	2.662	3.753	2001	5.341	2.190	5.262	2.205
2.662	3.753	3001	2.188	3.651	2001	4.312	1.985	4.377	2.062
2.021	3.621	3001	2.028	3.637	2001	4.312	1.985	4.377	2.062
2.985	3.813	3001	2.982	3.830	2001	5.852	2.314	5.847	2.340
2.662	3.753	3001	2.612	3.768	2001	5.262	2.102	5.182	2.229
2.519	3.752	3001	2.473	3.745	2001	5.036	2.204	4.960	2.192
2.449	3.690	3001	2.403	3.683	2001	4.442	2.105	4.368	2.093
2.108	3.651	3001	2.010	3.667	2001	4.377	2.062	4.220	2.068
3.828	3.837	3001	3.826	3.854	2001	5.847	2.340	5.843	2.366
2.982	3.838	3001	2.933	3.881	2001	5.773	2.328	5.695	2.344
2.612	3.768	3001	2.654	3.798	2001	5.182	2.229	5.250	2.278
2.608	3.791	3001	2.592	3.784	2001	5.176	2.266	5.182	2.255
2.519	3.752	3001	2.515	3.777	2001	5.834	2.284	5.827	2.244

2.515	3.777	3.031	2.469	3.770	2.001	5.027	2.244	4.553	2.233
2.469	3.770	3.031	2.473	3.745	2.001	4.953	2.233	4.960	2.192
2.376	3.756	3.031	2.330	3.749	2.001	4.805	2.211	4.731	2.200
2.217	3.736	3.031	2.130	3.729	2.001	4.583	2.177	4.506	2.166
2.149	3.690	3.031	2.144	3.722	2.001	4.442	2.135	4.434	2.155
2.103	3.663	3.031	2.098	3.715	2.001	4.358	2.093	4.360	2.144
2.098	3.715	3.031	2.010	3.667	2.001	4.350	2.154	4.220	2.158
3.026	3.654	3.031	3.023	3.664	2.001	5.043	2.166	5.039	2.163
2.933	3.640	3.031	2.977	3.664	2.001	5.635	2.344	5.765	2.783
2.654	3.798	3.031	2.605	3.615	2.001	5.250	2.275	5.170	2.304
2.608	3.791	3.031	2.505	3.615	2.001	5.176	2.266	5.170	2.304
2.605	3.615	3.031	2.556	3.609	2.001	5.170	2.266	5.096	2.294
2.558	3.609	3.031	2.562	3.609	2.001	5.036	2.234	5.102	2.255
2.558	3.609	3.031	2.512	3.602	2.001	5.036	2.234	5.022	2.284
2.376	3.756	3.031	2.372	3.724	2.001	4.885	2.211	4.799	2.255
2.372	3.704	3.031	2.326	3.774	2.001	4.793	2.255	4.724	2.245
2.326	3.774	3.031	2.330	3.769	2.001	4.724	2.255	4.731	2.245
2.237	3.736	3.031	2.233	3.765	2.001	4.583	2.177	4.576	2.229
2.233	3.765	3.031	2.186	3.759	2.001	4.576	2.225	4.502	2.215
2.233	3.765	3.031	2.130	3.729	2.001	4.502	2.215	4.508	2.166
2.146	3.759	3.031	2.130	3.747	2.001	4.434	2.155	4.353	2.195
2.144	3.722	3.031	2.093	3.747	2.001	5.633	2.393	5.336	2.613
3.023	3.670	3.031	3.021	3.687	2.001	5.765	2.333	5.667	2.602
2.977	3.664	3.031	2.926	3.676	2.001	5.315	2.359	5.240	2.350
2.695	3.649	3.031	2.646	3.644	2.001	5.170	2.314	5.156	2.342
2.685	3.615	3.031	2.602	3.618	2.001	5.096	2.234	5.017	2.332
2.558	3.609	3.031	2.555	3.613	2.001	5.022	2.234	5.017	2.324
2.512	3.602	3.031	2.506	3.626	2.001	4.953	2.215	4.846	2.247
2.033	3.747	3.031	2.033	3.779	2.001	5.836	2.613	5.833	2.646
3.021	3.687	3.031	3.019	3.693	2.001	5.687	2.442	5.759	2.638
2.928	3.676	3.031	2.973	3.699	2.001	5.315	2.353	5.311	2.394
2.695	3.649	3.031	2.633	3.671	2.001	5.311	2.354	5.240	2.379
2.693	3.671	3.031	2.646	3.644	2.001	5.156	2.312	5.152	2.379
2.602	3.638	3.031	2.535	3.662	2.001	5.091	2.343	5.087	2.372
2.555	3.633	3.031	2.552	3.657	2.001	5.087	2.343	5.012	2.365
2.952	3.657	3.031	2.906	3.663	2.001	5.012	2.343	5.017	2.324
2.906	3.653	3.031	2.906	3.626	2.001	4.946	2.247	4.941	2.258
2.089	3.779	3.031	2.086	3.811	2.001	4.946	2.247	4.941	2.258
1.805	3.784	3.031	1.759	3.779	2.001	4.833	2.445	5.131	2.667
3.019	3.903	3.031	3.018	3.911	2.001	5.631	2.467	5.759	2.636
3.018	3.917	3.031	2.973	3.699	2.001	5.152	2.379	5.155	2.610
2.599	3.662	3.031	2.537	3.669	2.001	5.009	2.338	4.935	2.391
2.584	3.673	3.031	2.457	3.669	2.001	4.836	2.366	4.861	2.360
2.270	3.854	3.031	2.223	3.850	2.001	4.836	2.366	4.861	2.360
2.086	3.811	3.031	2.036	3.834	2.001	4.836	2.366	4.861	2.360
1.930	3.830	3.031	1.943	3.826	2.001	4.836	2.366	4.861	2.360
1.836	3.822	3.031	1.849	3.818	2.001	4.836	2.366	4.861	2.360
1.805	3.784	3.031	1.803	3.814	2.001	4.836	2.366	4.861	2.360
1.803	3.814	3.031	1.759	3.779	2.001	4.836	2.366	4.861	2.360
2.597	3.681	3.031	2.536	3.695	2.001	5.153	2.418	5.156	2.463
2.584	3.673	3.031	2.502	3.669	2.001	5.009	2.338	5.006	2.438
2.455	3.695	3.031	2.455	3.689	2.001	5.006	2.438	4.932	2.431
2.270	3.854	3.031	2.266	3.863	2.001	4.932	2.431	4.935	2.431
2.266	3.863	3.031	2.221	3.860	2.001	4.836	2.366	4.832	2.413
2.221	3.880	3.031	2.223	3.850	2.001	4.836	2.366	4.832	2.413
2.036	3.834	3.031	2.034	3.867	2.001	4.836	2.366	4.832	2.413
2.034	3.867	3.031	1.987	3.864	2.001	4.836	2.366	4.832	2.413
1.987	3.864	3.031	1.930	3.864	2.001	4.836	2.366	4.832	2.413
1.943	3.826	3.031	1.940	3.861	2.001	4.836	2.366	4.832	2.413
1.940	3.861	3.031	1.893	3.862	2.001	4.836	2.366	4.832	2.413
1.893	3.857	3.031	1.896	3.862	2.001	4.836	2.366	4.832	2.413
1.849	3.810	3.031	1.800	3.851	2.001	4.836	2.366	4.832	2.413
2.596	3.931	3.031	2.546	3.931	2.001	5.156	2.483	5.077	2.525
2.594	3.931	3.031	2.546	3.931	2.001	5.156	2.483	5.077	2.525
2.486	3.946	3.031	2.459	3.947	2.001	4.852	2.518	4.777	2.515

1.844	3.494	3.001	1.796	3.929	2.001	3.965	2.431	3.870	2.486
2.566	3.953	3.001	2.533	3.976	2.001	5.077	2.523	5.151	2.562
2.405	3.968	3.001	2.405	3.973	2.001	4.892	2.518	4.851	2.557
2.485	3.973	3.001	2.358	3.972	2.001	4.851	2.557	4.776	2.556
2.358	3.972	3.001	2.358	3.972	2.001	4.776	2.556	4.777	2.515
2.830	3.967	3.001	1.983	3.966	2.001	4.252	2.547	4.177	2.545
1.795	3.929	3.001	1.795	3.963	2.001	3.878	2.486	3.877	2.580
2.593	3.976	3.001	2.545	3.998	2.001	5.151	2.562	5.076	2.596
2.038	3.967	3.001	2.029	3.997	2.001	4.252	2.547	4.251	2.595
2.829	3.997	3.001	1.982	3.997	2.001	4.251	2.595	4.176	2.595
1.982	3.997	3.001	1.983	3.966	2.001	4.176	2.595	4.177	2.545
1.795	3.963	3.001	1.795	3.996	2.001	3.877	2.540	3.876	2.594
2.639	4.023	3.001	2.593	4.026	2.001	5.226	2.637	5.151	2.638
2.545	3.998	3.001	2.493	4.025	2.001	5.076	2.596	5.001	2.640
1.795	3.996	3.001	1.842	4.036	2.001	3.876	2.534	3.952	2.658
2.639	4.023	3.001	2.687	4.036	2.001	5.226	2.637	5.302	2.661
2.593	4.024	3.001	2.593	4.041	2.001	5.151	2.638	5.152	2.655
2.499	4.025	3.001	2.546	4.042	2.001	5.001	2.640	5.077	2.668
1.852	4.031	3.001	1.796	4.055	2.001	3.952	2.658	3.870	2.782
2.687	4.038	3.001	2.641	4.073	2.001	5.302	2.661	5.229	2.717
2.593	4.041	3.001	2.594	4.075	2.001	5.152	2.655	5.154	2.721
2.594	4.075	3.001	2.548	4.078	2.001	5.154	2.721	5.079	2.725
2.568	4.078	3.001	2.546	4.042	2.001	5.079	2.725	5.077	2.658
1.796	4.064	3.001	1.845	4.116	2.001	3.878	2.782	3.956	2.785
2.641	4.073	3.001	2.596	4.095	2.001	5.229	2.717	5.156	2.752
2.549	4.098	3.001	2.502	4.101	2.001	5.001	2.757	5.006	2.762
1.845	4.116	3.001	1.893	4.142	2.001	3.956	2.785	4.034	2.827
2.596	4.095	3.001	2.597	4.119	2.001	5.156	2.752	5.159	2.789
2.583	4.098	3.001	2.551	4.122	2.001	5.081	2.757	5.084	2.796
2.502	4.101	3.001	2.504	4.126	2.001	5.006	2.762	5.009	2.802
1.893	4.142	3.001	1.943	4.176	2.001	4.836	2.827	4.113	2.878
2.597	4.119	3.001	2.646	4.135	2.001	5.159	2.789	5.237	2.816
2.551	4.122	3.001	2.553	4.145	2.001	5.084	2.796	5.087	2.833
2.553	4.145	3.001	2.506	4.149	2.001	5.087	2.831	5.013	2.839
2.506	4.149	3.001	2.504	4.126	2.001	5.013	2.839	5.009	2.882
2.506	4.149	3.001	2.459	4.154	2.001	5.013	2.839	4.938	2.846
1.853	4.174	3.001	1.946	4.205	2.001	4.113	2.878	4.118	2.928
2.646	4.135	3.001	2.602	4.166	2.001	5.237	2.816	5.166	2.865
2.556	4.171	3.001	2.509	4.177	2.001	5.092	2.874	5.018	2.883
2.586	4.149	3.001	2.589	4.177	2.001	5.013	2.839	5.018	2.883
2.589	4.177	3.001	2.462	4.182	2.001	5.018	2.883	4.943	2.891
2.462	4.182	3.001	2.459	4.154	2.001	4.943	2.891	4.938	2.846
1.946	4.205	3.001	1.950	4.243	2.001	4.118	2.928	4.124	2.988
2.682	4.166	3.001	2.651	4.181	2.001	5.166	2.865	5.245	2.889
2.685	4.187	3.001	2.558	4.193	2.001	5.171	2.899	5.097	2.909
2.556	4.171	3.001	2.558	4.193	2.001	5.092	2.874	5.097	2.909
2.558	4.193	3.001	2.512	4.200	2.001	5.097	2.909	5.022	2.919
2.512	4.200	3.001	2.509	4.177	2.001	5.022	2.919	5.018	2.883
2.665	4.206	3.001	2.619	4.212	2.001	4.948	2.929	4.874	2.939
1.950	4.243	3.001	2.000	4.268	2.001	4.124	2.988	4.205	3.029
2.651	4.181	3.001	2.688	4.209	2.001	5.245	2.889	5.176	2.933
2.605	4.187	3.001	2.608	4.209	2.001	5.171	2.899	5.176	2.933
2.608	4.209	3.001	2.562	4.216	2.001	5.176	2.933	5.102	2.944
2.562	4.216	3.001	2.558	4.193	2.001	5.102	2.944	5.097	2.909
2.665	4.206	3.001	2.469	4.229	2.001	4.948	2.929	4.933	2.967
2.669	4.229	3.001	2.422	4.236	2.001	4.953	2.967	4.879	2.978
2.622	4.236	3.001	2.419	4.212	2.001	4.879	2.978	4.874	2.939
2.608	4.268	3.001	2.651	4.292	2.001	4.205	3.029	4.206	3.067
2.608	4.209	3.001	2.474	4.268	2.001	5.176	2.933	4.981	3.015
2.651	4.292	3.001	2.104	4.323	2.001	4.236	3.067	4.378	3.116
2.674	4.268	3.001	2.678	4.283	2.001	4.981	3.015	4.988	3.053
2.684	4.323	3.001	2.109	4.352	2.001	4.378	3.116	4.378	3.162
2.678	4.283	3.001	2.484	4.334	2.001	4.988	3.053	4.977	3.101
2.609	4.352	3.001	2.254	4.361	2.001	4.378	3.162	4.610	3.177
2.678	4.399	3.001	2.024	4.409	2.001	4.316	3.238	4.283	3.253
2.609	4.265	3.001	2.763	4.276	2.001	5.497	3.024	5.424	3.040

2.100	4.114	1001	2.104	6.127	2001	5.112	1.106	5.050	1.122
2.101	4.114	1001	2.107	6.157	2001	6.977	1.101	6.039	1.171
2.102	4.114	1001	2.109	6.178	2001	6.918	1.177	6.992	1.203
2.103	4.114	1001	2.177	6.429	2001	6.216	1.228	6.127	1.205
2.104	4.114	1001	2.124	6.539	2001	6.127	1.205	6.263	1.253
2.105	4.114	1001	2.415	6.291	2001	5.697	1.124	5.587	1.165
2.106	4.114	1001	2.763	6.278	2001	5.507	1.089	5.828	1.189
2.107	4.114	1001	2.813	6.136	2001	5.361	1.111	5.216	1.116
2.108	4.114	1001	2.587	6.187	2001	5.182	1.108	5.187	1.194
2.109	4.114	1001	2.516	6.127	2001	5.163	1.156	5.050	1.122
2.110	4.114	1001	2.585	6.152	2001	6.039	1.171	6.052	1.226
2.111	4.114	1001	2.105	6.178	2001	6.052	1.226	6.052	1.203
2.112	4.114	1001	2.726	6.123	2001	5.281	1.101	5.166	1.113
2.113	4.114	1001	2.598	6.195	2001	5.216	1.116	5.146	1.168
2.114	4.114	1001	2.826	6.125	2001	5.365	1.113	5.521	1.123
2.115	4.114	1001	2.643	6.175	2001	5.377	1.168	5.232	1.201
2.116	4.114	1001	2.535	6.188	2001	5.166	1.158	5.166	1.228
2.117	4.114	1001	2.831	6.169	2001	5.521	1.128	5.532	1.157
2.118	4.114	1001	2.761	6.175	2001	5.558	1.179	5.188	1.233
2.119	4.114	1001	2.636	6.169	2001	5.377	1.168	5.316	1.221
2.120	4.114	1001	2.581	6.182	2001	5.232	1.208	5.265	1.263
2.121	4.114	1001	2.598	6.188	2001	5.261	1.261	5.161	1.221
2.122	4.114	1001	1.482	6.751	2001	1.583	1.778	1.777	1.188
2.123	4.114	1001	1.487	6.791	2001	1.233	1.843	1.161	1.164
2.124	4.114	1001	1.172	6.791	2001	7.688	2.639	7.675	1.795
2.125	4.114	1001	1.172	6.791	2001	1.275	6.627	7.688	2.648
2.126	4.114	1001	6.108	6.038	2002	5.926	1.037		
2.127	4.114	1001	6.108	6.038	2002	6.086	1.114		
2.128	4.114	1001	6.108	6.038	2002	5.223	1.158		
2.129	4.114	1001	6.108	6.038	2002	6.106	1.114		
2.130	4.114	1001	6.108	6.038	2002	6.106	1.114		
2.131	4.114	1001	6.108	6.038	2002	6.106	1.114		
2.132	4.114	1001	6.108	6.038	2002	6.106	1.114		
2.133	4.114	1001	6.108	6.038	2002	6.106	1.114		
2.134	4.114	1001	6.108	6.038	2002	6.106	1.114		
2.135	4.114	1001	6.108	6.038	2002	6.106	1.114		
2.136	4.114	1001	6.108	6.038	2002	6.106	1.114		
2.137	4.114	1001	6.108	6.038	2002	6.106	1.114		
2.138	4.114	1001	6.108	6.038	2002	6.106	1.114		
2.139	4.114	1001	6.108	6.038	2002	6.106	1.114		
2.140	4.114	1001	6.108	6.038	2002	6.106	1.114		
2.141	4.114	1001	6.108	6.038	2002	6.106	1.114		
2.142	4.114	1001	6.108	6.038	2002	6.106	1.114		
2.143	4.114	1001	6.108	6.038	2002	6.106	1.114		
2.144	4.114	1001	6.108	6.038	2002	6.106	1.114		
2.145	4.114	1001	6.108	6.038	2002	6.106	1.114		
2.146	4.114	1001	6.108	6.038	2002	6.106	1.114		
2.147	4.114	1001	6.108	6.038	2002	6.106	1.114		
2.148	4.114	1001	6.108	6.038	2002	6.106	1.114		
2.149	4.114	1001	6.108	6.038	2002	6.106	1.114		
2.150	4.114	1001	6.108	6.038	2002	6.106	1.114		
2.151	4.114	1001	6.108	6.038	2002	6.106	1.114		
2.152	4.114	1001	6.108	6.038	2002	6.106	1.114		
2.153	4.114	1001	6.108	6.038	2002	6.106	1.114		
2.154	4.114	1001	6.108	6.038	2002	6.106	1.114		
2.155	4.114	1001	6.108	6.038	2002	6.106	1.114		
2.156	4.114	1001	6.108	6.038	2002	6.106	1.114		
2.157	4.114	1001	6.108	6.038	2002	6.106	1.114		
2.158	4.114	1001	6.108	6.038	2002	6.106	1.114		
2.159	4.114	1001	6.108	6.038	2002	6.106	1.114		
2.160	4.114	1001	6.108	6.038	2002	6.106	1.114		
2.161	4.114	1001	6.108	6.038	2002	6.106	1.114		
2.162	4.114	1001	6.108	6.038	2002	6.106	1.114		
2.163	4.114	1001	6.108	6.038	2002	6.106	1.114		
2.164	4.114	1001	6.108	6.038	2002	6.106	1.114		
2.165	4.114	1001	6.108	6.038	2002	6.106	1.114		
2.166	4.114	1001	6.108	6.038	2002	6.106	1.114		
2.167	4.114	1001	6.108	6.038	2002	6.106	1.114		
2.168	4.114	1001	6.108	6.038	2002	6.106	1.114		
2.169	4.114	1001	6.108	6.038	2002	6.106	1.114		
2.170	4.114	1001	6.108	6.038	2002	6.106	1.114		
2.171	4.114	1001	6.108	6.038	2002	6.106	1.114		
2.172	4.114	1001	6.108	6.038	2002	6.106	1.114		
2.173	4.114	1001	6.108	6.038	2002	6.106	1.114		
2.174	4.114	1001	6.108	6.038	2002	6.106	1.114		
2.175	4.114	1001	6.108	6.038	2002	6.106	1.114		
2.176	4.114	1001	6.108	6.038	2002	6.106	1.114		
2.177	4.114	1001	6.108	6.038	2002	6.106	1.114		
2.178	4.114	1001	6.108	6.038	2002	6.106	1.114		
2.179	4.114	1001	6.108	6.038	2002	6.106	1.114		
2.180	4.114	1001	6.108	6.038	2002	6.106	1.114		
2.181	4.114	1001	6.108	6.038	2002	6.106	1.114		
2.182	4.114	1001	6.108	6.038	2002	6.106	1.114		
2.183	4.114	1001	6.108	6.038	2002	6.106	1.114		
2.184	4.114	1001	6.108	6.038	2002	6.106	1.114		
2.185	4.114	1001	6.108	6.038	2002	6.106	1.114		
2.186	4.114	1001	6.108	6.038	2002	6.106	1.114		
2.187	4.114	1001	6.108	6.038	2002	6.106	1.114		
2.188	4.114	1001	6.108	6.038	2002	6.106	1.114		
2.189	4.114	1001	6.108	6.038	2002	6.106	1.114		
2.190	4.114	1001	6.108	6.038	2002	6.106	1.114		
2.191	4.114	1001	6.108	6.038	2002	6.106	1.114		
2.192	4.114	1001	6.108	6.038	2002	6.106	1.114		
2.193	4.114	1001	6.108	6.038	2002	6.106	1.114		
2.194	4.114	1001	6.108	6.038	2002	6.106	1.114		
2.195	4.114	1001	6.108	6.038	2002	6.106	1.114		
2.196	4.114	1001	6.108	6.038	2002	6.106	1.114		
2.197	4.114	1001	6.108	6.038	2002	6.106	1.114		
2.198	4.114	1001	6.108	6.038	2002	6.106	1.114		
2.199	4.114	1001	6.108	6.038	2002	6.106	1.114		
2.200	4.114	1001	6.108	6.038	2002	6.106	1.114		